

Myren Consulting, Inc.

**United States
Environmental Protection Agency
Woodheater Certification Program
Woodheater Certification Test Report**

**High Valley
Construction and Maintenance, Inc.
High Valley Stoves
Model 1600
Noncatalytic Woodstove**

April 12, 1999

Myren Consulting, Inc.

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EPA WEIGHTED AVERAGES CALCULATIONS
EPA WEIGHTED AVERAGE PARTICULATE EMISSION RATE

The weighted average particulate emission rate (\overline{PM}) for the
High Valley 1600 Noncatalytic woodheater
manufactured by High Valley
Woodstoves, Inc. is 2.73 g/hr.

EPA WEIGHTED AVERAGE OVERALL EFFICIENCY

The weighted average overall efficiency (\overline{OE}) for the
High Valley 1600 Noncatalytic woodheater is default (63)%.

II. EPA TEST RESULTS

* Denotes runs used in weighted average calculations

Run #	Dry Burn Rate/kg/hr	Grams/Hour	Overall Efficiency
<u>3</u>	<u>0.976</u>	<u>3.324</u>	
<u>2</u>	<u>0.989</u>	<u>3.380</u>	
<u>6</u>	<u>1.704</u>	<u>1.694</u>	
<u>1</u>	<u>3.353</u>	<u>3.455</u>	
<u>5'</u>	<u>1.246</u>	<u>1.749</u>	
<u>4²</u>	<u>1.360</u>	<u>1.560</u>	

Notes: 1. Run 5 = Fan Confirmation Test.
2. Run 4 broke Delta T.

III. EPA CUMULATIVE PROBABILITY CALCULATIONS

$$P_n = \frac{[\text{Hi Prob.} - \text{Low Prob.}][\text{Act. Dry Burn Rate} - \text{Low Dry Burn Rate}]}{.05} + \text{Low Prob.} = P_n$$

$P_1 = \frac{[.380 - .328][.976 - .950]}{.05} + .328 = .3550$
 $P_2 = \frac{[.380 - .328][.989 - .950]}{.05} + .328 = .3686$
 $P_3 = \frac{[.857 - .840][1.704 - 1.700]}{.05} + .840 = .8414$
 $P_4 = \frac{[.989 - .989][3.353 - 3.350]}{.05} + .989 = .9890$
 $P_5 = \frac{[- -][- -]}{.05} + =$
 $P_6 = \frac{[- -][- -]}{.05} + =$
 $P_7 = \frac{[- -][- -]}{.05} + =$
 $P_8 = \frac{[- -][- -]}{.05} + =$
 $P_9 = \frac{[- -][- -]}{.05} + =$
 $P_{10} = \frac{[- -][- -]}{.05} + =$
 $P_{11} = \frac{[- -][- -]}{.05} + =$
 $P_{12} = \frac{[- -][- -]}{.05} + =$
 $P_{13} = \frac{[- -][- -]}{.05} + =$
 $P_{14} = \frac{[- -][- -]}{.05} + =$
 $P_{15} = \frac{[- -][- -]}{.05} + =$

$K_1 = P_2 - P_0 =$	<u>.3686</u>	-	<u>.000</u>	=	<u>.3686</u>
$K_2 = P_3 - P_1 =$	<u>.8414</u>	-	<u>.3550</u>	=	<u>.4864</u>
$K_3 = P_4 - P_2 =$	<u>.9890</u>	-	<u>.3686</u>	=	<u>.6204</u>
$K_4 = P_5 - P_3 =$	<u>1.0000</u>	-	<u>.8414</u>	=	<u>.1586</u>
$K_5 = P_6 - P_4 =$	_____	-	_____	=	_____
$K_6 = P_7 - P_5 =$	_____	-	_____	=	_____
$K_7 = P_8 - P_6 =$	_____	-	_____	=	_____
$K_8 = P_9 - P_7 =$	_____	-	_____	=	_____
$K_9 = P_{10} - P_8 =$	_____	-	_____	=	_____
$K_{10} = P_{11} - P_9 =$	_____	-	_____	=	_____
$K_{11} = P_{12} - P_{10} =$	_____	-	_____	=	_____
$K_{12} = P_{13} - P_{11} =$	_____	-	_____	=	_____
$K_{13} = P_{14} - P_{12} =$	_____	-	_____	=	_____
$K_{14} = P_{15} - P_{13} =$	_____	-	_____	=	_____
$K_{15} = P_{16} - P_{14} =$	_____	-	_____	=	_____

IV. EPA WEIGHTED AVERAGES CALCULATIONS

The following formula is the one set out in Equation 28-1, Section 8.1, Method 28 and is to be used to calculate both the weighted average particulate emission rate (PM) and the weighted average overall efficiency (OE) as shown below. The formula uses interpolated probabilities for a given heat output demand calculated from the values listed in Table 28-1(2) in Method 28.

$$\overline{PM} = \frac{K_1 PM_1 + K_2 PM_2 + K_3 PM_3 + \dots + K_n PM_n}{K_1 + K_2 + K_3 + \dots + K_n}$$

WST5-Form 1, Page 4 of 4

Where \overline{PM} = The EPA weighted average particulate matter (PM) emission rate in grams per hour (g/hr).
 $K_1, K_2, K_3, \dots, K_n$ = The weighting factors for the individual test runs as determined in III above.
 $PM_1, PM_2, PM_3, \dots, PM_n$ = The particulate emission rates for the individual test runs as listed in II above.

And

$$\overline{OE} = \frac{K_1 OE_1 + K_2 OE_2 + K_3 OE_3 + \dots + K_n OE_n}{K_1 + K_2 + K_3 + \dots + K_n}$$

Where \overline{OE} = The EPA weighted average overall efficiency in percent (%).
 $K_1, K_2, K_3, \dots, K_n$ = The weighting factors for the individual runs as determined in III above.
 $OE_1, OE_2, OE_3, \dots, OE_n$ = The overall efficiencies for the individual test runs as listed in II above.

IV.A. EPA WEIGHTED AVERAGE PARTICULATE EMISSIONS CALCULATIONS

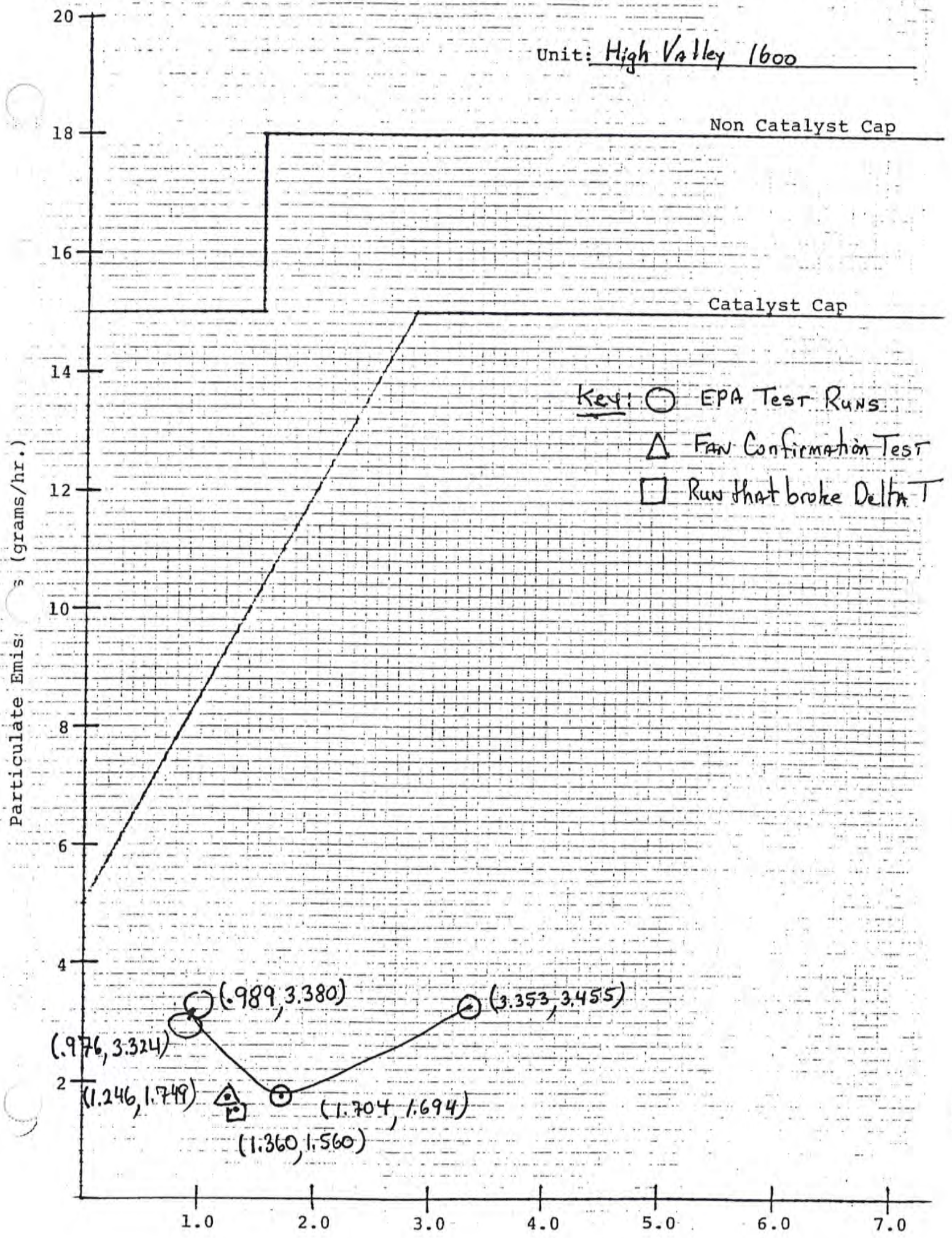
$$\overline{PM} = \frac{.3686(3.324) + .4864(3.380) + .6204(1.694) + .1586(3.455)}{.3686 + .4864 + .6204 + .1586} = \frac{3.640}{1.6340} = 2.2345 \text{ g/hr}$$

IV.B. EPA WEIGHTED AVERAGE OVERALL EFFICIENCY CALCULATIONS

$$\overline{OE} = \frac{K_1 OE_1 + K_2 OE_2 + K_3 OE_3 + \dots + K_n OE_n}{K_1 + K_2 + K_3 + \dots + K_n} = \frac{4.4682}{1.6340} = 2.7345$$

$$\overline{OE} = \frac{\quad}{\quad} = \frac{\quad}{\quad} = \frac{\quad}{\quad}$$

Unit: High Valley 1600



Woodstove Data Summary

	Run #	3	2	6	1	5'	4 ²
<u>Particulate Emissions:</u>							
Concentration:	grains/dscf:						
	grams/m ³ :						
Emission Rate:	grams/hr:	<u>3324</u>	<u>3380</u>	<u>1694</u>	<u>3455</u>	<u>1749</u>	<u>1560</u>
Emission Factor:	gms/kg:						
	(dry fuel weight basis)						
Front Half Catch:	% of total						
Total Mass Captured:							
Frt & Bck Halves:		<u>48.9</u>	<u>48.6</u>	<u>12.8</u>	<u>15.4</u>	<u>18.1</u>	<u>14.3</u>
							mg
<u>Efficiency Values:</u>							
Overall Appliance Efficiency							%
Combustion Efficiency							%
Heat Transfer Efficiency							%
<u>Heat Output:</u>							
Avg. BTU/hr for test cycle		<u>14768</u>	<u>11921</u>	<u>20548</u>	<u>40407</u>	<u>15023</u>	<u>16491</u>
							BTU/hr
<u>Fuel Burn Rates:</u>							
Avg Kg/hr for test cycle	(Wet basis)						
Avg Kg/hr for test cycle	(Dry basis)	<u>0.976</u>	<u>0.989</u>	<u>1.704</u>	<u>3.353</u>	<u>1.246</u>	<u>1.360</u>
							Kg/hr

Notes: 1. Run 5 = Fan Confirmation Test
 2. Run 4 broke Delta T

	3	2	6	1	5	4
<u>Average Temperatures:</u>						
Stack Gas	228	225	341	527	287	203 OF
Primary Combustion Chamber Gas	500	504	831	996	699	521 OF
Secondary Combustion Chamber Gas	846	873	1028	1201	948	947 OF
Catalytic Combustor Exit Gas	N/A	N/A	N/A	N/A	N/A	N/A OF
Stove Top	347	353	450	628	411	402 OF
Stove Left Sidewall	258	346	454	561	293	421 OF
Stove Back	349	346	416	504	416	410 OF
Stove Right Sidewall	408	413	505	680	442	478 OF
Stove Bottom	424	408	476	515	456	470 OF
Stove Temperature Change	-118.6	-83.2	-87.2	-88.0	-90.6	-125.8 OF

<u>Test Chamber Environment:</u>						
Avg. Barometric Pressure	28.527	28.546	28.394	28.537	28.400	28.518 in Hg
Avg. Temperature	69	71	69	76	71	69 OF
Avg. % Ambient Moisture	1.25	1.525	1.5125	1.20	1.125	1.225 % H2O
Avg. % Relative Humidity	48.0	52.0	56.5	42.0	45.0	48.0 %RH
Avg. Air Velocity	0	0	0	0	0	0 m/sec
Avg. Dilution Tunnel Draft (If Applicable)	0	0	0	0	0	0 in/H2O

<u>Test Fuel Weight and Burn Time:</u>						
Density (Dry basis)	4665	4359	4911	4205	4574	5363 gm/cm ³
Coal Bed Weight	4.2	4.3	3.5	3.5	3.5	3.5 lbs.
Pre Test Fuel Wt (Inc Kindling)	67.0	54.2	55.7	61.6	60.5	57.2 lbs.
Test Fuel Load Weight	17.2	17.2	17.4	17.2	17.2	17.3 lbs.
Total Test Cycle Burn Time	395	390	230	115	310	285 min.

	3	2	6	1	5	4
<u>Fuel Moisture Content:</u>						
Kindling (Wet basis)	11.479	11.248	12.470	11.478	11.609	11.609 %
Pretest Fuel (Wet basis)	19.010	18.194	18.159	18.624	18.805	18.576 %
Test Fuel (Wet basis)	17.647	17.632	17.234	17.616	17.492	17.215 %
<u>Air/Fuel Ratio:</u>						
lbs air/lbs fuel						
<u>Average Stack Gas Composition:</u>						
Avg. % CO2						%
Avg. % O2						%
Avg. % CO						%
Avg. % Excess Air						%
Avg. % Moisture						%
<u>Average Stack Gas Flow Rate:</u>						
Stack flow rate - EPA CMB						dscfm
CHO balance						dscfm
Tracer Gas						dscfm
Draft (Static)	-0.442	-0.416	-0.605	-0.870	-0.56	-0.59 in.H2O
Proportionality - Average	99.985	99.990	99.909	99.992	99.958	99.907
<u>Average Stack Gas Emission Factors:</u>						
CO - g/Kg						
g/hr						

DILUTION TUNNEL CALCULATIONS
3/31/96

hivalleyepa3

MYREN CONSULTING CERTIFICATION TEST DATA

File Name: hivalleyepa3

Stove Manufacturer: HI VALLEY

Model Number: XTEC

Lab Name: MYREN

Test Date: 3/22/99

Run Number: EPA 3

Meter Box Y Factor: 1.003

Barometric pressure (in): 28.527

Gas meter temp (ave): 81
delta H(ave): 0.900

Gas meter initial reading: 64.302

Gas meter final reading: 283.974

Front catch (acetone) mg: 7.4
first filter catch (mg): 42.8
second filter catch (mg): -1.3

tunnel flow (ave cfm): 144.276

Emission Rate(g/hr): 2.067

Emission Rate(M5H) : 3.324
vs/MtS:

vs ave: 0.0074
832.063
Tunnel average temp (°f): 86.902

Test time(min): 395

Fuel Load(lb. wet): 17.2

Wood moisture(%wet): 17.647

Burn rate(dry kg/hr): 0.976

Samp vol(scf): 205.417

front filter number: 778

back filter number: 777

acetone beaker number: 2

PRELIMINARY RESULTS

FINAL RESULTS

AUDITED

DATA SUMMARY

MODEL : XTEC

RUN: EPA 3

DATE: 3/22/99

DBR: 0.976

GPH UNADJ 2.067

ADJ 3.324431254

Run Time (min)	PITOT DELTAP (- INCH H2O)	TNL TEMP (°F)	GAS METER RDG (ft3)	GAS METER TEMP (°F)	GAS METER DELTA H (in.H2O)	TUNNEL VELOCIT (ft/min)	PROP RATE (%)	dDGM vol std (ft3)
0	0.041	92	64.302	76	0.900	846.36		
10	0.041	110	69.975	75	0.900	860.05	105.7	5.364
20	0.040	100	75.493	76	0.900	842.01	99.2	5.208
30	0.040	102	81.048	77	0.900	843.51	102.2	5.233
40	0.040	104	86.595	79	0.900	845.01	101.8	5.206
50	0.040	105	92.143	79	0.900	845.76	101.9	5.207
60	0.040	105	97.702	79	0.900	845.76	102.0	5.218
70	0.039	104	103.325	80	0.900	834.38	102.8	5.268
80	0.039	103	108.889	80	0.900	833.64	102.9	5.213
90	0.040	100	114.410	81	0.900	842.01	101.5	5.163
100	0.040	97	119.938	81	0.900	839.75	100.0	5.169
110	0.040	93	125.490	82	0.900	836.73	99.8	5.182
120	0.040	91	131.090	82	0.900	835.22	100.7	5.227
130	0.040	89	136.678	81	0.900	833.70	100.5	5.225
140	0.040	88	142.260	82	0.900	832.94	100.2	5.210
150	0.040	87	147.858	81	0.900	832.18	100.6	5.235
160	0.040	85	153.443	81	0.900	830.66	100.1	5.223
170	0.040	85	159.032	81	0.900	830.66	100.3	5.226
180	0.040	85	164.596	80	0.900	830.66	100.1	5.213
190	0.040	85	170.116	80	0.900	830.66	99.3	5.171
200	0.040	84	175.659	80	0.900	829.90	99.5	5.193
210	0.040	83	181.245	80	0.900	829.13	100.2	5.233
220	0.040	82	186.865	81	0.900	828.37	100.5	5.255
230	0.040	82	192.411	80	0.900	828.37	99.5	5.196
240	0.040	81	197.962	82	0.900	827.61	99.0	5.181
250	0.040	81	203.531	82	0.900	827.61	99.4	5.198
260	0.040	80	209.095	83	0.900	826.84	99.0	5.184
270	0.040	79	214.633	82	0.900	826.07	98.6	5.169
280	0.040	79	220.179	83	0.900	826.07	98.6	5.167
290	0.040	79	225.739	82	0.900	826.07	99.1	5.190
300	0.040	79	231.299	83	0.900	826.07	98.9	5.180
310	0.040	78	236.703	82	0.900	825.31	96.1	5.044
320	0.040	78	242.383	83	0.900	825.31	100.9	5.292
330	0.040	78	247.991	84	0.900	825.31	99.5	5.215
340	0.040	77	253.531	83	0.900	824.54	98.3	5.161
350	0.040	76	259.065	82	0.900	823.77	98.2	5.165

hivalleyepa3

360	0.040	76	264.574	83	0.900	823.77	97.7	5.133
370	0.040	76	270.096	82	0.900	823.77	98.1	5.154
380	0.040	75	275.600	83	0.900	823.00	97.4	5.128
390	0.040	75	281.121	82	0.900	823.00	98.0	5.153
395	0.040	75	283.974	82	0.900	823.00	101.3	2.663
420						0.00	0.0	0.000
430						0.00	0.0	0.000
440						0.00	0.0	0.000
450						0.00	0.0	0.000
460						0.00	0.0	0.000
470						0.00	0.0	0.000
480						0.00	0.0	0.000
490						0.00	0.0	0.000
500						0.00	0.0	0.000
510						0.00	0.0	0.000
520						0.00	0.0	0.000
530						0.00	0.0	0.000
540						0.00	0.0	0.000
550						0.00	0.0	0.000
560						0.00	0.0	0.000
570						0.00	0.0	0.000
580						0.00	0.0	0.000
590						0.00	0.0	0.000
600						0.00	0.0	0.000
610						0.00	0.0	0.000
620						0.00	0.0	0.000
630						0.00	0.0	0.000
640						0.00	0.0	0.000
650						0.00	0.0	0.000
660						0.00	0.0	0.000
670						0.00	0.0	0.000
680						0.00	0.0	0.000
690						0.00	0.0	0.000
700						0.00	0.0	0.000
710						0.00	0.0	0.000
720						0.00	0.0	0.000
730						0.00	0.0	0.000
740						0.00	0.0	0.000
750						0.00	0.0	0.000
760						0.00	0.0	0.000
770						0.00	0.0	0.000

DATE 3/22/99

PAGE 1 OF 2

MODEL # HIGH VALLEY X-TEC RUN # EPA #3

METER BOX # 511-M

METER Y 1,002

FILTER # (F) 778 (R) 777

PRE TEST LEAK RATE = .0005 CFM @ -15.5 IN. HG .9325/933

FILTER SIZE: 110 MM

POST TEST LEAK RATE = .000 CFM @ -10.0 IN. HG .974/974

PROBE LENGTH 24" G/ASS

TIME		METER READING CU.FT.	PITOT dp	TNL TEMP. (°F)	METER TEMP. (°F)	GAS METER dh	VAC IN. Hg	VELOCITY TRAVERSE			
CLOCK	ELAPSED							POINT	LOCATION	ΔP	TEMP
1435	00	64.302	-041	92	76	.90	0	N-1	0.5"	.028	96
45	10	69.975	-041	110	75	.90	0	2	1.5"	.040	96
55	20	75.493	-040	100	76	.90	0	3	4.5"	.044	96
1505	30	81.048	-040	102	77	.90	0	4	5.5"	.038	96
15	40	86.595	-040	104	79	.90	0	W-1	0.5"	.037	98
25	50	92.143	-040	105	79	.90	0	2	1.5"	.045	99
35	60	97.702	-040	105	79	.90	0	3	4.5"	.040	99
45	70	103.325	-039	104	80	.90	0	4	5.5"	.033	100
55	80	108.889	-039	103	80	.90	0	Avg. .0371 98			
1605	90	114.410	-040	100	81	.90	0	Pilot Leak Check Pre <input checked="" type="checkbox"/> Post <input checked="" type="checkbox"/>			
15	100	119.938	-040	97	81	.90	0	Cp = <u>0.99</u>	N 1 2 → W 1 2 (3) 4 3 4		
25	10	125.490	-040	93	82	.90	0	*-point of Avg. delta p			
35	20	131.090	-040	91	82	.90	0	Qs = $\left(\frac{\sqrt{(\Delta P \times BP)}}{T(^{\circ}R)}\right) \times 3167.2 =$ <u>138.133</u> cfm			
45	30	136.678	-040	89	81	.90	0	BP = <u>START 28.56</u> in Hg 60 28.54 120 28.53 180 28.53 240 28.52 300 28.52 360 28.51 395 28.505			
55	40	142.260	-040	88	82	.90	0	$\bar{X} = 28.527$ ✓			
1705	50	147.858	-040	87	81	.90	0				
15	60	153.443	-040	85	81	.90	0				
25	70	159.032	-040	85	81	.90	0				
35	80	164.596	-040	85	80	.90	0				
45	90	170.116	-040	85	80	.90	0				

DATE 3/22/99

PAGE 2 OF 2

MODEL # HIGH VALLEY X-TEC

RUN # EPA #3

METER BOX # 571M

METER Y 1.003

FILTER # (F) 778 (R) 777

PRE TEST LEAK RATE = .0005 CFM @ -15.5 IN. HG .9315/933

FILTER SIZE: 110 MM

POST TEST LEAK RATE = .000 CFM @ -100 IN. HG .974/971

PROBE LENGTH 24" GLASS

TIME		METER READING CU. FT.	PITOT dp	TNL TEMP. (°F)	METER TEMP. (°F)	GAS METER dh	VAC IN. Hg	VELOCITY TRAVERSE				
CLOCK	ELAPSED							POINT	LOCATION	ΔP	TEMP	
1755	2 ⁰⁰	175.659	-040	84	80	.90	0	N-1	0.5"	-.028	96	
1805	10	181.245	-040	83	80	.90	0	2	1.5"	-.040	96	
15	20	186.865	-040	82	81	.90	0	3	4.5"	-.044	96	
25	30	192.411	-040	82	80	.90	0	4	5.5"	-.038	96	
35	40	197.962	-040	81	82	.90	0	W-1	0.5"	-.037	98	
45	50	203.531	-040	81	82	.90	0	2	1.5"	-.045	99	
55	60	209.095	-040	80	83	.90	0	3	4.5"	-.040	99	
1905	70	214.633	-040	79	82	.90	0	4	5.5"	-.033	100	
15	80	220.179	-040	79	83	.90	0	Avg.		.0371	98	
25	90	225.739	-040	79	82	.90	0	Pilot Leak Check				
35	3 ⁰⁰	231.299	-040	79	83	.90	0	Pre	<input checked="" type="checkbox"/>		Post	<input checked="" type="checkbox"/>
45	10	236.703	-040	78	82	.90	0	Cp =	0.99			
55	20	242.383	-040	78	83	.90	0				N	
2005	30	247.991	-040	78	84	.90	0				1	
15	40	253.531	-040	77	83	.90	0				2	
25	50	259.065	-040	76	82	.90	0				3	
35	60	264.574	-040	76	83	.90	0				4	
45	70	270.096	-040	76	82	.90	0					
55	80	275.600	-040	75	83	.90	0					
2105	90	281.121	-040	75	82	.90	0					
2110	395	283.974	-040	75	82	.90	0					

Pilot Leak Check
Pre Post

Cp = 0.99

→ W 1 2 3 4

(3/4)

*=point of Avg. delta p

$$Q_s = \left(\frac{\sqrt{(\Delta P \times BP)}}{T(^{\circ}R)} \right) \times 3167.2 =$$

138.133 cfm

BP = ~~28.56~~ 28.56 in Hg

60 28.54
120 28.52
180 28.53
240 28.52
300 28.52
360 28.51
395 28.505

17.647 $\bar{x} = 28.527$

F - 44.9 R .5 395 17.2

WOODSTOVE DATA SHEET #4-1: INITIAL FILTER WEIGHTS (TARE WEIGHTS)

Into Dessicator: Date 1/8/99 Time 12:00 By ATM Front Half Back Half

Manufacturer: Schleicher & Schuell Size: 11cm Lot No.: ZB951 Grade: #25 g/ass
Order No. 06220

Filter #	First Wt	Date	Time	By	Second Wt	Date	Time	By	Third Wt	Date	Time	By
776	.7853	2/7/99	12:55	T.M.	.7853	2/10/99	1629	ATM				
777	.8127		12:56	T.M.	.8129		1628	ATM	←			
778	.8044		12:57	T.M.	.8040		1627	ATM	←			
779	.8036		12:58	T.M.	.8034		1626	ATM				
780	.7889		12:59	T.M.	.7888		1625	ATM				
781	.7894		1:00	T.M.	.7892		1625	ATM				
782	.7905		1:01	T.M.	.7903		1624	ATM				
783	.7967		1:02	T.M.	.7968		1623	ATM				
784	.8120		1:03	T.M.	.8118		1622	ATM				
785	.8166		1:04	T.M.	.8164		1621	ATM				
786	.7925		1:05	T.M.	.7923		1620	ATM				
787	.8064		1:06	T.M.	.8064		1619	ATM				
788	.7928		1:07	T.M.	.7926		1619	ATM				
789	.7774		1:08	T.M.	.7774		1618	ATM				
790	.7835		1:09	T.M.	.7835		1617	ATM				
791	.7981		1:10	T.M.	.7982		1616	ATM				
792	.8036		1:11	T.M.	.8035		1615	ATM				
793	.8116		1:12	T.M.	.8116		1614	ATM				
794	.8025		1:13	T.M.	.8024		1613	ATM				
795	.7766		1:14	T.M.	.7765		1613	ATM				
796	.7916		1:15	T.M.	.7915		1612	ATM				
797	.7755		1:16	T.M.	.7756		1611	ATM				
798	.8133		1:17	T.M.	.8133		1610	ATM				
799	.7949		1:18	T.M.	.7948		1610	ATM				
800	.8266	✓	1:19	T.M.	.8266	✓	1609	ATM				

Checked by Jen. Meyer Date: 2/21/99 Time 1405

QA REWEIGH

Filter #	WT	Date	Time	By
781	.7891	2/21/99	1412	Sm
789	.7772	2/21/99	1414	Sm
795	.7765	2/21/99	1415	Sm

BALANCE ROOM ENVIRONMENTAL CONDITIONS

WB	DB	%RH	Date	Time	By
62	76	45	2/21/99	1235	ATM
63	72	45	2/21/99	1305	ATM
65	80	44	2/21/99	1312	ATM

Post Weighing Section Scale Checks
 0.0000 0.0010 0.0020 0.0000
 1.0000 1.0001 1.0000 1.0001

WOODSTOVE DATA SHEET #4-2:
INITIAL BEAKER WEIGHTS (TARE WEIGHTS)

Into Dessicator: Date: 2/4/99 Time: 1600 By: A. T. Mucari

Beaker #	First Wt	Date	Time	By	Second Wt	Date	Time	By	Third Wt	Date	Time	By
1	65.4810	2/1/99	915	ATM	65.4838	2/3/99	1605	JM				
2	66.1516		917	ATM	65.1515	2/3	1606	JM	←			
3	67.8577		919	ATM	67.8571	2/3	1609	JM	67.8571	2/7/99	1245	ATM
4	67.5891		920	ATM	67.5886	2/3	1612	JM				
5	Broken											
6	67.4282		921	ATM	67.4282	2/3	1615	JM				
7	65.5451		922	ATM	65.5453	2/3	1617	JM				
8	60.0213		923	ATM	66.0213	2/3	1618	JM	← Blank			
9	66.9293		924	ATM	66.9294	2/3	1620	JM				
10	66.0888		926	ATM	66.0885	2/3	1621	JM				
11	65.6997		927	ATM	65.7015	2/3	1623	JM	65.7016	2/7/99	1247	ATM
12	56.0653		928	ATM	56.0652	2/3	1625	JM				
13	57.8945		929	ATM	57.8942	2/3	1627	JM				

Checked By: A. T. Mucari Date: 2/8/99 Time: 1705

Beaker #	WT	Date	Time	By

WB	DB	%RH	Date	Time	By
55	69	39	2/1/99	0910	ATM
63	76	48	2/3/99	1555	ATM
62	76	45	2/7/99	1235	ATM

WOODSTOVE DATA SHEET #4-3: CONSTANT FINAL WEIGHTS

WST5-Form9, Pg1, Rev4/90
 Unit Hi-Vol by XTEC
 Run # EPA-8
 Date: 3/22/99

FINAL BEAKER WEIGHTS

Beaker #	Into Dessic	Date	Time	By	First	Date	Time	By	Second	1999 Date	Time	By	Third	Date	Time	By
2	✓	3/29	2100	ATM	66.1590	4/6/99	1037	ATM	66.1590	7/7	1730	Jim	66.1590	4/8/99	1354	Jim

FINAL FILTER WEIGHTS

Filter #	Into Dessic	Date	Time	By	First	Date	Time	By	Second	Date	Time	By	Third	Date	Time	By
778		3/22/99	2237	ATM	.8492	3/23	1320	ATM	.8469	3/29	2047	Jim	.8468	4/5	1744	ATM
777		3/22/99	2237	ATM	.8119	3/23	1322	ATM	.8116	3/29	2100	Jim	.8116	4/5	1742	ATM

QA REWEIGH: FINAL WEIGHTS

Date	Beaker #	Final Wt	By
Date	Filter #	Final WT	By

SCALE ROOM ENVIRONMENTAL CONDITIONS

Weighing Session	Date	Time	By	WB	DB	%RH
1	3/23	1115	ATM	64	84	46
2	3/29	2038	ATM	59	72	45
3	4/5	1230	ATM	64	80	41
4	4/6	1030	ATM	61	75	44
5	4/7	1724	Jim	65	85	33

SCALE ROOM ENVIRONMENTAL CONDITIONS

	Date	Time	By	WB	DB	%RH
6	4/8	1346	ATM	67	80	50
7						
8						
9						
Comments						

WOODSTOVE DATA SHEET #4-3: CONSTANT FINAL WEIGHTS

Blank
3/13/99

WST5-Form9, Pg1, Rev4/90
Unit High Valley XTEC
Run # 5 EPA 23
Date: 3/22/99

Acetone Blank - 100 ml Acetone

Beaker #	Into Dessic	Date	Time	By	First	Date	Time	By	Second	Date	Time	By	Third	Date	Time	By
8	✓	3/13/99	0854	AMM	66.0215	3/19/99	2237	ATM	66.0215	3/20/99	1332	ATM				

FINAL FILTER WEIGHTS

Filter #	Into Dessic	Date	Time	By	First	Date	Time	By	Second	Date	Time	By	Third	Date	Time	By

QA REWEIGH: FINAL WEIGHTS

Date	Beaker #	Final Wt	By
Date	Filter #	Final WT	By

SCALE ROOM ENVIRONMENTAL CONDITIONS

Weighing Session	Date	Time	By	WB	DB	%RH
1	3/18	2140	AMM	68	84	43
2	3/20	1300	AMM	64	84	32
3						
4						
5						

SCALE ROOM ENVIRONMENTAL CONDITIONS

	6	7	8	9	Comments

WOODSTOVE DATA SHEET #4-4
SCALE QA SHEET

Scale Mettler
Model AE100
SN K04827

Dates From 1/9/99

Through _____

Level	Recalibrated	100g Weight	10g Weight	1.0g Weight	100mg Weight	20mg Weight	Date	Time	Tech	Wet Bulb	Dry Bulb	% RH
✓	Yes	99.9999	10.0001	1.0002	.1003	.0203	1/9/99	1243	ATM	58	70	48
✓	No	100.0002	10.0000	1.0000	.1000	.0200	1/14/99	1113	ATM	62	75	47
✓	YES	99.9999	10.0002	1.0000	.0999	.0201	1/23/99	1100	ATM	63	77	43
✓	YES	99.9999	10.0000	1.0000	.1000	.0201	1/24/99	1318	ATM	59	74	45
✓	YES	99.9999	10.0002	1.0000	.1002	.0200	2/1/99	0910	ATM	55	69	39
✓	YES	99.9999	10.0001	1.0001	.1002	.0201	2/2/99	0939	ATM	60	73	46
✓	YES	99.9999	10.0004	1.0001	.1001	.0200	2/3/99	1555	ATM	63	76	45
✓	YES	99.9999	10.0000	1.0001	.1001	.0201	2/4/99	1235	ATM	62	76	45
✓	YES	99.9999	10.0000	1.0000	.1000	.0200	2/10/99	1600	ATM	63	77	45
✓	YES	99.9999	10.0000	1.0001	.1000	.0200	2/19/99	0246	ATM	64	78	46
✓	No	99.9999	10.0000	1.0000	.1000	.0200	2/21/99	1312	ATM	65	80	44
✓	No	99.9999	10.0000	1.0001	.1000	.0200	2/25/99	1935	ATM	64	80	41
✓	YES	99.9999	10.0000	1.0000	.1001	.0200	2/26/99	1135	ATM	64	79	43
✓	YES	99.9999	10.0000	1.0001	.1000	.0200	3/15/99	1526	ATM	65	80	44
✓	YES	99.9999	10.0001	1.0001	.1001	.0200	3/14/99	1355	ATM	63	78	43
✓	No	100.0001	10.0000	1.0000	.1000	.0200	3/15/99	1622	ATM	66	81	45
✓	Yes	99.9997	10.0000	1.0001	.1000	.0200	3/16/99	2025	ATM	65	82	39
✓	Yes	99.9997	10.0000	1.0001	.1001	.0200	3/12/99	1615	ATM	63	77	42
✓	Yes	99.9997	10.0000	1.0001	.1000	.0200	3/18/99	2140	ATM	68	84	43
✓	Yes	99.9997	10.0000	1.0002	.1001	.0200	3/20/99	1300	ATM	64	84	32
✓	Yes	99.9999	10.0000	1.0001	.1001	.0201	3/21/99	2215	ATM	61	74	47
✓	Yes	99.9997	10.0000	1.0000	.1001	.0200	3/22/99	2122	ATM	65	85	33
✓	Yes	99.9997	10.0000	1.0001	.1000	.0200	3/23/99	1115	ATM	69	84	46
✓	Yes	99.9997	10.0000	1.0002	.1001	.0201	3/24/99	1120	ATM	77	89	43
✓	Yes	99.9999	10.0000	1.0002	.1001	.0201	3/29/99	2038	ATM	89	72	45
✓	No	99.9999	10.0002	1.0002	.1001	.0202	3/30/99	0610	ATM	66	80	47
✓	No	99.9999	10.0000	1.0000	.1001	.0201	3/31/99	1200	Sum	64	80	41
✓	No	99.9996	10.0000	1.0000	.1001	.0201	4/3/99	1730	ATM	64	80	41
✓	Yes	99.9998	10.0001	1.0001	.1001	.0201	4/6/99	1030	ATM	61	75	44
QC	Sequences	Audit	4/6/97	- wt.	Scale checked	at 100g						
✓	No	100.0003	10.0001	1.0001	.1001	.0201	4/6/99	1730	ATM			
✓	Yes	99.9999	10.0001	1.0001	.1001	.0200	4/8/99	1741	ATM	65	85	33
✓	No	99.9996	10.0000	1.0001	.1001	.0201	4/8/99	1346	ATM	67	80	50
✓	Yes	99.9997	10.0000	1.0000	.1000	.0200	4/16/99	1230	ATM	66	82	42
✓	Yes	99.9997	10.0000	1.0000	.1000	.0200	4/17/99	1625	ATM	68	84	43

Woodstove Particulate
Catch Processing Sheet
Woodstove Data Sheet #5
EPA M5G-1

Unit: Hi Valley XTEC
Run: EPA 3
Date: 3/22/99
Technicians: ATM
Revised 1/16/98-Data Sheet #5

Filters

Filter # (Front) 778 Beaker # 2 Final Wt. 66.1590 g ✓
Final Wt. .8468 g ✓ MI 65 Tare Wt. 66.1515 g ✓
Tare Wt. .8040 g ✓ Desc. Acetone Net Wt. .0075 g ✓
Net Wt. .0428 g ✓

Filter # (Rear) 777 Beaker # _____ Final Wt. _____ g
Final Wt. .8116 g ✓ MI _____ Tare Wt. _____ g
Tare Wt. .8129 g ✓ Desc. _____ Net Wt. _____ g
Net Wt. -.0013 g ✓

Acetone Blank Calculation:

Blank Date: 3/13/99
Blank Beaker # 8 Final Wt. 66.0215 g
MI 100 Tare Wt. 66.0213 g
Desc. Acetone Net Wt. 1.0002 g
.0002 g ÷ 100 ml = .000002 g/ml

Blank Residue Value Calculation:

.000002 g/ml acetone X 65 ml acetone = .00013 g
Blank Residue Value

Total Particulate Catch Calculation

Filter: .0428 g ✓
Filter: -.0013 g ✓
Beakers: .0075 g - .0001 g = .0074 g
Total Catch Blank Residue Value
Total Catch = .0489 g

Unit HIGH VALLEY X-TEC
 Run # EPA # 3
 Date 3/22/99
 Technician ATM, RLS,
 WST6-Form1, Rev8/96

MISCELLANEOUS TEST DATA
 WOODSTOVE DATA SHEET #8

Useable Firebox Dimensions: See QC Section Useable Volume: 2,713 ft³

Dilution Tunnel Draft (If applicable): Start 00.0 Stop 00.0

Test Chamber Air Velocity: Start: 00.0 Stop: 00.0 Avg: 00.0

Wet Bulb/ Start: WB: 56 °F DB: 68 °F 1.1 % Amb Moisture 46 %RH

Dry Bulb Stop: WB: 60 °F DB: 70 °F 1.4 % Amb Moisture 56 %RH

$\bar{X} = 1.250$ % Ambient Moisture $\bar{X} = 48.0$ % Relative Humidity (RH)

Empty

Stove Wt: 514.0 lbs.

Empty

Stove Wt with Stack (Inc. Oil Seal) Wet: 606.3 lbs. Dry: 604.2 lbs.

Empty

Stove Wt with Stack and Ash Ash: 0 lbs. Total: 604.2 lbs.

Kindling Wt.

Paper: 0.3 lbs. Wood: 5.0 lbs.

Pre Burn Fuel Wt. 17.0 + 17.2 + 16.6 + 16.2 Total: 67.0 lbs.

Total Kindling and Pre Burn Fuel Wt 72.3 lbs.

Coal Bed Wt-lbs: Range (608.5 - 607.7) 4.3 - 3.5 lbs. Actual: (4.2) lbs.

Allowable Amount of Charcoal that can be removed:

Coal Bed Wt. Range 4.3 + 3.5 12 X .25 = .9 lbs. ✓
 Upper Wt. Lower Wt.

Test Fuel Wt-lbs: Ideal 19.0 lbs. Range: 17.1 - 20.8 lbs. Actual: 17.2 lbs.

Test Fuel Size (pcs.) (.75 x 1.5 x 5" Flanges) 20 Pcs.

2 x 4's x 17.5 " 4 Pcs 9.3 lbs. 54.1 % ✓

4 x 4's x 17.5 " 2 Pcs 7.9 lbs. 45.9 % ✓

Est. Dry Burn Rate (Kg/Hr.) $\frac{17.2 - (17.2 \times .17647)}{2.2046} \times \frac{60}{395} = \frac{0.9760}{}$ Est. Dry Burn Rate (Kg/Hr) ✓

Est EPA Heat Output (HO_E) (Avg BTU's/Hr) $(19,140) \times \frac{.63}{100} \times .9760 = \frac{11,768}{}$ Est Heat Output (HO_E) BTU's/Hr ✓

Comments:

Stove Operating Data
Woodstove Test Data Sheet #9
Cold Start

Unit: HIGH VALLEY X-TEC
Run: EPA #3
Date: 3/22/99
Technician(s): ATM, PLS
Data Sheet #9 - Rev 1/98-Pg.2

Fire Started: 0813 P.S.T.

Warm up and Preburn: Primary Air: Wide open from ignition until the start of preburn when the primary air control(s) was (were) adjusted to the run setting of .75" OPEN. At the run setting until the start of the test.

Secondary Air: No Controls, Naturally drafted.

Secondary Burn/Cat Bypass: N/A

Charcoal Bed Preparation: Broke up, raked and leveled the coal bed prior to the addition of each warm up/pre burn fuel charge. Starting 1:30 before the start of the test, broke up, raked and leveled the coal bed. In stove for 35 seconds.

Test: Door wide open during loading 1 min 20 sec, then closed.

Primary Air: Wide open during the start of the test until 4:55. Adjusted to the run setting of 0.75" between 4:55 and 5:00. At the run setting of 0.75" at 5:00 into the run.

Secondary Air: No Controls, Naturally drafted.

Secondary Burn/Cat Bypass: N/A

Fan: ON/OFF during the warm up, ON/OFF high during the preburn, ON/OFF at the start of the test, ON/OFF for the first 30 minutes of the test, ON/OFF high at 30 minutes into the test, ON/OFF for the rest of the test.

Test Run Anomalies: This run was to be about 1.15 kg/hr, but a major wood fall @ about 100 mins blocked the LPDO air flow for a long time which slowed the burn rate down dramatically. There were also 2 preburns. The 1st was aborted when it was discovered that the Primary Air Setting was wrong (Su99)

WOODSTOVE OPERATING DATA
 WOODSTOVE DATA SHEET #9A-1

Wood Data: Kindling: A mix of the below grades

	Size	Mill	Grade	Species
Pre Burn	<u>2x4</u>	<u>CANYON LBR.</u>	<u>STD. & BTR.</u>	<u>D. FIR, S. GRN.</u>
Test Fuel	<u>2x4</u>	<u>CANYON LBR.</u>	<u>#2 STD. & BTR.</u>	<u>D. FIR, S. GRN.</u>
	<u>4x4</u>	<u>STAND & 879</u>	<u>#2 STD. & BTR.</u>	<u>D. FIR, S. GRN.</u>

All grades WCLB Rules unless otherwise noted.

Warm up Information:

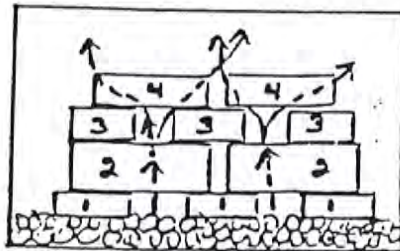
1st Warm up/Pre Burn Fuel charge (17.0 lbs) added at 0833.
 2nd Warm up/Pre Burn Fuel charge (17.2 lbs) added at 0938.
 3rd Warm up/Pre Burn Fuel charge (16.6 lbs) added at 1050.
 4th Warm up/Pre Burn Fuel charge (16.2 lbs) added at 1238.
 5th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.
 6th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.
 7th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.
 8th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.

The coals were scooped out of the stove immediately prior to adding the 3rd pre burn/warm up fuel charge. The stove lost 2.1 lbs. 3.0 lbs of coals put back in after the scoop.

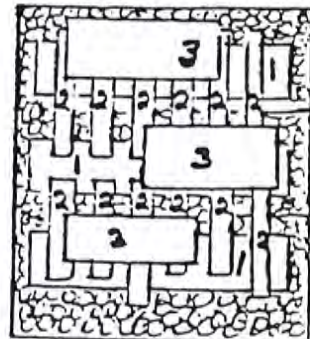
All pre burn/warm up fuel pieces were either 16 or _____ inches long. All preburn pieces/fuel charges were "ricked" in the stove. The pieces in the bottom layer in each rick contained 2 pcs that were 16 inches long and were loaded flat and perpendicular to the door. The pieces in the second layer in each rick were loaded on their side (edge) approximately parallel to the door and contained 4 pcs 16 inches long. The third layer (and fourth layer if present) was loaded flat, perpendicular to the door and contained 3 pcs 16 inches long. The majority of the pieces in each rick were in the second layer which had an approximate 0.5-1.0" space between pieces. (The loading directions indicate the direction of the longest dimension on each piece relative to the loading door opening.) Each pre burn/warm up fuel charge normally weighs within the weight range allowed for the actual test fuel charge

Warm up Information (cont.):

Each warm up/preburn fuel charge was ricked in exactly (as much as possible) the same manner and the weight of each rick was usually within the allowable weight range for the test fuel charge. The physical arrangement and alignment of each rick was designed to accomplish three (3) things: (1) The bottom layer was nestled firmly into the coal bed and was as close to being level with the bottom of the stove as possible, thus providing a stable loading platform for the rest of the rick, keeping it in a ricked state (as opposed to a col-lapsed or fallen down state) until the rick reached the charcoal stage and sags or collapses of its own accord. (2) It enhances the flow of primary air through the ricked preburn fuel charge, for the primary air would flow through the spaces between the pieces in the first layer and then up through the spaces between the pieces in the second, third and, if present, fourth layers. (3) It maximized, as much as possible, the surface to volume ratio of each preburn fuel charge, thereby allowing the fire immediate access to as much wood surface as possible and, thereby, insuring uniform charcoalization. All three of these enhance combustion and so get the stove as hot as possible during the warm up period, thereby maximizing the amount of heat (BTU's) stored in the stove. The actual preburn was not started until the stove surface temperatures had maximized and stabilized, thus indicating that the amount of heat stored in the stove had peaked. For this stove, the thermal storage was monitored using the TOP surface temperature(s) and the peak value(s) obtained were 930 of.



Front View



Top View

The arrows indicate the direction of the air flow through the rick.

The primary air was adjusted to the run setting of 0.75" SS lbs above the upper charcoal bed weight.

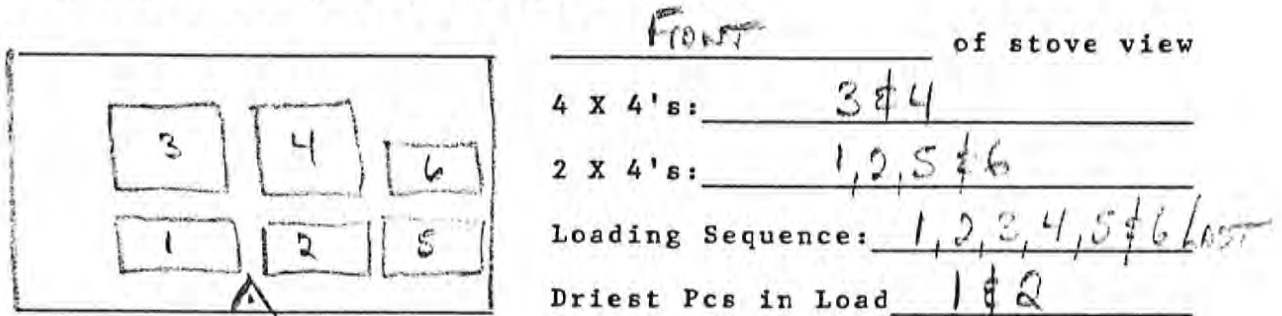
WOODSTOVE OPERATING DATA
WOODSTOVE DATA SHEET #9A-3

Unit HIGH VALLEY X-TEC
Run # EPA #3
Date 3/22/99
Technician ATH, RLS
Page 3 of 4
WST5-Form2-Rev11/89

Additional Comments: Test Start Sequence: ① Turned fan off.
② Opened Primary Air Control Wide Open ③ Opened door
④ Loaded test fuel charge into stove ⑤ cleaned coals
away from air front of V.C. LPAO ⑥ Photograph ⑦ closed
door.

Test Fuel Charge Loading Information:

Test Fuel Charge and Loading Sequence Diagram

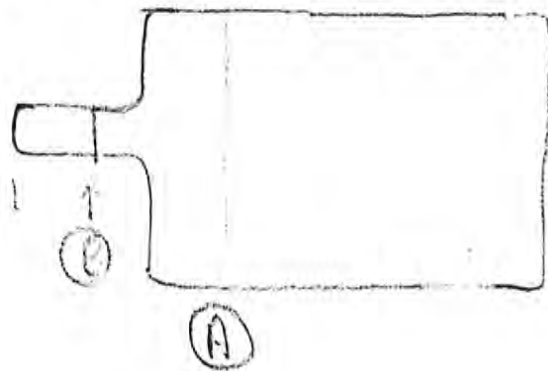


Loaded the test fuel charge on an essentially level, medium
sized, avg to cold coal bed (in appearance, color and temperature
for a M. low burn rate. Load 1:20, Ignition: N 1:00
VC to baffle 1:44, Secondaries igniting 2:00 Gas Balance
< 3:30, 5:00 Flames decreased. Maintained VC to baffle
with canyon with 2nds on top of VC, Plus a small VC
in R. canyon. Out of Balance 6:15, R. VC out 6:30, Back
@ 6:42, 11:30 2nd Tube has ignited already, 2nd tube is firing
13:08 2nds above 5 & 6, 16:20 4th tube firing
24:15 Gas Balance,
was a slower start than expected,

WOODSTOVE OPERATING DATA
WOODSTOVE DATA SHEET #9A-4

Additional Comments:

As noted earlier, there were two problems prior to the start of the test. The first was aborted because the primary air control was set wrong. The primary air inlet orifice is shaped as shown.



The first problem was with the PAC set at A. It was to be set at B. As the data shows the burn rate was too fast at A, so the problem was

aborted. The fire was burnt down to 2.0 lbs of coals & the 1/2" pile of problem fuel was added. From there on all was normal.

FUEL MOISTURE
WOODSTOVE TEST DATA SHEET #10

Unit: HIGH VALLEY X-TEC
Run: EPA #3
Date: 3/22/99
Technician: ATM, RLS.
WST1-Form7-Rev11/89

Room Temperature: 70 °F

Correction Factor: 0

NOTE: Record readings to the nearest 0.5% moisture
Uncor Values are corrected for temperature: Yes No
Time Test Fuel Moisture Readings taken at: 1045 ✓
Calibration Checks: X Y 12.5 12.5 22.0 22.2

Pc #	Dimen	Use	Top		Bottom		Side		Piece Avg Corrected
			Uncor	Cor	Uncor	Cor	Uncor	Cor	
1	2x4x8'	K	12.5	13.3	12.0	12.8	12.0	12.8	(12.967)
2									
3									
4	2x4x8'	P	22.0	23.7	22.0	23.7	21.0	22.6	23.333
5	"	P	22.0	23.7	22.0	23.7	21.5	23.1	23.500
6	"	P	22.0	23.7	22.5	24.3	22.0	23.7	23.900
7	"	P	21.5	23.1	22.0	23.7	21.5	23.1	23.300
8	"	P	22.0	23.7	21.5	23.1	21.5	23.1	23.300
9	"	P	22.0	23.7	22.0	23.7	21.5	23.1	23.500
10									(140.833)
11	2x4x17.5"	T	18.0	19.2	18.0	19.2	18.0	19.2	19.200
12	"	T	18.5	19.8	18.5	19.8	18.0	19.2	19.600
13	"	T	21.5	23.1	21.0	22.6	20.5	22.0	22.567
14	"	T	22.0	23.7	22.0	23.7	22.0	23.7	23.700
15									
16	4x4x17.5"	T	18.0	19.2	18.0	19.2	18.0	19.2	19.200
17	"	T	22.5	24.3	22.5	24.3	22.5	24.3	24.300
18									(128.567)
19	FEET	T	19.0	20.3	18.5	19.8	18.5	19.8	(19.967)
20									(OUT SPACERS)

	Kindling	Pretest Fuel	Test Load
% Moisture - Dry Basis:	12.967%	23.472%	21.428%
% Moisture - Wet Basis:	11.479%	19.010%	17.647%

To obtain Wet from Dry: $\frac{100 \times \% \text{ Dry Rdg.}}{100 + \% \text{ Dry Rdg.}} = \% \text{ Moisture, Wet Basis}$

Acceptable Ranges: 16-20% wet; 19-25% dry
(17.5 - 22.5 on Meter [Uncor reading] at 70°F)

Key for Use: K= Kindling P= Pretest Fuel T= Test Fuel

WOOD DENSITY DETERMINATION
WOODSTOVE TEST DATA SHEET #11

Unit: HIGH VALLEY X-TEC
Run#: EPA #3
Date: 3/22/99
Technician: ATM, PLS.
WST2-form11-Rev 6/90

Wood Piece: Nominal Dimensions: 3 1/2" x 3 1/2" x 1 1/2"
Depth (D): in 1.558 cm 3.957 ✓
Width (W): in 3.500 cm 8.890 ✓
Length (L): 3.579 cm in
3.531 cm in
3.535 cm in Length \bar{X} = 3.534 ✓ cm 8.976 ✓
3.550 cm in Volume: 315.755 cm³ ✓
(D X W X L)

MOISTURE: Room Temperature: 70 °F Correction Factor: 0
Uncorrected Meter Readings Corrected for temperature: Yes No

NOTE: Record moisture meter readings to the nearest 0.5%

	Uncor	Cor	%
Top:	<u>21.5</u>	<u>23.1</u>	<u>22.567</u> % ✓
Bottom:	<u>21.0</u>	<u>22.6</u>	<u>18.412</u> % ✓
Side:	<u>20.5</u>	<u>22.0</u>	
\bar{X} :		<u>22.567</u>	<u>22.567</u> % ✓

Avg % Moisture (Dry) 22.567 % ✓
Avg % Moisture (Wet) 18.412 % ✓
Scale: Leveled In Out
Zeroed: In Out

Wet Weight: 176.2 g Dry Weight: 147.3 g

% Moisture Dried Basis: 16.402 % ✓
[1 - (Dry Wt ÷ Wet Wt)] X 100

Into Dryer Date 3/22/99 Time 1050 Temp 213 °F
Out of Dryer Date 3/29/99 Time 1415 Temp 218 °F
(Minimum Time in Dryer: 24 hrs.) Minimum Dryer Temp 100°C (212°F)

Density = $\frac{147.3}{(\text{dry wt})}$ g ÷ $\frac{315.755}{(\text{volume})}$ cm³ = 0.4665 g/cm³ ✓

Pellet Fuel Moisture Content Determination

Tare Beaker Wt. _____ g
Wet Wt: _____ g - _____ g = _____ g
Gross Wet Wt. Tare Beaker Wt. Net Wet Wt.
Dry Wt: _____ g - _____ g = _____ g
Gross Dry Wt. Tare Beaker Wt. Net Dry Wt.
% Moisture Dried Basis: _____ %
[1 - (Net Dry Wt ÷ Net Wet Wt.)] X 100

DATE AND FLUE GAS DATA
 MODEL: OVE DATA SHEET #12
 WST2-Form 14 Rev 1/88
 EnvO Wt.: 628.4 lbs

Unit: HIGH VALLEY X-TEC Date: 3/22/99
 Run: EPA #3 Technician(s): ATM, P.S.
 Page: 1 of 4

Minute Time	Scale Wt	lbs left	Burn Rate	CO2		O2		CO		T/C(1)/T/C(2)		T/C(3)		Static Press.	Comments
				v.	%CO2	v.	%O2	TeI	v.	%CO	Bal	Wet Bulb	Dry Bulb		
5	625.6	17.2	0	1.77	4.42	59.7	14.96	29.4	1.48	3.0	81	115	103	-1.045	Flow
10	624.6	16.2	1.0	1.78	11.91	57.0	6.76	6.2	0.32	37.2	92	128	116	-1.082	SO2 1.5
15	624.1	15.7	1.5	2.77	6.91	53.1	13.31	15.9	0.81	8.5	119	143	132	-1.062	SO2 1.5
20	623.5	15.1	1.6	3.10	7.73	48.3	12.10	17.4	0.89	8.7	122	140	133	-1.062	SO2 1.5
25	622.9	14.5	1.6	3.64	9.07	43.9	11.00	22.5	1.14	8.0	124	140	135	-1.062	SO2 1.5
30	622.2	13.8	1.7	4.16	10.37	39.2	9.57	20.1	1.01	10.3	126	140	136	-1.065	
35	621.5	13.1	1.7	4.89	12.18	32.6	8.16	13.1	0.66	18.5	128	142	138	-1.068	
40	620.7	12.3	1.8	5.26	13.10	29.3	7.34	11.2	0.56	23.4	129	144	140	-1.070	
45	619.9	11.5	1.8	5.67	14.12	25.5	6.38	9.2	0.47	30.0	131	147	142	-1.072	
50	619.1	10.7	1.8	5.75	14.22	25.5	6.38	9.4	0.48	29.8	130	148	141	-1.072	
55	618.4	10.0	1.7	5.49	13.67	27.5	6.88	7.4	0.38	36.0	129	148	140	-1.071	
60	617.7	9.3	1.7	5.28	13.15	29.8	7.46	8.3	0.42	31.3	129	147	140	-1.070	
65	617.0	8.6	1.7	5.57	13.72	28.1	7.03	7.7	0.40	34.3	129	147	140	-1.801	Flow
70	616.4	8.0	1.6	5.42	13.50	28.1	7.03	6.4	0.33	40.9	128	145	139	-1.070	SO2 1.5
75	615.8	7.4	1.6	5.31	13.22	29.1	7.29	6.9	0.36	36.7	126	143	138	-1.069	SO2 1.5
80	615.3	6.9	1.5	5.32	13.25	29.0	7.26	6.6	0.34	39.0	124	141	137	-1.067	SO2 1.5
85	614.7	6.3	1.6	5.76	12.85	30.3	7.59	7.8	0.40	32.1	123	140	136	-1.067	SO2 1.5
90	614.2	5.8	1.5	4.99	12.43	31.5	7.89	10.1	0.52	23.9	121	137	135	-1.065	
95	613.8	5.4	1.4	4.73	11.78	33.7	8.44	8.2	0.43	27.4	118	133	132	-1.063	
100	613.4	5.0	1.4	4.39	10.94	37.0	9.27	7.5	0.38	28.8	115	130	130	-1.061	
105	613.2	4.8	1.2	3.40	8.48	45.8	11.47	19.9	1.02	8.3	111	124	126	-1.058	
110	613.0	4.6	1.2	2.89	7.21	50.1	12.55	17.9	0.92	7.8	106	118	122	-1.054	
115	612.8	4.4	1.2	2.79	6.96	50.9	12.75	16.5	0.84	8.3	100	113	118	-1.052	
120	612.7	4.3	1.1	2.60	6.49	52.7	13.21	17.2	0.88	7.4	95	109	113	-1.051	
125	612.7	4.3	1.1	2.60	6.49	52.7	13.21	17.2	0.88	7.4	95	109	113	-1.744	

7.1.111

Minute Time	Scale Wt	lbs left	Burn Rate	CO2		O2		CO		T/C(1)T/C(2)		T/C(3)		SO2 v.	Static Press.	Comments	
				v.	%CO2	v.	%O2	Te1	v.	%CO	Bal	Wet Bulb	Dry Bulb				% H2O
120	612.5	4.1	.1	26.9	6.71	50.9	12.75	21.1	1.07	6.3	91	107	4.4	111	247	-.050	Flow
125	612.4	4.0	.1	25.2	6.29	52.6	13.18	22.3	1.13	5.6	89	107	4.0	109	241	-.048	SO2 1.5
130	612.3	3.9	.1	24.6	6.14	53.3	13.36	23.4	1.18	5.2	86	107	3.5	107	235	-.047	SO2 1.5
135	612.2	3.8	.1	24.3	6.07	53.5	13.41	24.0	1.21	5.0	83	105	3.1	105	229	-.046	SO2 1.5
140	612.1	3.7	.1	24.8	6.19	53.1	13.31	23.4	1.18	5.2	82	104	2.9	104	226	-.045	SO2 1.5
145	612.0	3.6	.1	23.6	5.89	54.5	13.66	22.7	1.15	5.1	80	104	2.6	104	222	-.045	
150	612.0	3.6	0	23.3	5.82	54.5	13.66	24.4	1.24	4.7	79	103	2.5	102	219	-.044	
155	611.9	3.5	.1	22.5	5.62	55.3	13.86	25.9	1.32	4.3	78	102	2.4	102	216	-.043	
160	611.9	3.5	0	22.3	5.57	55.6	13.93	27.2	1.38	4.0	78	101	2.4	102	212	-.042	
165	611.8	3.4	.1	21.5	5.37	56.4	14.13	27.0	1.36	3.9	77	99	2.3	101	210	-.041	
170	611.7	3.3	.1	21.3	5.32	56.5	14.16	27.0	1.36	3.9	77	100	2.3	101	208	-.040	
175	611.6	3.2	.1	22.2	5.54	55.7	13.96	26.1	1.33	4.2	77	102	2.3	99	206	-.041	
180	611.5	3.1	.1	22.8	5.69	55.3	13.86	23.6	1.18	4.8	78	104	2.3	99	205	-.532	Flow
185	611.4	3.0	.1	21.7	5.42	56.0	14.03	26.5	1.33	4.1	78	104	2.3	98	203	-.040	SO2 1.5
190	611.3	2.9	.1	22.1	5.52	55.9	14.01	25.2	1.26	4.4	78	104	2.3	98	201	-.040	SO2 1.5
195	611.2	2.8	.1	22.1	5.52	56.0	14.03	26.2	1.32	4.2	78	104	2.3	98	200	-.040	SO2 1.5
200	611.1	2.7	.1	22.0	5.49	56.2	14.08	25.9	1.30	4.2	78	104	2.3	97	198	-.039	
205	611.0	2.6	.1	21.5	5.37	56.4	14.13	27.4	1.39	3.9	79	104	2.4	96	196	-.036	
210	610.9	2.5	.1	21.0	5.25	56.9	14.26	28.7	1.45	3.6	78	102	2.4	97	195	-.036	
215	610.8	2.4	.1	20.7	5.17	57.4	14.38	27.7	1.41	3.7	78	101	2.5	96	194	-.036	
220	610.7	2.3	.1	21.4	5.34	56.7	14.21	28.0	1.42	3.8	77	101	2.3	98	193	-.036	
225	610.6	2.2	.1	21.6	5.39	56.5	14.16	28.4	1.45	3.7	77	101	2.3	97	193	-.036	Wood Seal
230	610.6	2.2	0	20.5	5.12	59.1	14.81	25.0	1.28	4.0	78	100	2.5	97	192	-.035	IMO brand
235	610.5	2.1	.1	19.9	4.97	58.7	14.71	23.4	1.18	4.2	77	100	2.3	97	190	-.035	
															2360	-.448	(.980)
															5031		(.980)

END WT. 608.4 lbs

Minute Time	Scale Wt	lbs left	Burn Rate	CO ₂		O ₂		Tel		CO		Wet Bulb	Dry Bulb	% H ₂ O	Calc W/B	Stack	SO ₂ v.	PPM	Static Press.	Comments
				v.	%CO ₂	v.	%O ₂	v.	%CO											
240	610.4	2.0	.1	.193	4.82	59.1	14.81			24.2	1.22	77	100	2.3	96	189		-035	Flow	
245	610.3	1.9	.1	.192	4.80	59.2	14.84			26.0	1.33	76	99	2.2	95	187		-035	SO ₂ 1.5	
250	610.2	1.8	.1	.189	4.72	59.4	14.89			27.4	1.39	76	99	2.3	95	186		-034	CO ₂ 1.5	
255	610.2	1.8	0	.184	4.60	59.7	14.96			28.2	1.41	76	98	2.2	95	185		-034	O ₂ 1.5	
260	610.1	1.7	.1	.186	4.65	59.7	14.96			28.1	1.41	75	98	2.1	94	184		-034	CO 1.5	
265	610.0	1.6	.1	.189	4.72	59.1	14.81			30.0	1.51	75	98	2.1	93	183		-034		
270	609.9	1.5	.1	.195	4.83	58.6	14.69			29.6	1.50	75	97	2.1	92	181	Burnt flow	-034		
275	609.9	1.5	0	.216	5.39	58.8	14.23			27.7	1.40	75	97	2.1	92	181	CO ₂ 1.5	-034		
280	609.8	1.4	.1	.215	5.37	56.9	14.26			28.1	1.43	75	97	2.1	92	181	Flow	-034		
285	609.7	1.3	.1	.212	5.29	57.7	14.46			24.5	1.23	75	97	2.1	92	181		-033		
290	609.6	1.2	.1	.213	5.32	57.4	14.38			25.6	1.28	75	97	2.1	92	181		-033		
295	609.5	1.1	.1	.211	5.27	57.6	14.44			25.9	1.30	75	97	2.1	92	179		-033		
300	609.4	1.0	.1	.202	5.05	58.7	14.71									<u>2198</u>		<u>(-407)</u>	Flow	
305	609.4	1.0	0	.193	4.82	54.5	14.91			26.2	1.31	75	97	2.1	92	179		-033	SO ₂ 1.5	
310	609.3	.9	.1	.190	4.75	59.5	14.91			25.4	1.29	75	97	2.1	92	178		-032	CO ₂ 1.5	
315	609.2	.8	.1	.193	4.82	59.1	14.81			26.2	1.33	75	97	2.1	92	178		-033	O ₂ 1.5	
320	609.2	.8	0	.193	4.82	60.1	15.06			26.7	1.35	74	96	2.0	92	177		-032	CO 1.5	
325	609.1	.7	.1	.177	4.42	61.6	15.44			24.7	1.23	74	96	2.0	92	177		-032		
330	609.0	.6	.1	.166	4.15	62.0	15.54			23.7	1.20	74	96	2.0	92	176		-032		
335	609.0	.6	0	.158	3.95	63.5	15.92			25.9	1.32	74	96	2.0	92	176		-032		
340	608.9	.5	.1	.154	3.85	63.5	15.92			24.1	1.21	73	95	2.0	91	174		-031		
345	608.9	.5	0	.152	3.80	63.7	15.97			26.0	1.30	73	95	2.0	91	173		-031		
350	608.8	.4	.1	.152	3.80	63.8	15.99			25.1	1.27	73	95	2.0	90	172		-031		
355	608.8	.4	0	.153	3.83	63.6	15.94			24.9	1.28	73	94	2.0	90	170		-030		
360	608.8	.4	0							26.4	1.33	72	94	1.9	89	170		-030		
365	608.8	.4	0							<u>2100</u>						<u>2100</u>		<u>(-379)</u>		
370	608.8	.4	0							<u>4298</u>						<u>4298</u>		<u>(-786)</u>		

Pre Bu ⁵ Star w/f.
5.4 lbs. WP
Test Star w/f. Range 165.
608.4-607.7

PRE BURN DATA
RECORD SHEET #13
WST2-F01M16

18.67
BARD. P.E.
PRESSURE
38.65
50 W/M

Unit: HIGH VALLEY X-TEC Date: 3/22/99
Technician(s): ATH, PLS,
Run: EPA # 3 Page: 1 of 2

T/C#-3

Hot Box ON

Minute Time	Scale Weight	Burn Rate	Stack	Stove Top	Left Side	Back	Right Side	Bottom	Firebox	2nd Burn Catalyst	Room Temp	Static	Comments
0	613.8	0	644	905	538	482	584	554	714	1627	69	7.100	Primary Air Set at .75" OPEN
5	612.5	1.3	602	855	550	474	599	555	734	1523	69	7.097	Secondary Air Set at 1" X3"
10	611.5	1.0	560	791	563	472	613	555	760	1443	68	7.092	Fan: ON HIGH
15	610.7	.8	523	724	569	476	619	554	787	1385	70	7.087	TUNNEL ON AT: 1123
20	610.0	.7	501	677	575	483	624	555	809	1343	70	7.085	Buckets. I.A.E.D
25	609.5	.5	480	641	576	487	627	553	816	1296	70	7.087	ANALYZERS SPANNED
30	609.0	.5	462	611	573	492	627	548	827	1227	70	7.080	Pumps turned on at: 1200
35	608.6	.4	433	569	563	500	623	546	828	1166	70	7.075	AT
40	608.3	.3	413	536	556	510	615	544	817	1132	70	7.074	608.3 - 1 611.6
45	611.2	.5	411	507	544	578	606	544	807	1388	70	7.077	Check WB/DB: 3.4 lbs.
50	610.4	.8	448	550	540	504	601	538	803	1306	70	7.080	546.6
55	609.8	.6	439	556	538	495	595	529	801	1276	70	7.080	Probe IN TUNNEL
60	609.2	.6	429	548	537	488	587	523	795	1282	71	7.079	536.6
65	608.8	.4	370	535	534	485	581	531	784	1257	70	7.067	533.2
70	608.6	.2	327	504	529	472	571	539	764	1221	71	7.062	523.0
75	608.5	.1	307	475	577	462	560	543	744	1113	72	7.059	511.4
80													
85													
90													
95													
100													
105													

Aborted PAC Wrong - 12th Reburn

Pre Burn () itator wt.
 5.5 lbs. VP
 Test Start wt. Range WST2-Form16

PRE BURN DATA
 RECORD SHEET #13

28.62
 BAPD. PRESSURE
 28.59

Unit: HIGH VALLEY X-TEC Date: 3/22/99
 Run: EPA #3 Technician(s): ATH, PLS.
 Page: 1 of 2

Hot Box On

T/C#-3

Minute Time	Scale Weight	Burn Rate	Stack	Stove Top	Left Side	Back	Right Side	Bottom	Firebox	2nd Burn	Room Temp	Static	Comments
0	613.9	0	624	831	517	598	535	579	735	1412	73	-094	Primary Air Set at 75" OPEN
5	613.0	.9	488	779	530	564	557	533	735	1364	74	-082	Secondary Air Set at 1' X 3"
10	612.3	.7	431	711	535	525	559	537	738	1345	72	-077	Fan: ON HIGH
15	611.7	.6	401	661	536	502	561	534	742	1338	72	-074	TUNNEL ON AT: 1307
20	611.2	.5	381	626	534	493	562	529	741	1373	72	-072	Buckets I.C.E.D
25	610.8	.4	360	591	529	494	560	523	737	1375	71	-069	ANALYZERS SPANNED
30	610.5	.3	337	557	521	497	558	518	730	1252	71	-065	Pumps turned on at: 1350
35	610.2	.3	320	514	514	502	554	514	722	1206	72	-062	AT
40	609.9	.2	305	488	501	505	550	510	714	1179	71	-058	570.8
45	609.9	.1	289	461	491	503	544	506	706	1059	70	-058	Check WB/DB: 86/97
50	609.8	.1	278	437	480	497	538	503	700	1024	71	-055	RAKE COALS FORWARD
55	609.6	.2	276	427	475	486	531	501	691	991	71	-055	Probe IN TUNNEL
60	609.6	0	267	416	463	459	579	497	672	955	71	-052	
65	609.5	.1	261	406	456	446	571	494	661	957	71	-051	462.6
70	608.6	.1	266	392	450	435	501	490	656	941	71	-050	REMOVE COALS, 81b, 453.6
75	608.6	0	257	375	442	421	490	490	644	857	70	-050	443.6
80	608.5	.1	241	361	433	404	480	489	631	827	70	-049	433.4
85	608.5	0	235	349	423	389	468	486	613	819	70	-047	
90	608.4	.1	229	333	412	376	455	481	603	801	71	-045	411.4

Site: HIGH VALLEY X-TEC Date: 3/22/99
 Run: EPA #3 Technician(s): ATM, RLS,
 Page: 2 of 4

T/C#	Minute	Stove Top	Left Side	Back	Right Side	Bottom	Firebox	2nd Burn	Room Temp	Tunnel	C. Gas Box	Impinger Out	5G-1 Filter	5G-1 Condenser	Gen- dat
	120	392	441	386	464	421	611	927	68	91	257	42	82	41	250
	125	379	415	379	458	423	601	890	68	90	257	42	82	41	250
	130	367	405	373	452	427	591	867	68	89	257	42	81	41	250
	135	357	399	369	446	431	583	853	68	88	257	42	81	41	250
	140	349	393	368	441	434	575	840	67	88	250	41	80	41	250
	145	341	387	367	436	436	567	832	67	87	250	41	80	41	250
	150	335	382	365	432	438	559	822	67	87	250	40	79	41	250
	155	329	376	362	428	439	552	807	67	86	250	40	79	41	250
	160	323	372	359	424	440	545	793	67	85	250	40	78	41	251
	165	317	367	356	420	440	538	782	67	85	250	40	78	41	251
	170	313	366	352	417	440	532	769	68	85	257	41	78	41	251
	175	309	362	352	414	440	527	764	69	85	257	41	78	41	251
	180	306	358	353	412	440	522	764	69	85	257	41	78	41	251
	185	303	355	352	409	441	517	753	69	85	257	41	78	42	251
	190	300	351	352	407	441	512	752	70	85	257	41	78	42	251
	195	298	347	353	405	441	507	742	69	84	257	41	78	42	251
	200	295	345	356	404	440	502	735	69	84	257	41	78	42	251
	205	291	341	357	400	438	494	723	70	83	251	41	78	42	251
	210	290	339	358	399	437	490	724	70	83	251	41	78	42	251
	215	288	336	359	397	435	486	726	70	83	251	41	78	42	250
	220	286	333	359	396	433	481	726	70	82	250	41	78	42	250
	225	284	330	362	395	430	476	731	70	82	250	41	78	42	250
	230	282	327	367	395	427	472	707	70	82	249	41	77	42	248
	235	279	325	363	394	424	467	698	70	82	249	41	77	42	248
	240	285	350	408	481	522	595	838	81	82	249	41	77	42	248
	245	302	408	487	513	522	596	838	81	82	249	41	77	42	248
	250	350	468	549	581	522	596	838	81	82	249	41	77	42	248
	255	352	469	549	581	522	596	838	81	82	249	41	77	42	248
	260	352	469	549	581	522	596	838	81	82	249	41	77	42	248
	265	352	469	549	581	522	596	838	81	82	249	41	77	42	248

Hot Box 17

3654 41

@ 240 min DT = 354.0 DST = -57.4

2nd Box 17 18

T/C#	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
Minute	Stove Top	Left Side	Back	Right Side	Bottom	Firebox	2nd Burn	Room Temp	Tunnel	C. Gas Box	Impinger Out	5G-1 Filter	5G-1 Condenser	Gen. Jar	
240	275	322	358	393	422	461	694	70	81	249	40	77	44	248	
245	273	319	355	392	423	456	687	70	81	249	40	77	44	248	
250	271	315	353	391	424	451	679	70	81	249	42	77	44	249	
255	269	313	351	390	424	445	672	70	80	248	42	76	44	248	
260	266	310	349	389	423	441	672	70	80	248	42	76	44	249	
265	265	307	347	388	421	436	668	70	80	248	42	76	44	249	
270	263	304	346	388	420	432	681	70	79	249	42	76	44	249	
275	263	302	353	387	418	424	703	69	79	248	42	76	44	249	
280	263	299	366	388	416	424	694	70	79	247	42	75	45	249	
285	263	297	368	389	415	421	695	69	79	248	42	75	45	249	
290	263	295	368	389	414	419	696	69	79	247	42	75	45	249	
295	262	294	369	390	413	417	696	69	79	247	42	75	45	249	
300	261	293	368	391	413	416	694	69	79	247	42	75	45	249	315.2
305	260	291	366	390	413	415	682	69	78	247	42	74	45	248	
310	259	290	363	389	412	414	679	69	78	247	42	74	45	249	
315	258	289	358	387	410	413	674	69	78	246	42	74	45	248	
320	256	288	356	386	409	413	659	69	78	247	42	74	45	248	
325	255	288	352	384	410	414	647	69	78	246	42	74	45	247	
330	254	287	348	379	414	413	631	68	78	246	42	74	45	247	
335	251	287	345	374	412	411	629	69	77	246	42	74	45	248	
340	248	285	341	368	414	407	621	68	77	246	42	74	44	248	
345	246	283	338	362	419	404	612	68	77	246	42	73	44	247	
350	244	281	332	356	417	401	608	68	76	245	42	73	44	247	
355	241	278	324	351	415	397	609	68	76	245	42	73	44	247	
360	233	276	321	348	415	397	609	68	76	245	42	73	44	247	
365	229	271	317	341	410	391	601	68	76	245	42	73	44	247	

PRE AND POST TEST ZERO/SPAN CHECK
WOODSTOVE DATA SHEET #15-1

Site: Myren Consulting, Woodinville, WA Date: 3/22/99 Analyte: CO₂

Source: HIGH VALLEY X-TEC Run #: EPA # 3

Zero Cyl #: 36919 Conc. 00.0 % CO₂ Cyl Press: 220 psi

Certified by: CASCADE AIRGAS Date: 4/24/96

Span Cyl #: 250-1060 Conc. 6.0 % CO₂ Cyl Press: 1490 psi

Certified by: OxARC Date: 8/22/97

Analyzer: Make: Horiba Model: PIR-2000 SN: 607024

Range: 0 - 25.0% CO₂ Analyzer Output: 0 - 1.0 v.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter:

EPA Span Value = 25.0% CO₂

EPA Control Limits = + 2.5% of 25.0% CO₂ = + 0.625% CO₂

Pre Run Audit: By: ATM, RLS Time: 1337 Temp: 71 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	00.0	.000	.0256	.0256	+0.10
Span	24.0	.240	6.0	6.0	.240	5.991	-.0093	-0.15

Comments:

Post Run Audit: By: ATM, RLS. Time: 2256 Temp: 66 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	00.0	.001	.0504	+ .0504	+0.20
Span	24.0	.240	6.0	24.0	.230	5.941	-.0590	-0.98

Comments:

+ Conc. Difference = Act % - Exp (Std) %

Zero % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$

Span % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

PRE AND POST TEST ZERO/SPAN CHECK
WOODSTOVE DATA SHEET #15-2

Site: Myren Consulting, Woodinville, WA Date: 3/22/99 Analyte: O₂

Source: HIGH VALLEY X-TEC Run #: EPA # 3

Zero Cyl #: 36919 Conc. 00.0 % O₂ Cyl Press: 220 psi

Certified by: CASCADE AIRGAS Date: 4/24/96

Span Cyl #: 250-1060 Conc. 6.0 % O₂ Cyl Press: 1490 psi

Certified by: OxARC Date: 8/22/97

Analyzer: Make: Taylor Model: OA 137 SN: 13714772

Range: 0 - 25.0% O₂ Analyzer Output: 0 - 100 mv.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter: _____

EPA Span Value = 25.0% O₂

EPA Control Limits = + 2.5% of 25.0% O₂ = + 0.625% O₂

Pre Run Audit: By: ATH, RLS. Time: 1337 Temp: 71 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ%
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	00.0	00.0	0.0156	-0.0156	-0.06
Span	6.0	24.0	6.0	6.0	23.9	5.981	-0.0195	-0.32

Comments:

Post Run Audit: By: ATH, RLS. Time: 2256 Temp.: 66 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ%
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	00.0	00.0	0.0156	-0.0156	-0.06
Span	6.0	24.6	6.0	6.0	23.9	5.981	-0.0195	-0.32

Comments:

+ Conc. Difference = Act % - Exp (Std) %

Zero % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$

Span % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

PRE AND POST TEST ZERO/SPAN CHECK
WOODSTOVE DATA SHEET #15-3

Site: Myren Consulting, Woodinville, WA Date: 3/22/99 Analyte: CO

Source: HIGH VALLEY X-TEC Run #: EPA # 3

Zero Cyl #: 36919 Conc. 00.0 % CO Cyl Press: 270 psi

Certified by: CASCADE AIRGAS Date: 4/24/96

Span Cyl #: 250-1060 Conc. 1.26 % CO Cyl Press: 1490 psi

Certified by: OXARC Date: 8/22/97

Analyzer: Make: Infra Red Model: 702 D SN: 113

Range: 0 - 10.0% CO Analyzer Output: 0 - 100 mv.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter:

EPA Span Value = 5.0% CO

EPA Control Limits = +2.5% of 5.0% CO = + 0.125% CO

Pre Run Audit: By: ATM, RLS Time: 1337 Temp: 71 °F

Audit Results

Point #	Expected Response			Actual Response			± Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.00	00.0	0.0091	-0.0091	-0.18
Span	1.26	25.2	1.26	1.26	25.0	1.2467	-0.01326	-1.05

Comments:

Post Run Audit: By: ATM, RLS Time: 2256 Temp.: 56 °F

Audit Results

Point #	Expected Response			Actual Response			± Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.00	00.0	0.0091	-0.0091	0.18
Span	1.26	25.2	1.26	1.27	24.8	1.2367	-0.0233	-1.85

Comments:

+ Conc. Difference = Act % - Exp (Std) %

Zero % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$

Span % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

QUALITY CHECKS
 WOODSTOVE DATA SHEET #16

Ambient = Tr: 69 °F T/C#30: _____ °F
 Thermocouple Check (at ambient): T/C#1: 66 °F; T/C#2: 66 °F;
 T/C #3: 90 °F; T/C #4: 94 °F; T/C #5: 116 °F;
 T/C #6: 107 °F; T/C #7: 113 °F; T/C #8: 141 °F;
 T/C #9: 143 °F; T/C #10: 138 °F; T/C #11: 69 °F;
 T/C #12: 68 °F; T/C #13: 68 °F; T/C #14: 67 °F;
 T/C #15: 68 °F; T/C #16: 67 °F; T/C #17: 68 °F;
 T/C #18: _____ °F; T/C #19: _____ °F; T/C #20: _____ °F;
 T/C #21: _____ °F; T/C #22: _____ °F; T/C #23: _____ °F;
 T/C #24: _____ °F; T/C #25: _____ °F; T/C #26: _____ °F;

Comments: STOVE STILL WARM FROM OVER NIGHT BURN.

Thermocouple Readout: Pretest Zero/Span Check and Calibration:
 Zero (0°F) : 000 °F Adj to: 000 °F Post Test Check Zero (0°F): 000 °F % Difference +0.10
 Span (2000°F): 1999 °F Adj to: 2000 °F Span (2000°F): 2000 °F 0

(Allowable % Difference = 1.5%. Use formulas on Woodstove Data Sheet #15 to calculate % Difference)

Thermocouple Readout Pretest Linearity Check

0°F = 000 °F; 200°F = 200 °F; 400°F = 399 °F;
 600°F = 599 °F; 800°F = 800 °F; 1000°F = 1000 °F;
 1200°F = 1200 °F; 1400°F = 1400 °F; 1600°F = 1599 °F
 1800°F = 1800 °F; 2000°F = 2000 °F

Combustion Gas (CO₂, O₂, CO) Train Leak Check: Pre Post
 Draft (Static) Gauge Zero Check: Pre Post

Scale Check Pre (Wt, #'s): 606.3 - 611.3 5.0 lbs. OK (PLS!)
 Post (Wt, #'s): 613.3 - 608.3 = 5.0 lbs/5.0 lb = Ok ATH

Stack cleaned prior to the run: Yes _____ No
 Tunnel cleaned prior to the run: Yes _____ No

DILUTION TUNNEL CALCULATIONS

3/31/96

hivalleyepa2

MYREN CONSULTING CERTIFICATION TEST DATA

File Name: hivalleyepa2

Stove Manufacturer: HI VALLEY

Model Number: XTEC

Lab Name: MYREN

Test Date: 3/21/99

Run Number: EPA 2

Meter Box Y Factor: 1.003

Barometric pressure (in): 28.546

Gas meter temp (ave): 84
delta H(ave): 0.900

Gas meter initial reading: 846.701

Gas meter final reading: 1062.849

Front catch (acetone) mg: 6.1

first filter catch (mg): 41.1

second filter catch (mg): 1.5

tunnel flow (ave cfm): 144.829

Emission Rate(g/hr): 2.108

Emission Rate(M5H) : 3.380

vs/VmTs: 0.0076
vs ave: 834.045

Tunnel average temp (°f): 86.475

Test time(min): 390

Fuel Load(lb. wet): 17.2

Wood moisture(%wet): 17.632

Burn rate(dry kg/hr): 0.989

Samp vol(scf): 201.200

front filter number: 776

back filter number: 775

acetone beaker number: 1

PRELIMINARY RESULTS

FINAL RESULTS

AUDITED

MODEL: XTEC

RUN: EPA 2

DATE: 3/21/99

DBR: 0.989

GPH UNADJ: 2.108

ADJ: 3.380154065

Run Time (min)	PITOT DELTAP (- INCH H2O)	TNL TEMP (°F)	GAS METER RDG (ft3)	GAS METER TEMP (°F)	GAS METER DELTA H (in.H2O)	TUNNEL VELOCIT (ft/min)	PROP RATE (%)	dDGM vol std (ft3)
0	0.040	88	846.701	70	0.900	832.66		
10	0.038	100	852.150	73	0.900	820.42	103.0	5.175
20	0.039	97	857.611	76	0.900	828.91	103.6	5.158
30	0.039	99	863.110	77	0.900	830.40	103.4	5.184
40	0.041	100	868.615	79	0.900	852.19	103.2	5.170
50	0.040	99	874.145	80	0.900	840.98	100.6	5.184
60	0.041	100	879.775	81	0.900	852.19	103.8	5.268
70	0.040	100	885.219	82	0.900	841.73	98.9	5.085
80	0.040	99	890.745	83	0.900	840.98	101.2	5.152
90	0.041	97	896.289	83	0.900	849.90	101.3	5.169
100	0.041	94	901.826	84	0.900	847.61	99.4	5.153
110	0.040	92	907.370	85	0.900	835.70	99.2	5.150
120	0.041	91	913.020	85	0.900	845.31	102.4	5.248
130	0.041	89	918.448	85	0.900	843.78	96.9	5.042
140	0.041	87	923.993	85	0.900	842.24	98.8	5.151
150	0.041	86	929.631	86	0.900	841.47	100.3	5.227
160	0.041	85	935.097	86	0.900	840.70	97.1	5.068
170	0.041	83	941.200	85	0.900	839.15	108.3	5.669
180	0.040	82	946.200	84	0.900	828.09	88.9	4.653
190	0.041	82	951.775	85	0.900	838.38	100.3	5.178
200	0.041	81	957.307	85	0.900	837.61	98.1	5.138
210	0.041	81	962.878	86	0.900	837.61	98.7	5.165
220	0.041	80	968.495	85	0.900	836.83	99.5	5.217
230	0.040	80	974.005	86	0.900	826.56	97.5	5.109
240	0.040	80	979.555	85	0.900	826.56	99.6	5.155
250	0.040	80	985.112	85	0.900	826.56	99.8	5.162
260	0.040	80	990.610	85	0.900	826.56	98.7	5.107
270	0.040	80	996.228	85	0.900	826.56	100.9	5.218
280	0.040	80	1001.791	85	0.900	826.56	99.9	5.167
290	0.040	80	1007.371	85	0.900	826.56	100.2	5.183
300	0.040	80	1013.007	86	0.900	826.56	101.0	5.226
310	0.040	81	1018.453	86	0.900	827.33	97.8	5.049
320	0.040	81	1023.996	84	0.900	827.33	99.8	5.158
330	0.040	81	1029.561	85	0.900	827.33	100.0	5.169
340	0.040	80	1035.110	86	0.900	826.56	99.3	5.145
350	0.040	81	1040.663	85	0.900	827.33	99.9	5.158

hivalleyepa2

360	0.040	81	1046.197	86	0.900	827.33	99.3	5.131
370	0.040	80	1051.754	85	0.900	826.56	99.7	5.162
380	0.040	81	1057.300	86	0.900	827.33	99.6	5.142
390	0.040	81	1062.849	85	0.900	827.33	99.7	5.154
400						0.00	0.0	0.000
410						0.00	0.0	0.000
420						0.00	0.0	0.000
430						0.00	0.0	0.000
440						0.00	0.0	0.000
450						0.00	0.0	0.000
460						0.00	0.0	0.000
470						0.00	0.0	0.000
480						0.00	0.0	0.000
490						0.00	0.0	0.000
500						0.00	0.0	0.000
510						0.00	0.0	0.000
520						0.00	0.0	0.000
530						0.00	0.0	0.000
540						0.00	0.0	0.000
550						0.00	0.0	0.000
560						0.00	0.0	0.000
570						0.00	0.0	0.000
580						0.00	0.0	0.000
590						0.00	0.0	0.000
600						0.00	0.0	0.000
610						0.00	0.0	0.000
620						0.00	0.0	0.000
630						0.00	0.0	0.000
640						0.00	0.0	0.000
650						0.00	0.0	0.000
660						0.00	0.0	0.000
670						0.00	0.0	0.000
680						0.00	0.0	0.000
690						0.00	0.0	0.000
700						0.00	0.0	0.000
710						0.00	0.0	0.000
720						0.00	0.0	0.000
730						0.00	0.0	0.000
740						0.00	0.0	0.000
750						0.00	0.0	0.000
760						0.00	0.0	0.000
770						0.00	0.0	0.000

DATE 3/21/99

PAGE 1 OF 2

MODEL # HIGH VALLEY X-TEC RUN # EPA # 2

METER BOX # 511 M

METER Y 1.003

FILTER # (F) 776 (R) 77

PRE TEST LEAK RATE = .001 CFM @ -15.5 IN. HG. 3775/3785

FILTER SIZE: 110 MM

POST TEST LEAK RATE = .001 CFM @ -9.5 IN. HG. 869/870

PROBE LENGTH 24" Glass

TIME		METER READING CU. FT.	PITOT dp	TNL TEMP. (°F)	METER TEMP. (°F)	GAS METER dh	VAC IN. Hg	VELOCITY TRAVERSE			
CLOCK	ELAPSED							POINT	LOCATION	ΔP	TEMP
1510	00	846.701	-0.040	88	70	.90	0	N-1	0.5"	-0.034	96
20	10	852.150	-0.038	100	73	.90	0	2	1.5"	-0.043	97
30	20	857.611	-0.039	97	76	.90	0	3	4.5"	-0.041	98
40	30	863.110	-0.039	99	77	.90	0	4	5.5"	-0.035	98
50	40	868.615	-0.041	100	79	.90	0	W-1	0.5"	-0.038	101
1600	50	874.145	-0.040	99	80	.90	0	2	1.5"	-0.042	102
10	60	879.775	-0.041	100	81	.90	0	3	4.5"	-0.042	103
20	70	885.219	-0.040	100	82	.90	0	4	5.5"	-0.033	104
30	80	890.745	-0.040	99	83	.90	0	Avg. -0.0385			99.87
40	90	896.289	-0.041	97	83	.90	0	Pilot Leak Check			559.8
50	100	901.826	-0.041	94	84	.90	0	Pre	<input checked="" type="checkbox"/>	Post	<input checked="" type="checkbox"/>
1700	10	907.370	-0.040	92	85	.90	0	Cp = 0.99	N		
10	20	913.020	-0.041	91	85	.90	0	→ W 1 2 3 4			1
20	30	918.448	-0.041	89	85	.90	0				2
30	40	923.993	-0.041	87	85	.90	0	* = point of Avg. delta p			3
40	50	929.631	-0.041	86	86	.90	0	Qs = $\left(\frac{\sqrt{(\Delta P \times BF)}}{T(^{\circ}R)}\right) \times 3167.2 =$			4
50	60	935.097	-0.041	85	86	.90	0	140.260 cfm			
1800	70	941.200	-0.041	83	85	.90	0	BP = START 28.52 in Hg			
10	80	946.200	-0.040	82	84	.90	0	60 28.52			
20	90	951.775	-0.041	82	85	.90	0	120 28.52			
								180 28.52			
								240 28.525			
								300 28.550			
								28.590			
								360 28.600			
								X = 28.546			

F R
43.2 2.6

DATE 3/21/99

PAGE 2 OF 2

MODEL # STEC

RUN # EPA#2

METER BOX # 511M

METER Y 1.003

FILTER # (F) 776 (R) 775

PRE TEST LEAK RATE = .001 CFM @ -15.5 IN. HG .3775/.3785

FILTER SIZE: 110 mm

POST TEST LEAK RATE = .001 CFM @ -9.5 IN. HG .869/.870

PROBE LENGTH 24" gkas

TIME		METER READING CU. FT.	PITOT dp	TNL TEMP. (°F)	METER TEMP. (°F)	GAS. METER dh	VAC IN. Hg	VELOCITY TRAVERSE			
CLOCK	ELAPSED							POINT	LOCATION	ΔP	TEMP
1830	2 ⁰⁰	957.307	-041	81	85	.90	0	N-1	0.5"	-034	96
	40	962.878	-041	81	86	.90	0	2	1.5"	-043	97
	50	968.495	-041	80	85	.90	0	3	4.5"	-041	98
1900	30	974.005	-040	80	86	.90	0	4	5.5"	-035	98
	10	979.555	-040	80	85	.90	0	W-1	0.5"	-038	101
	20	985.112	-040	80	85	.90	0	2	1.5"	-042	102
	30	990.610	-040	80	85	.90	0	3	4.5"	-042	103
	40	996.228	-040	80	85	.90	0	4	5.5"	-033	104
	50	1001.791	-040	80	85	.90	0	Avg.		-0385	99.825
2000	90	1007.371	-040	80	85	.90	0	Pilot Leak Check			559.87
	10	1013.007	-040	80	86	.90	0	Pre		<input checked="" type="checkbox"/>	
	20	1018.453	-040	81	86	.90	0	Post		<input checked="" type="checkbox"/>	
	30	1023.946	-040	81	84	.90	0	Cp = 0.99			
	40	1029.561	-040	81	85	.90	0	→ W 1 2 3 4			
	50	1035.110	-040	80	86	.90	0	* = point of Avg. delta p			
2100	50	1040.663	-040	81	85	.90	0	Qs = $\left(\frac{\sqrt{(\Delta P \times BP)}}{T(^{\circ}R)}\right) \times 3167.2 =$			
	10	1046.197	-040	81	86	.90	0				140.260 cfm
	20	1051.754	-040	80	85	.90	0	BP = $\frac{54.5 \times 28.52}{60 \times 28.52}$ in Hg			
	30	1057.300	-040	81	86	.90	0				120 28.52
	40	1062.849	-040	81	85	.90	0				180 28.525
											240 28.550
											200 28.590
											360 28.600
											END 28.600

$\bar{X} = 28.546$

WOODSTOVE DATA SHEET #4-1: INITIAL FILTER WEIGHTS (TARE WEIGHTS)

Into Dessicator: Date 1/8/99 Time 12:00 By ATM Front Half Back Half

Manufacturer: Schleicher & Schuell Size: 11 cm Lot. No.: 78951 Grade: # 25g/las
Order No. 06220

Filter #	First Wt	Date	Time	By	Second Wt	Date	Time	By	Third Wt	Date	Time	By
751	.7787	1/23/99	1115	ATM	.7786	2/2/99	1051	T.M.				
752	.8115		1116	ATM	.8115		1050	ATM				
753	.8063		1117		.8061		1049	ATM				
754	.8044		1118		.8043		1048	ATM				
755	.7882		1119		.7878		1047	ATM				
756	.7831		1120		.7827		1046	ATM				
757	.7893		1121		.7886		1045	ATM	.7886	2/2/99	1430	Jm
758	.8025		1122		.8023		1044	ATM				
759	.7960		1123		.7956		1044	ATM	.7957	2/2/99	1240	T.M.
760	.7915		1124		.7914		1043	ATM				
761	.8115		1125		.8116		1042	ATM				
762	.7689		1126		.7687		1041	ATM				
763	.7894		1127		.7893		1040	ATM				
764	.7793		1128		.7792		1039	ATM				
765	.7910		1129		.7907		1038	ATM				
766	.7957		1130		.7954		1037	ATM				
767	.8028		1131		.8024		1036	ATM				
768	.8048		1132		.8044		1036	ATM				
769	.7728		1133		.7716		1035	ATM	.7715	2/2/99	1240	T.M.
770	.7894		1134		.7897		1034	ATM				
771	.7653		1135		.7691		1034	ATM				
772	.7895		1136		.7893		1033	ATM				
773	.8073		1137		.8070		1030	ATM				
774	.8181		1138		.8177		1031	ATM				
775	.8058	✓	1139	✓	.8051	✓	1030	ATM	←			

Checked by Jessie Miller Date: 2/2/99 Time 1430

QA REWEIGH

Filter #	WT	Date	Time	By
758	.8021	2/2/99	1431	Jm
762	.7685	2/2/99	1432	Jm
767	.8028	2/2/99	1433	Jm

BALANCE ROOM ENVIRONMENTAL CONDITIONS

WB	DB	%RH	Date	Time	By
62	77	42	1/22/99	1100	ATM
60	73	46	2/2/99	0939	ATM
62	76	45	2/2/99	1235	ATM
65	80	44	2/19/99	1312	ATM

Post Weighing Desiccation Scale Check
 1st 2nd 3rd
 0.0000 0.0000 -0.0002 0.0000
 1.0000 1.0000 0.9998 1.0001

WOODSTOVE DATA SHEET #4-1: INITIAL FILTER WEIGHTS (TARE WEIGHTS)

Into Dessicator: Date 1/8/99 Time 12:00 By ATM Front Half Back Half

Manufacturer: Schleicher & Schuell Size: 11cm Lot No.: ZR 951 Grade: #25 g/lbs
Order No. 06220

Filter #	First Wt	Date	Time	By	Second Wt	Date	Time	By	Third Wt	Date	Time	By
776	.7853	2/7/99	12:55	T.M.	.7853	2/10/99	1629	ATM	←			
777	.8127		12:56	T.M.	.8129		1628	ATM				
778	.8044		12:57	T.M.	.8040		1627	ATM				
779	.8036		12:58	T.M.	.8034		1626	ATM				
780	.7859		12:59	T.M.	.7888		1625	ATM				
781	.7894		1:00	T.M.	.7892		1625	ATM				
782	.7905		1:01	T.M.	.7903		1624	ATM				
783	.7967		1:02	T.M.	.7968		1623	ATM				
784	.8120		1:03	T.M.	.8118		1622	ATM				
785	.8166		1:04	T.M.	.8164		1621	ATM				
786	.7925		1:05	T.M.	.7923		1620	ATM				
787	.8064		1:06	T.M.	.8064		1619	ATM				
788	.7928		1:07	T.M.	.7926		1619	ATM				
789	.7774		1:08	T.M.	.7774		1618	ATM				
790	.7835		1:09	T.M.	.7835		1617	ATM				
791	.7981		1:10	T.M.	.7982		1616	ATM				
792	.8036		1:11	T.M.	.8035		1615	ATM				
793	.8116		1:12	T.M.	.8116		1614	ATM				
794	.8025		1:13	T.M.	.8024		1613	ATM				
795	.7766		1:14	T.M.	.7765		1613	ATM				
796	.7916		1:15	T.M.	.7915		1612	ATM				
797	.7755		1:16	T.M.	.7756		1611	ATM				
798	.8133		1:17	T.M.	.8133		1610	ATM				
799	.7949		1:18	T.M.	.7948		1610	ATM				
800	.8266	✓	1:19	T.M.	.8266	✓	1609	ATM				

Checked by Gene M. [Signature]

Date: 2/21/99 Time 1405

QA REWEIGH

Filter #	WT	Date	Time	By
781	.7891	2/21/99	1412	Sm
789	.7772	2/24/99	1414	Sm
795	.7765	2/21/99	1415	Sm

BALANCE ROOM ENVIRONMENTAL CONDITIONS

WB	DB	%RH	Date	Time	By
62	26	45	2/21/99	1235	ATM
63	72	45	2/21/99	1600	ATM
65	80	44	2/21/99	1312	ATM

Post Weighing 2000 Scale Check
 0.0000 0.0010 0.0020 0.0030
 1.0000 1.0001 1.0000 1.0001

QA

WOODSTOVE DATA SHEET #4-2:
INITIAL BEAKER WEIGHTS (TARE WEIGHTS)

Into Dessicator: Date: 1/4/99 Time: 1600 By: A.T.M. 191

Beaker #	First Wt	Date	Time	By	Second Wt	Date	Time	By	Third Wt	Date	Time	By
1	65.4840	2/1/99	915	ATM	65.4838	2/3/99	1605	JM	←			
2	66.1516		917	ATM	65.1515	2/3	1606	JM				
3	67.8577		919	ATM	67.8571	2/3	1609	JM	67.8571	2/7/99	1245	ATM
4	67.5891		920	ATM	67.5886	2/3	1612	JM				
5	Broken											
6	67.4202		921	ATM	67.4282	2/3	1615	JM				
7	65.5451		922	ATM	65.5453	2/3	1617	JM				
8	60.0213		923	ATM	60.0213	2/3	1618	JM	← Blank			
9	66.9293		924	ATM	66.9294	2/3	1620	JM				
10	66.0888		926	ATM	66.0885	2/3	1621	JM				
11	65.6997		927	ATM	65.7015	2/3	1623	JM	65.7016	2/7/99	1247	ATM
12	56.0653		928	ATM	56.0652	2/3	1625	JM				
13	57.8945		929	ATM	57.8942	2/3	1627	JM				

Checked By: A.T.M. Mucanj Date: 2/8/99 Time: 1705

QA REWEIGH

Beaker #	WT	Date	Time	By

BALANCE ROOM ENVIRONMENTAL CONDITIONS

WB	DB	%RH	Date	Time	By
55	69	39	2/1/99	0910	ATM
63	76	48	2/3/99	1555	ATM
62	76	45	2/7/99	1235	ATM

WOODSTOVE DATA SHEET #4-3: CONSTANT FINAL WEIGHTS

WST5-Form9, Pgl, Rev4/90
 Unit H. Valley, XTEC
 Run # E014 2
 Date 3/21/99

FINAL BEAKER WEIGHTS

Beaker #	Into Dessic	Date	Time	By	First	Date	Time	By	Second	Date	Time	By	Third	Date	Time	By
1	✓	3/24	1140	ATM	65.4905	3/25	2135	Jim	65.4900	4/6/99	1040	ATM	65.4899	4/7/99	1815	Jim

FINAL FILTER WEIGHTS

Filter #	Into Dessic	Date	Time	By	First	Date	Time	By	Second	Date	Time	By	Third	Date	Time	By
776	.8285	3/21/99	2221	ATM	.8275	3/22/99	2300	ATM	.8263	3/25	2105	Jim	.8264	4/5	1739	ATM
775	.8077	3/21/99	2221	ATM	.8067	3/22/99	2259	ATM	.8066	3/25	2104	Jim				

QA REWEIGH: FINAL WEIGHTS

Date	Beaker #	Final Wt	By
Date	Filter #	Final WT	By

SCALE ROOM ENVIRONMENTAL CONDITIONS

Session	Date	Time	By	WB	DB	%RH
1	3/22	2015	ATM	65	85	33
2	3/25	2038	ATM	59	72	45
3	4/5	1730	ATM	64	90	41
4	4/6	1030	ATM	61	75	44
5	4/7	1724	Jim	65	85	33

SCALE ROOM ENVIRONMENTAL CONDITIONS

Session	Date	Time	By	WB	DB	%RH
6						
7						
8						
9						
Comments						

Blank
3/13/99

WOODSTOVE DATA SHEET #4-3: CONSTANT FINAL WEIGHTS

Acetone Blank - 100 ml Acetone

Beaker #	Into Dessic	Date	Time	By	First	Date	Time	By	Second	Date	Time	By	Third	Date	Time	By
B	✓	3/13/99	0854	AM	66.0215	3/13/99	2237	ATM	66.0215	3/13/99	1332	ATM				

FINAL FILTER WEIGHTS

Filter #	Into Dessic	Date	Time	By	First	Date	Time	By	Second	Date	Time	By	Third	Date	Time	By

QA REWEIGH: FINAL WEIGHTS

Date	Beaker #	Final Wt	By

SCALE ROOM ENVIRONMENTAL CONDITIONS

Weighing Session	Date	Time	By	WB	DB	%RH
1	3/18	2140	ATM	68	74	43
2	3/20	1300	ATM	64	84	32
3						
4						
5						

SCALE ROOM ENVIRONMENTAL CONDITIONS

6						
7						
8						
9						
Comments						

WOODSTOVE DATA SHEET #4-4
SCALE QA SHEET

Dates From 1/19/99

Scale Mettler
Model AE101
SN K0482

Through _____

Level	Recall- brated	100g Weight	10g Weight	1.0g Weight	100mg Weight	20mg Weight	Date	Time	Tech	Wet Bulb	Dry Bulb	% RH
✓	Yes	99.9999	10.0001	1.0002	.1003	.0203	1/19/99	1243	ATM	57	70	48
✓	No	100.0002	10.0000	1.0000	1.000	1.0200	1/14/99	1113	ATM	62	75	47
✓	Yes	99.9996	10.0002	1.0000	.0999	.0201	1/23/99	1100	ATM	63	77	42
✓	Yes	99.9999	10.0000	1.0000	1.000	1.0201	1/14/99	1318	ATM	59	71	40
✓	Yes	99.9996	10.0002	1.0000	1.000	1.0200	2/1/99	0910	ATM	55	69	39
✓	Yes	99.9994	10.0001	1.0001	1.0002	1.0201	2/2/99	0959	ATM	60	73	46
✓	Yes	99.9999	10.0001	1.0001	1.0001	1.0200	2/3/99	1535	ATM	63	76	47
✓	Yes	99.9999	10.0000	1.0001	1.0001	1.0201	2/7/99	1235	ATM	62	76	45
✓	Yes	99.9998	10.0000	1.0000	1.000	1.0200	2/10/99	1600	ATM	63	77	45
✓	Yes	99.9998	10.0000	1.0001	1.0000	1.0200	2/19/99	0246	ATM	64	78	44
✓	No	99.9999	10.0000	1.0000	1.000	1.0200	2/21/99	1312	ATM	63	80	44
✓	No	99.9997	10.0000	1.0001	1.000	1.0200	3/5/99	1435	ATM	64	80	41
✓	Yes	99.9997	10.0000	1.0000	1.0001	1.0200	3/6/99	1135	ATM	64	79	43
✓	Yes	99.9997	10.0000	1.0001	1.000	1.0200	3/13/99	1526	ATM	65	80	44
✓	Yes	99.9999	10.0001	1.0001	1.0001	1.0200	3/14/99	1335	ATM	63	78	40
✓	No	100.0001	10.0000	1.0000	1.000	1.0200	3/15/99	1642	ATM	66	81	40
✓	Yes	99.9997	10.0000	1.0001	1.000	1.0200	3/16/99	0025	ATM	65	82	39
✓	Yes	99.9996	10.0000	1.0001	1.0001	1.0200	3/17/99	1615	ATM	62	77	42
✓	Yes	99.9997	10.0000	1.0001	1.000	1.0200	3/18/99	2140	ATM	68	84	43
✓	Yes	99.9997	10.0000	1.0000	1.000	1.0200	3/20/99	1300	ATM	64	84	32
✓	Yes	99.9999	10.0000	1.0001	1.0001	1.0201	3/21/99	2215	ATM	61	74	47
✓	Yes	99.9997	10.0000	1.0000	1.0001	1.0200	3/22/99	2127	ATM	65	85	33
✓	Yes	99.9997	10.0000	1.0001	1.000	1.0200	3/23/99	1115	ATM	69	74	46
✓	Yes	99.9997	10.0000	1.0002	1.0001	1.0201	3/24/99	1120	ATM	77	89	43
✓	Yes	99.9999	10.0000	1.0002	1.0001	1.0201	3/29/99	2038	ATM	67	72	45
✓	No	99.9999	10.0002	1.0002	1.0001	1.0202	3/30/99	0910	ATM	66	80	47
✓	No	99.9999	10.0000	1.0000	1.0001	1.0201	3/31/99	1200	Yes	67	80	41
✓	No	99.9996	10.0000	1.0000	1.0001	1.0201	4/5/99	1730	ATM	64	80	41
✓	Yes	99.9997	10.0001	1.0001	1.0001	1.0201	4/6/99	1030	ATM	61	75	44
QA	Success	Fluid	4/6/97	- wt. / scale	0.0001	0.0201						
✓	No	100.0003	10.0001	1.0001	1.0001	1.0201	4/6/99	1730	ATM			
✓	Yes	99.9998	10.0001	1.0001	1.0001	1.0200	4/7/99	1724	ATM	65	85	33

Woodstove Particulate
Catch Processing Sheet
Woodstove Data Sheet #5
EPA M5G-1

Unit: H: Valley ATEC
Run: EPA 12
Date: 3/21/98
Technicians: ATM
Revised 1/16/98-Data Sheet #5

Filters

Filter # (Front) 776 Beaker # 1
Final Wt. .8264 g MI 35
Tare Wt. .7853 g Desc. Acetone
Net Wt. .0411 g

Final Wt. 65.4899 g ✓
Tare Wt. 65.4838 g ✓
Net Wt. .0061 g ✓

Filter # (Rear) 775 Beaker # _____
Final Wt. .8066 g MI _____
Tare Wt. .8051 g Desc. _____
Net Wt. .0015 g ✓

Final Wt. _____ g
Tare Wt. _____ g
Net Wt. _____ g

Acetone Blank Calculation:

Blank Date: 3/13/99

Blank Beaker # 8
MI 100
Desc. Acetone
.0002 g ÷ 100 ml =

Final Wt. 66.0215 g
Tare Wt. 66.0213 g
Net Wt. .0002 g
.000002 g/ml

Blank Residue Value Calculation:

.000002 g/ml acetone X 35 ml acetone = .00007 g
Blank Residue Value

Total Particulate Catch Calculation

Filter: .0411 g ✓
Filter: .0015 g ✓
Beakers: .0061 g - .0001 g = .0060 g
Total Catch Blank Residue Value
Total Catch = .0486 g

Unit: HIGH VALLEY X-TEC
 Run # BDA #2
 Date 3/21/99
 Technician ATM, RLS.
 WST6-Form1, Rev8/96

MISCELLANEOUS TEST DATA
 WOODSTOVE DATA SHEET #8

Useable Firebox Dimensions: See QC Section Useable Volume: 2.713 ft³

Dilution Tunnel Draft (If applicable): Start 00.0 Stop 00.0

Test Chamber Air Velocity: Start: 00.0 Stop: 00.0 Avg: 00.0

Wet Bulb/ Start: WB: 64 °F DB: 74 °F 1.65 % Amb Moisture 58 %RH

Dry Bulb Stop: WB: 61 °F DB: 74 °F 1.40 % Amb Moisture 46 %RH

$\bar{X} = 1.525$ % Ambient Moisture $\bar{X} = 52$ % Relative Humidity (RH)

Empty

Stove Wt: 514.0 lbs.

Empty

Stove Wt with Stack (Inc. Oil Seal) Wet: 606.6 lbs. Dry: 604.8 lbs.

Empty

Stove Wt with Stack and Ash Ash: 0 lbs. Total: 604.8 lbs.

Kindling Wt. Paper: 0.6 lbs. Wood: 5.9 lbs.

Pre Burn Fuel Wt. 15.1 + 16.3 + 16.3 Total: 47.7 lbs. ✓

Total Kindling and Pre Burn Fuel Wt. 54.2 lbs. ✓

Coal Bed Wt-lbs: Range (4.3 - 3.5) 609.1 - 608.3 lbs. Actual: (4.3) lbs.

Allowable Amount of Charcoal that can be removed:

Coal Bed Wt. Range 4.3 + 3.5 $12 \times .25 =$ 0.9 lbs. ✓
 Upper Wt. Lower Wt.

Test Fuel Wt-lbs: Ideal 19.0 lbs. Range: 17.1 - 20.8 lbs. Actual: 17.2 lbs.

Test Fuel Size (pcs.) (.75 x 1.5 x 5" Flanges) 20 Pcs.

2 x 4's x " 4 Pcs 9.4 lbs. 54.65 % ✓

4 x 4's x " 2 Pcs 7.8 lbs. 45.35 % ✓

Est. Dry Burn Rate (Kg/Hr.) $\frac{17.2 - (17.2 \times .17632)}{2.2046} \times \frac{60}{390} =$.9886 Est. Dry Burn Rate (Kg/Hr) ✓

Est EPA Heat Output (HO_E) (19,140) $\times \frac{63}{100} \times .9886 =$ 11921 Est Heat Output (HO_E) BTU's/Hr ✓

Comments:

385 min = 1.0015

Stove Operating Data
Woodstove Test Data Sheet #9
Cold Start

Unit: HIGH VALLEY X-TEC
Run: EPA #2
Date: 3/21/99
Technician(s): ATM, RLS
Data Sheet #9 - Rev 1/98-Pg.2

Fire Started: 10:20 P.S.T.

Warm up and Preburn: Primary Air: Wide open from ignition until the start of preburn when the primary air control(s) was (were) adjusted to the run setting of 0.55". At the run setting until the start of the test.

Secondary Air: No Controls, Naturally drafted.

Secondary Burn/Cat Bypass: N/A

Charcoal Bed Preparation: Broke up, raked and leveled the coal bed prior to the addition of each warm up/pre burn fuel charge. Starting 1:30 before the start of the test, broke up, raked and leveled the coal bed. In stove for _____ seconds.

Test: Door wide open during loading 1 min 30 sec, then closed,

Primary Air: Wide open during the start of the test until 4:55. Adjusted to the run setting of 0.55" between 4:55 and 5:00. At the run setting of 0.55" at 5:00 into the run.

Secondary Air: No Controls, Naturally drafted

Secondary Burn/Cat Bypass: N/A

Fan: ON OFF during the warm up, ON/OFF high during the preburn, ON/OFF at the start of the test, ON/OFF for the first 30 minutes of the test, ON/OFF high at 30 minutes into the test, ON/OFF for the rest of the test.

Test Run Anomalies:

WOODSTOVE OPERATING DATA
 WOODSTOVE DATA SHEET #9A-1

Wood Data: Kindling: A mix of the below grades

	Size	Mill	Grade	Species
Pre Burn	<u>2x4</u>	<u>CANYON LBR.</u>	<u>STD. & BTR.</u>	<u>D. FIR, S. GRN.</u>
Test Fuel	<u>2x4</u>	<u>CANYON LBR.</u>	<u>#2 STD. & BTR.</u>	<u>D. FIR, S. GRN.</u>
	<u>4x4</u>	<u>STAND #879</u>	<u>#2 STD. & BTR.</u>	<u>D. FIR, S. GRN.</u>

All grades WCLB Rules unless otherwise noted.

Warm up Information:

1st Warm up/Pre Burn Fuel charge (15.1 lbs) added at 1040.
 2nd Warm up/Pre Burn Fuel charge (16.3 lbs) added at 1148.
 3rd Warm up/Pre Burn Fuel charge (16.3 lbs) added at 1250.
 4th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.
 5th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.
 6th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.
 7th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.
 8th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.

The coals were scooped out of the stove immediately prior to adding the 3rd pre burn/warm up fuel charge. The stove lost 1.8 lbs. 3.0 lbs. of coals put back in after the scoop

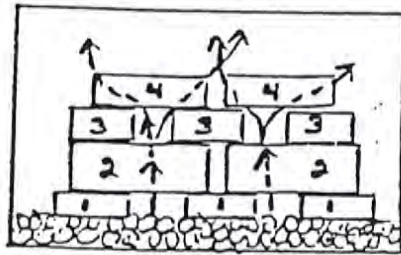
All pre burn/warm up fuel pieces were either 16" or _____ inches long. All preburn pieces/fuel charges were "ricked" in the stove. The pieces in the bottom layer in each rick contained 2 pcs that were 16 inches long and were loaded flat and perpendicular to the door. The pieces in the second layer in each rick were loaded on their side (edge) approximately parallel to the door and contained 4 pcs 16 inches long. The third layer (and fourth layer if present) was loaded flat, perpendicular to the door and contained 3 pcs 16 inches long. The majority of the pieces in each rick were in the second layer which had an approximate 0.5-1.0" space between pieces. (The loading directions indicate the direction of the longest dimension on each piece relative to the loading door opening.) Each pre burn/warm up fuel charge normally weighs within the weight range allowed for the actual test fuel charge

WOODSTOVE OPERATING DATA
WOODSTOVE DATA SHEET #9A-2

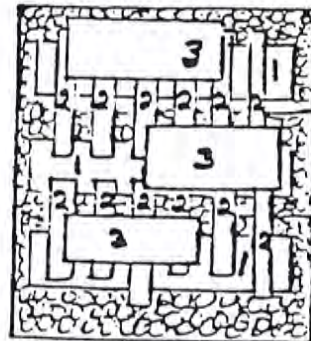
Unit: HIGH VALUE X-1EC
Run # REPA E.2
Date 3/21/99
Technician ATH, RLS.
Page 2 of 3
WST7-Form2-A, Rev 6/90

Warm up Information (cont.):

Each warm up/preburn fuel charge was ricked in exactly (as much as possible) the same manner and the weight of each rick was usually within the allowable weight range for the test fuel charge. The physical arrangement and alignment of each rick was designed to accomplish three (3) things: (1) The bottom layer was nestled firmly into the coal bed and was as close to being level with the bottom of the stove as possible, thus providing a stable loading platform for the rest of the rick, keeping it in a ricked state (as opposed to a collapsed or fallen down state) until the rick reached the charcoal stage and sags or collapses of its own accord. (2) It enhances the flow of primary air through the ricked preburn fuel charge, for the primary air would flow through the spaces between the pieces in the first layer and then up through the spaces between the pieces in the second, third and, if present, fourth layers. (3) It maximized, as much as possible, the surface to volume ratio of each preburn fuel charge, thereby allowing the fire immediate access to as much wood surface as possible and, thereby, insuring uniform charcoalization. All three of these enhance combustion and so get the stove as hot as possible during the warm up period, thereby maximizing the amount of heat (BTU's) stored in the stove. The actual preburn was not started until the stove surface temperatures had maximized and stabilized, thus indicating that the amount of heat stored in the stove had peaked. For this stove, the thermal storage was monitored using the TOP surface temperature(s) and the peak value(s) obtained were 950 of.



Front View



Top View

The arrows indicate the direction of the air flow through the rick.

The primary air was adjusted to the run setting of 0.55" open 4.9 lbs above the upper charcoal bed weight.

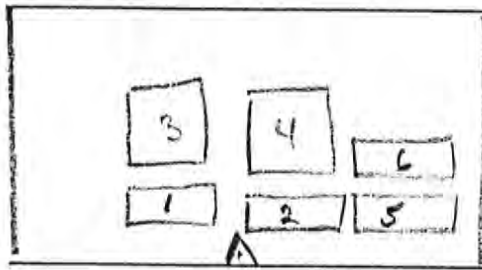
WOODSTOVE OPERATING DATA
WOODSTOVE DATA SHEET #9A-3

Unit HIGH VALLEY X-TE.
Run # EPA # 2
Date 3/21/99
Technician ATM, RLS.
Page 3 of 3
WST5-Form2-Rev11/89

Additional Comments: Test Start Sequence: ① Turned Fan OFF
② Opened Primary Air Control Wide Open ③ Opened door
④ Loaded test fuel charge into the stove ⑤ Cleared
coals away from the front of LPAD ⑥ Photograph ⑦
Closed door.

Test Fuel Charge Loading Information:

Test Fuel Charge and Loading Sequence Diagram



FRONT of stove view
4 X 4's: 3, 4
2 X 4's: 1, 2, 5 & 6
Loading Sequence: 1, 2, 3, 4, 5 & 6 LAST
Driest Pcs in Load 1 & 2

Loaded the test fuel charge on an essentially level, medium
sized, Average coal bed (in appearance, color and temperature
for a Low (≤ 1.0 kg/hr) burn rate. Load 1:30 - had trouble getting
pc 6 in. Ignition N 1:00. Secondaries igniting @ 2:00
2nd Tube igniting @ 3:00 5:00 Flames ↓
Out of Balance @ 6:15. Back in Balance @ 8:24 Out
again @ 11:40 Back in 17:02 Out 17:10 In 19:20
then out In/out again @ 19:51 In 20:53.
The whole time had VC to baffle w/ secondaries on
do p of VC.

FUEL MOISTURE
WOODSTOVE TEST DATA SHEET #10

Unit: HIGH VALLEY X-TEC
Run: EPA #2
Date: 3/21/99
Technician: ATM, PLS.
WST1-Form7-Rev11/89

Room Temperature: 60 °F

Correction Factor: +1

NOTE: Record readings to the nearest 0.5% moisture
Uncor Values are corrected for temperature: Yes No
Time Test Fuel Moisture Readings taken at: 1130
Calibration Checks: X Y 12.0 12.0 22.0 22.3

Pc #	Dimen	Use	Top		Bottom		Side		Piece Avg Corrected
			Uncor	Cor	Uncor	Cor	Uncor	Cor	
1	2x4x8'	K	12.0	12.8	12.0	12.8	12.0	12.8	12.800
2									
3									
4	2x4x8'	P	20.5	22.0	22	23.7	21.5	23.1	22.933
5	"	P	20.5	22.0	22	23.7	20	21.4	22.367
6	"	P	18.5	19.8	19.5	20.9	21	22.6	21.100
7	"	P	19	20.3	20.5	22.0	19.5	20.9	21.067
8	"	P	22.5	24.3	23	24.9	20.5	22.0	23.733
9									(111.200)
10									
11	2x4x17 1/8	T	18.0	19.2	18.0	19.2	18.0	19.2	19.200
12	"	T	19.0	20.3	19.0	20.3	20.0	21.4	20.667
13	"	T	20	21.4	20	21.4	20.5	22.0	21.600
14	"	↓ T	21	22.6	22	23.7	22.5	24.3	23.533
15									
16	4x4x17 1/8	T	19	20.3	19.5	20.9	20	21.4	20.867
17	"	↓ T	21	22.6	20	21.4	22	23.7	22.567
18									(128.434)
19	FEET	T	19	20.3	19	20.3	19.5	20.9	20.500
20									OUT SPACES

	Kindling	Pretest Fuel	Test Load
% Moisture - Dry Basis:	12.800% ✓	22.240% ✓	21.406% ✓
% Moisture - Wet Basis:	11.348% ✓	18.194% ✓	17.632% ✓

To obtain Wet from Dry: $\frac{100 \times \% \text{ Dry Rdg.}}{100 + \% \text{ Dry Rdg.}} = \% \text{ Moisture, Wet Basis}$

Acceptable Ranges: 16-20% wet; 19-25% dry
(17.5 - 22.5 on Meter [Uncor reading] at 70°F)

Key for Use: K= Kindling P= Pretest Fuel T= Test Fuel

WOOD DENSITY DETERMINATION
WOODSTOVE TEST DATA SHEET #11

Unit: HIGH VALLEY X-TEC
Run#: EPA # 2
Date: 3/21/99
Technician: ATM, PLS.
WST2 form 11-Rev 6/90

Wood Piece: Nominal Dimensions: 3 1/2" x 3 1/2" x 1 1/2"
Depth (D): in 1.557 cm 3.9547 ✓
Width (W): in 3.548 cm 9.0119 ✓
Length (L): 2.995 cm in
2.838 cm
2.997 cm
3.031 cm
Length \bar{X} = in 2.9653 cm 7.5317 ✓
Volume: 268.425 cm³ ✓
(D X W X L)

MOISTURE: Room Temperature: 70 °F Correction Factor: —
Uncorrected Meter Readings Corrected for temperature: Yes No

NOTE: Record moisture meter readings to the nearest 0.5%

	Uncor	Cor	%
Top:	19.0	20.3	%
Bottom:	18.5	19.8	%
Side:	18.5	19.8	%
\bar{X} :		19.967	%

Avg % Moisture (Dry) 19.967 % ✓
Avg % Moisture (Wet) 16.644 % ✓
Scale: Leveled In Out
Zeroed: In Out

Wet Weight: 149.0 g Dry Weight: 117.0 g

% Moisture Dried Basis: 21.147 % ✓
[1 - (Dry Wt ÷ Wet Wt)] X 100

Into Dryer Date 3/21/98 Time 1325 Temp 220 °F
Out of Dryer Date 3/29/99 Time 1415 Temp 218 °F
(Minimum Time in Dryer: 24 hrs.) Minimum Dryer Temp 100°C (212°F)

Density = $\frac{117.0}{(\text{dry wt})} \text{ g} \div \frac{268.425}{(\text{volume})} \text{ cm}^3 = 0.4359 \text{ g/cm}^3$ ✓

Pellet Fuel Moisture Content Determination

Tare Beaker Wt. _____ g
Wet Wt: _____ g - _____ g = _____ g
Gross Wet Wt. Tare Beaker Wt. Net Wet Wt.
Dry Wt: _____ g - _____ g = _____ g
Gross Dry Wt. Tare Beaker Wt. Net Dry Wt.
% Moisture Dried Basis: _____ %
[1 - (Net Dry Wt ÷ Net Wet Wt.)] X 100

ENO WT. 609.1 lbs

Minute Time	Scale Wt	lbs Left	Burn Rate	CO ₂		O ₂		Tel	CO		T/C(1)/T/C(2)		T/C(3)		SO ₂ v.	PPM	Static Press.	Comments
				v.	%CO ₂	v.	%O ₂		v.	%CO	Bal	Wet Bulb	Dry Bulb	% H ₂ O				
240	1410	611.0	1.9	0	223	5.57	55.3	13.86	33.7	1.71	3.3	78	101	2.4	98	186	-034	Flow
245	13	610.9	1.8	1	216	5.39	56.1	14.06	31.6	1.58	3.4	78	101	2.4	97	185	-034	SO ₂ 1.5
250	20	610.8	1.7	1	216	5.39	56.1	14.06	32.2	1.61	3.3	78	100	2.5	96	183	-033	CO ₂ 1.5
255	25	610.8	1.7	0	215	5.38	56.4	14.13	30.4	1.53	3.5	78	100	2.5	95	182	-033	O ₂ 1.5
260	30	610.7	1.6	1	216	5.39	56.4	14.13	31.7	1.61	3.4	78	100	2.5	94	180	-033	CO 1.5
265	35	610.6	1.5	1	218	5.44	55.1	14.06	31.5	1.59	3.4	78	99	2.6	94	180	-032	
270	40	610.6	1.5	0	219	5.47	55.8	13.98	32.5	1.61	3.4	77	99	2.4	94	180	-032	
275	45	610.5	1.4	1	214	5.34	56.6	14.18	30.3	1.53	3.5	78	99	2.6	95	178	-033	
280	50	610.4	1.3	1	213	5.32	56.2	14.21	31.4	1.57	3.4	77	99	2.4	95	178	-032	
285	55	610.3	1.2	1	204	5.10	57.6	14.44	32.5	1.64	3.1	77	99	2.4	95	176	-031	
290	2000	610.3	1.2	0	204	5.10	57.5	14.41	33.7	1.69	3.0	76	98	2.3	94	176	-031	
295	05	610.2	1.1	1	203	5.07	57.8	14.49	30.7	1.56	3.3	77	98	2.3	94	175	-030	
300	2010	610.1	1.0	1	202	5.05	57.8	14.49	32.4	1.64	3.1	77	98	2.3	93	173	-030	Flow
305	15	610.1	1.0	0	202	5.05	57.5	14.41	33.4	1.68	3.0	77	98	2.3	92	172	-030	SO ₂ 1.5
310	20	610.0	.9	1	192	4.80	58.6	14.69	34.2	1.71	2.8	77	97	2.4	92	172	-029	CO ₂ 1.5
315	25	609.9	.8	1	190	4.75	58.7	14.71	34.9	1.77	2.7	77	97	2.4	92	171	-029	O ₂ 1.5
320	30	609.8	.7	1	214	5.34	57.6	14.44	31.6	1.68	3.2	77	97	2.4	92	170	-029	CO 1.5
325	35	609.8	.7	0	199	4.97	58.3	14.61	33.7	1.70	2.9	77	97	2.4	92	170	-029	Cooler Fell
330	40	609.7	.6	1	188	4.70	59.3	14.86	33.4	1.70	2.8	77	97	2.4	92	169	-029	Cooler Fell
335	45	609.7	.6	0	187	4.67	59.2	14.84	33.8	1.69	2.8	77	97	2.4	92	168	-028	
340	50	609.6	.5	1	189	4.72	59.1	14.81	33.5	1.71	2.8	77	96	2.4	92	167	-028	
345	55	609.6	.5	0	191	4.77	59.6	14.94	29.6	1.51	3.3	77	96	2.4	91	165	-028	
350	2100	609.5	.4	1	190	4.75	59.9	15.01	28.1	1.44	3.3	77	96	2.4	91	165	-027	
355	05	609.5	.4	0	182	4.55	60.4	15.14	30.3	1.53	3.0	77	96	2.4	91	164	-027	
																	-027	(2026)
																	-027	(4185)

Pre Burn
47 lbs. 613.6 lbs.
Test Stack wt. Range
609.1 - 608.2 lbs.

PRE BURN DATA
RECORD SHEET #13
WST2-Form16

BAPD
PRE-BURN
28.50 Hg

Unit: HIGH VALLEY X-TEC Date: 3/21/99
Technician(s): ATM, PLS.
Page: 1 of 1

Hot Box On ✓

Minute Time	Scale Weight	Burn Rate	Stack	Stove Top	Left Side	Back	Right Side	Bottom	Firebox	2nd Burn Catalytic	Room Temp	Static	Comments
0 15	613.6	0	589	845	592	682	617	546	981	1455	77	-090	Primary Air Set at 0.55"
5 25	612.5	1.1	480	798	597	618	625	555	906	1361	76	-083	Secondary Air Set at 1" X3"
10 30	611.9	.6	434	723	587	570	623	556	874	1374	76	-078	Fan: ON HIGH
15 35	611.3	.6	412	688	574	540	618	552	857	1383	74	-075	TUNNEL ON AT: 1347
20 40	610.8	.5	385	645	562	518	611	542	846	1377	73	-074	Buckets Iced
25 45	610.4	.4	362	602	552	503	600	532	841	1308	72	-070	ANALYZERS SPANNED ✓
30 50	610.2	.2	337	562	544	492	589	524	836	1186	72	-064	Pumps turned on at: 1430
35 55	610.0	.2	314	520	531	488	572	515	828	1074	72	-059	AT
40 1400	610.0	0	295	474	511	482	565	506	820	1028	71	-055	508.6
45 05	609.9	.1	285	453	494	475	556	500	813	1005	71	-054	Check WB/DB: 76/98
50 10	609.9	0	274	431	491	464	547	495	802	943	72	-050	5 Raked Coals to 81.5 MPD
55 15	609.8	.1	266	413	478	455	537	491	788	1125	73	-050	Probe IN TUNNEL ✓
60 1420	609.8	0	259	404	464	440	525	484	770	1053	72	-049	463.4
65 25	609.8	0	253	393	452	427	513	476	754	987	71	-046	452.2
70 30	609.7	.1	246	404	441	414	500	470	738	938	71	-047	
75 35	609.7	0	242	390	432	404	490	466	721	923	70	-048	assemble VC
80 40	609.6	.1	236	363	424	395	479	463	644	915	70	-046	to 60.1 lb.
85 45	609.6	0	231	355	418	387	470	460	627	878	70	-045	Removed 0.3 lbs
90 50	609.3	.0	230	347	410	380	461	459	614	914	70	-044	411.4
95 55	609.2	.1	224	343	403	373	454	457	602	870	70	-044	406.0
100 1500	609.2	.0	221	340	396	365	446	454	590	846	69	-043	400.2
105 05	609.2	0	218	336	390	357	439	451	579	839	69	-042	394.6
110 10	609.1	.1	217	333	388	352	435	449	572	832	69	-041	391.4

Unit: HIGH VALLEY X-TEC Date: 3/21/99
 Run: EPA #2 Technician(s): ATM, PLS.
 Page: 1 of 4

T/C#	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
Minute	Stove Top	Left Side	Back	Right Side	Bottom	Firebox	2nd Burn	Room Temp	Tunnel	C. Gas Box	Impinger Out	5G-1 Filter	5G-1 Condenser	Com. der	On/Off
0	333	386	352	435	449	572	832	69	88	251	40	79	53	244	769
5	421	380	336	417	438	556	1117	71	192	255	41	84	38	244	629
10	427	374	316	406	439	544	1221	70	100	258	41	85	38	244	630
15	417	368	303	394	438	531	1190	70	96	260	40	84	38	244	617
20	441	360	293	383	434	525	1221	70	97	254	41	84	38	244	645
25	495	359	287	380	430	524	1250	70	98	251	42	84	38	243	656
30	533	357	283	380	428	526	1228	70	99	249	41	84	37	243	685
35	575	361	273	384	426	535	1243	70	100	248	41	84	39	244	719
40	584	366	268	388	424	544	1221	70	100	247	42	84	38	244	737
45	575	374	266	391	421	553	1237	71	99	246	41	85	38	244	774
50	558	382	266	396	419	560	1291	71	99	246	41	85	38	244	795
55	545	390	268	404	418	567	1272	70	99	245	41	85	38	244	806
60	590	449	251	478	516	653	1437	84							
65	550	395	272	414	416	575	1249	70	100	245	41	86	38	244	811
70	550	398	274	420	416	578	1190	71	100	245	41	86	38	244	803
75	558	396	279	431	414	584	1216	71	100	244	42	86	38	244	827
80	552	397	285	442	413	588	1218	71	100	244	43	86	38	244	832
85	541	399	292	454	413	594	1216	71	99	244	40	86	38	244	847
90	527	400	300	464	413	597	1247	71	99	244	40	87	38	243	906
95	516	405	308	469	414	601	1231	71	97	243	41	86	38	244	905
100	486	414	323	472	413	604	1229	72	96	243	41	86	38	244	914
105	471	416	331	473	413	606	1214	73	94	242	42	86	38	242	953
110	454	415	339	472	413	607	1172	72	94	241	42	86	38	242	984
115	429	410	349	471	414	607	1135	72	92	240	42	85	38	243	860
120	613	485	368	545	496	604	1046	73	91	239	42	85	38	242	878
125	611	484	368	545	496	604	1435	85							
130	611	484	368	545	496	604	1435	85							
135	611	484	368	545	496	604	1435	85							
140	611	484	368	545	496	604	1435	85							
145	611	484	368	545	496	604	1435	85							
150	611	484	368	545	496	604	1435	85							
155	611	484	368	545	496	604	1435	85							
160	611	484	368	545	496	604	1435	85							
165	611	484	368	545	496	604	1435	85							
170	611	484	368	545	496	604	1435	85							
175	611	484	368	545	496	604	1435	85							
180	611	484	368	545	496	604	1435	85							
185	611	484	368	545	496	604	1435	85							
190	611	484	368	545	496	604	1435	85							
195	611	484	368	545	496	604	1435	85							
200	611	484	368	545	496	604	1435	85							

Site: HIGH VALLEY X-TEC Date: 3/21/99
 Unit: EPA #2 Technician(s): ATM, RLS,
 Page: 2 of 4

T/C#	Minute Time	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
		Stove Top	Left Side	Back	Right Side	Bottom	Firebox	2nd Burn	Room Temp	Tunnel	C. Gas Box	Impinger Out	5G-1 Filter	5G-1 Condenser	Com- Bar	
120	110	408	404	355	468	418	600	477	72	91	238	41	85	38	242	
125	15	387	396	360	465	421	591	912	73	89	237	40	84	38	242	
130	20	381	396	361	463	422	588	902	73	89	236	40	84	39	242	
135	25	367	391	361	459	424	581	883	73	88	235	40	83	39	241	
140	30	358	386	363	456	425	574	874	73	87	235	40	83	39	242	
145	35	350	382	364	454	426	568	866	72	87	234	40	83	39	241	
150	40	341	379	366	451	427	562	852	73	86	233	40	82	39	241	
155	45	335	376	368	449	428	558	838	73	85	233	39	82	39	241	
160	50	329	372	370	445	429	552	827	73	85	234	39	82	39	241	
165	55	323	369	370	442	429	547	817	72	84	234	39	81	39	241	
170	100	319	366	369	439	430	542	812	72	84	235	39	81	39	241	
175	65	315	362	369	435	430	536	802	72	84	235	39	80	39	241	
180	180	310	358	368	432	430	530	794	72	83	235	39	80	39	241	AT
185	15	307	356	367	429	430	524	782	72	83	235	39	80	39	240	3716
190	20	304	351	367	426	429	519	776	71	82	235	40	79	38	240	
195	25	301	348	368	424	427	514	774	71	82	235	40	79	38	240	
200	30	298	345	368	423	426	509	771	71	81	234	40	79	39	241	
205	35	297	344	368	422	425	506	770	72	81	234	40	79	39	240	
210	40	296	340	367	422	423	503	768	71	81	234	40	78	39	239	3712
215	45	294	339	368	421	421	499	757	71	81	234	40	78	39	239	
220	50	292	336	369	420	420	495	752	71	80	234	40	78	39	239	
225	55	291	332	370	420	419	490	752	70	81	234	40	78	39	239	
230	100	289	332	370	420	418	487	747	70	80	234	40	77	39	240	
235	65	288	330	371	419	417	484	742	70	80	233	40	77	39	240	
240	110	3567	4111	447	5078	5085	6059	9187	852	80						
245	115	7780	8692	8790	10504	10194	12858	19549	1723	80						

T/C#	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
Minute	Stove Top	Left Side	Back	Right Side	Bottom	Firebox	2nd Burn	Room Temp	Tunnel	C. Gas Box	Impinger Out	5G-1 Filter	5G-1 Condenser	Con- dar	
240	286	327	372	419	416	479	730	70	80	233	40	77	39	240	
245	283	326	372	417	414	472	715	71	80	233	40	76	39	239	
250	281	328	371	415	412	468	710	70	80	233	40	76	39	240	
255	278	320	370	412	410	464	712	71	80	233	40	76	39	239	
260	276	318	370	409	408	462	710	71	80	232	40	76	39	239	
265	275	317	371	407	408	459	709	71	80	233	40	76	39	238	
270	273	316	373	404	407	452	705	70	80	232	40	76	39	238	
275	272	314	376	402	406	454	698	71	80	232	40	76	39	237	
280	270	313	375	399	404	451	696	71	80	232	40	76	39	238	
285	269	312	376	397	402	447	694	70	80	232	40	76	39	238	
290	267	311	375	395	400	445	690	71	80	232	40	76	39	239	
295	266	309	375	393	398	442	687	71	80	232	40	76	39	239	
300	265	308	376	391	395	5502	8456	848	80	233	40	76	39	238	
305	264	306	377	389	393	438	683	71	80	233	40	76	39	239	
310	262	304	376	387	391	436	681	71	81	233	40	76	39	239	
315	261	303	375	386	388	432	674	71	81	232	40	76	39	238	
320	259	299	374	384	384	428	671	71	81	233	41	76	39	238	
325	258	297	376	383	380	423	681	71	81	233	41	76	40	239	
330	257	296	375	382	376	420	676	71	80	233	41	76	40	239	
335	256	295	371	379	373	417	663	71	81	233	41	76	40	239	
340	254	291	367	375	370	415	655	71	81	233	41	76	40	239	
345	251	292	365	372	368	412	654	71	80	232	41	76	40	239	
350	251	290	363	368	366	410	651	71	80	232	41	76	40	238	
355	250	284	362	366	365	407	645	71	81	232	41	76	40	239	
360	248	281	358	362	365	405	639	71	81	233	42	76	40	239	
365	247	280	357	361	364	5043	7933	852	80	232	41	76	40	239	
370	246	279	356	360	363	5043	7933	852	80	232	41	76	40	239	
375	245	278	355	359	362	10513	16429	1700	81	233	42	76	40	239	

PRE AND POST TEST ZERO/SPAN CHECK
WOODSTOVE DATA SHEET #15-1

Site: Myren Consulting, Woodinville, WA Date: 3/31/99 Analyte: CO₂

Source: HIGH VALLEY X-TEC Run #: EPA # 2

Zero Cyl #: 36919 Conc. 00.0 % CO₂ Cyl Press: 250 psi

Certified by: CASCADE AIRGAS Date: 4/24/96

Span Cyl #: 250-1060 Conc. 6.0 % CO₂ Cyl Press: 1480 psi

Certified by: OXARC Date: 8/22/97

Analyzer: Make: Horiba Model: PIR-2000 SN: 607024

Range: 0 - 25.0% CO₂ Analyzer Output: 0 - 1.0 v.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter:

EPA Span Value = 25.0% CO₂

EPA Control Limits = + 2.5% of 25.0% CO₂ = + 0.625% CO₂

Pre Run Audit: By: ATM, PLS. Time: 1405 Temp: 69 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	00.0	.001	.0504	+0.0504	+0.20
Span	24.0	.240	6.0	23.5	.238	5.941	-0.0590	-0.98

Comments:

Post Run Audit: By: ATM, PLS. Time: 2210 Temp: 70 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	00.0	.000	.0256	+0.0256	+0.10
Span	24.0	.240	6.0	6.0	.242	6.040	+0.0404	+0.67

Comments:

+ Conc. Difference = Act % - Exp (Std) %

Zero % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$

Span % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

PRE AND POST TEST ZERO/SPAN CHECK
WOODSTOVE DATA SHEET #15-2

Site: Myren Consulting, Woodinville, WA Date: 3/21/99 Analyte: O₂

Source: HIGH VALLEY X-TEC Run #: EPA #2

Zero Cyl #: 36919 Conc. 00.0 % O₂ Cyl Press: 250 psi

Certified by: CASCADE AIRGAS Date: 4/24/96

Span Cyl #: 250-1060 Conc. 6.0 % O₂ Cyl Press: 1480 psi

Certified by: OKARC Date: 8/22/97

Analyzer: Make: Taylor Model: OA 137 SN: 137/4772

Range: 0 - 25.0% O₂ Analyzer Output: 0 - 100 mv.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter:

EPA Span Value = 25.0% O₂

EPA Control Limits = + 2.5% of 25.0% O₂ = + 0.625% O₂

Pre Run Audit: By: ATM, RLS Time: 1405 Temp: 69 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ%
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0	00.0	0.0155	-0.0155	-0.06
Span	6.0	24.0	6.0	6.0	23.9	5.9805	-0.01946	-0.32

Comments:

Post Run Audit: By: ATM, RLS Time: 2210 Temp.: 70 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ%
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	00.0	00.0	0.0155	-0.0155	-0.06
Span	6.0	24.0	6.0	6.0	24.0	6.0056	+0.0056	+0.09

Comments:

+ Conc. Difference = Act % - Exp (Std) %

Zero % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$

Span % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

PRE AND POST TEST ZERO/SPAN CHECK
WOODSTOVE DATA SHEET #15-3

Site: Myren Consulting, Woodinville, WA Date: 3/21/99 Analyte: CO

Source: HIGH VALLEY X-TEC Run #: EPA # 2

Zero Cyl #: 36919 Conc. 00.0 % CO Cyl Press: 250 psi

Certified by: CASCADE AIRGAS Date: 4/24/96

Span Cyl #: 250-1060 Conc. 1.26 % CO Cyl Press: 1450 psi

Certified by: OXARC Date: 8/22/97

Analyzer: Make: Infra Red Model: 702 D SN: 113

Range: 0 - 10.0% CO Analyzer Output: 0 - 100 mv.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter: _____

EPA Span Value = 5.0% CO

EPA Control Limits = +2.5% of 5.0% CO = + 0.125% CO

Pre Run Audit: By: ATH, RLS Time: 1405 Temp: 69 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	00.1	00.0	00.91	-0.0091	-0.18
Span	1.26	2.52	1.26	1.25	24.7	1.2317	-0.0283	-2.25

Comments:

Post Run Audit: By: ATH, RLS Time: 2210 Temp.: 70 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	00.0	00.1	00.40	-0.0040	-0.08
Span	1.26	2.52	1.26	1.26	24.9	1.2417	-0.0183	-1.45

Comments:

+ Conc. Difference = Act % - Exp (Std) %

Zero % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$

Span % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

QUALITY CHECKS
WOODSTOVE DATA SHEET #16

Ambient = Tr: _____ °F T/C#30: _____ °F

Thermocouple Check (at ambient): T/C#1: 61 °F; T/C#2: 60 °F;

T/C #3: 165 °F; T/C #4: 201 °F; T/C #5: 200 °F;

T/C #6: 185 °F; T/C #7: 176 °F; T/C #8: 161 °F;

T/C #9: 165 °F; T/C #10: 189 °F; T/C #11: 60 °F;

T/C #12: 60 °F; T/C #13: 60 °F; T/C #14: 49 °F;

T/C #15: 60 °F; T/C #16: 51 °F; T/C #17: 61 °F;

T/C #18: _____ °F; T/C #19: _____ °F; T/C #20: _____ °F;

T/C #21: _____ °F; T/C #22: _____ °F; T/C #23: _____ °F;

T/C #24: _____ °F; T/C #25: _____ °F; T/C #26: _____ °F;

Comments: Stove still warm from previous burning.

Thermocouple Readout: Pretest Zero/Span Check and Calibration:

Zero (0°F) : 000 °F Adj _____ Post Test Check Zero (0°F): 001 °F % Difference 10.05

Span (2000°F): 2000 °F Adj _____ Span (2000°F): 2000 °F 0

(Allowable % Difference = 1.5%. Use formulas on Woodstove Data Sheet #15 to calculate % Difference)

Thermocouple Readout Pretest Linearity Check

0°F = 000 °F; 200°F = 202 °F; 400°F = 399 °F;

600°F = 600 °F; 800°F = 800 °F; 1000°F = 1002 °F;

1200°F = 1201 °F; 1400°F = 1401 °F; 1600°F = 1600 °F

1800°F = 1799 °F; 2000°F = 2000 °F

Combustion Gas (CO₂, O₂, CO) Train Leak Check: Pre Post

Draft (Static) Gauge Zero Check: Pre Post

Scale Check Pre (Wt, #'s): 611.6 - 606.6 = 50/50 = OK ATM

Post (Wt, #'s): 613.5 - 608.8 = 50/50 = OK (ATM)

Stack cleaned prior to the run: Yes _____ No

Tunnel cleaned prior to the run: Yes _____ No

DILUTION TUNNEL CALCULATIONS
3/31/96

MYREN CONSULTING CERTIFICATION TEST DATA

File Name: hivalleyepa6

Stove Manufacturer: HI VALLEY

Model Number: XTEC

Lab Name: MYREN

Test Date: 3/30/99

Run Number: EPA 6

Meter Box Y Factor: 1.003

Barometric pressure (in): 28.394

Gas meter temp (ave): 81
delta H(ave): 0.898

Gas meter initial reading: 617.408

Gas meter final reading: 744.112

Front catch (acetone) mg: 5.7
first filter catch (mg): 9.9
second filter catch (mg): -2.8

tunnel flow (ave cfm): 140.471

Emission Rate(g/hr): 0.917

Emission Rate(M5H) : 1.694
vs/MmTs: 0.0126

vs ave: 849.843
Tunnel average temp (°f): 111.042

Test time(min): 230

Fuel Load(lb. wet): 17.4

Wood moisture(%wet): 17.234

Burn rate(dry kg/hr): 1.704

Samp vol(scf): 117.884

front filter number: 785

back filter number: 783

acetone beaker number: 6

PRELIMINARY RESULTS

FINAL RESULTS

AUDITED

XTEC

EPA 6

3/30/99

1.704

0.917

1.693873102

ADJ

RUN TIME (min)	PITOT DELTAP (- INCH H2O)	TNL TEMP (°F)	GAS METER RDG (ft3)	GAS METER TEMP (°F)	GAS METER DELTA H (in.H2O)	TUNNEL VELOCIT (ft/min)	PROP RATE (%)	dDGM vol std (ft3)
0	0.040	110	617.408	72	0.900	851.48		
10	0.036	141	622.301	73	0.900	829.46	94.7	4.623
20	0.040	142	627.795	74	0.900	875.06	109.2	5.181
30	0.040	141	633.275	77	0.890	874.33	102.5	5.138
40	0.040	137	638.701	78	0.890	871.42	100.7	5.078
50	0.040	133	644.041	79	0.890	868.49	98.6	4.989
60	0.039	130	649.691	80	0.900	855.40	103.9	5.269
70	0.040	124	655.204	81	0.890	861.88	101.7	5.131
80	0.040	117	660.785	82	0.900	856.70	100.8	5.185
90	0.040	113	666.365	81	0.890	853.72	100.9	5.194
100	0.040	109	671.831	82	0.900	850.74	98.3	5.078
110	0.040	106	677.382	83	0.900	848.49	99.4	5.148
120	0.040	104	682.946	82	0.900	846.99	99.6	5.160
130	0.040	102	688.505	83	0.900	845.49	99.3	5.155
140	0.040	101	694.105	83	0.900	844.74	100.1	5.193
150	0.040	99	699.635	83	0.900	843.23	98.5	5.128
160	0.040	98	705.165	83	0.900	842.47	98.5	5.128
170	0.040	97	710.738	83	0.900	841.72	99.2	5.168
180	0.040	96	716.315	83	0.900	840.96	99.2	5.172
190	0.040	95	721.859	83	0.900	840.21	98.5	5.141
200	0.040	94	727.425	83	0.900	839.45	98.8	5.162
210	0.040	93	732.995	83	0.900	838.69	98.8	5.165
220	0.040	92	738.549	84	0.900	837.93	98.2	5.141
230	0.040	91	744.112	83	0.900	837.17	98.5	5.159
240						0.00	0.0	0.000
250						0.00	0.0	0.000
260						0.00	0.0	0.000
270						0.00	0.0	0.000
280						0.00	0.0	0.000
290						0.00	0.0	0.000
300						0.00	0.0	0.000
310						0.00	0.0	0.000
320						0.00	0.0	0.000
330						0.00	0.0	0.000
340						0.00	0.0	0.000
350						0.00	0.0	0.000

DATA SUMMARY

MODEL :

RUN:

DATE:

DBR:

GPH UNADJ

ADJ

DATE 3/30/99

PAGE 1 OF 2

MODEL # XTEC

RUN # EPA 6

METER BOX # 511-M

METER Y 1.003

FILTER # (F) 785 (R) 78

PRE TEST LEAK RATE = .000 CFM @ -10.0 IN. HG, 143/143

FILTER SIZE: 110MM

POST TEST LEAK RATE = .0005 CFM @ -10.0 IN. HG, 124/1245

PROBE LENGTH 24" glass

TIME		METER READING CU.FT.	PITOT dp	TNL TEMP. (°F)	METER TEMP. (°F)	GAS. METER dh	VAC IN. Hg	VELOCITY TRAVERSE			
CLOCK	ELAPSED							POINT	LOCATION	ΔP	TEMP
1425	00	617.408	-040	110	72	.90	0	N-1	0.5"	.035	114
35	10	622.301	-036	141	73	.90	0	2	1.5"	.043	115
45	20	627.795	-040	142	74	.90	0	3	4.5"	.04	115
55	30	633.275	-040	141	77	.89	0	4	5.5"	.035	115
1505	40	638.701	-040	137	78	.89	0	W-1	0.5"	.035	116
15	50	644.041	-040	133	79	.89	0	2	1.5"	.043	116
25	60	649.691	-039	130	80	.90	0	3	4.5"	.04	116
35	70	655.204	-040	124	81	.89	0	④	5.5"	.035	115
45	80	660.785	-040	117	82	.90	0	Avg. .03825			115.25
55	90	666.365	-040	113	81	.89	0	Pilot Leak Check			575.25
1605	100	671.831	-040	109	82	.90	0	Pre <input checked="" type="checkbox"/> Post <input checked="" type="checkbox"/>			
15	10	677.382	-040	106	83	.90	0	Cp = .99			N
25	20	682.946	-040	104	82	.90	0				1
35	30	688.505	-040	102	83	.90	0				2
45	40	694.105	-040	101	83	.90	0				3
55	50	699.635	-040	99	83	.90	0				4
1705	60	705.165	-040	98	83	.90	0				
15	70	710.738	-040	97	83	.90	0				
25	80	716.315	-040	96	83	.90	0				
35	90	721.859	-040	95	83	.90	0				

→ W 1 2 3 4 (3/4)

*=point of Avg. delta p
 $Q_s = \left(\frac{\sqrt{(\Delta P \times BP)}}{T(^{\circ}R)} \right) \times 3167.2 =$
 137.706 cfm

BP = ~~Static~~ 28.43 in Hg ↓
 60 28.41
 120 28.39
 180 28.38
 240 28.36

X = 28.394

DATE 3/30/99

PAGE 2 OF 2

MODEL # XTEC

RUN # EPA6

METER BOX # 511-M

METER Y 1.003

FILTER # (F) 785 (R) 788

PRE-TEST LEAK RATE = 1.000 CFM @ -10.0 IN. HG. 143/143

FILTER SIZE: 110 MM

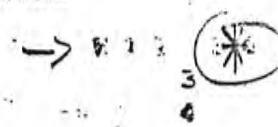
POST TEST LEAK RATE = 1.0005 CFM @ -10.0 IN. HG. 124/

PROBE LENGTH 24" g box

TIME		METER READING CU. FT.	PITOT dp	TNL TEMP. (°F)	METER TEMP. (°F)	GAS METER dh	VAC IN. Hg	VELOCITY TRAVERSE			
CLOCK	ELAPSED							POINT	LOCATION	ΔP	TEMP
1745	200	727.425	-040	94	83	.90	0	N-1	0.5"	<u>-035</u>	<u>114</u>
55	(10)	732.995	-040	93	83	.90	0	2	1.5"	<u>-043</u>	<u>115</u>
1805	20	738.549	-040	92	84	.90	0	3	4.5"	<u>-040</u>	<u>115</u>
15	30	744.112	-040	91	83	.90	0	4	5.5"	<u>-035</u>	<u>115</u>
	40							W-1	0.5"	<u>-035</u>	<u>116</u>
	50							2	1.5"	<u>-043</u>	<u>116</u>
	60							3	4.5"	<u>-040</u>	<u>116</u>
	70							4	5.5"	<u>-035</u>	<u>115</u>
	80									<u>03825</u>	<u>115.25</u>
	90										<u>575.2</u>
	00										
	10										
	20										
	30										
	40										
	50										
	60										
	70										
	80										
	90										

Pre Post

Cp = 0.99



*-point of Avg. delta P

$$Q_s = \left(\frac{\sqrt{(\Delta P \times EF)}}{T(^{\circ}R)} \right) \times 3167.2$$

137.706 cfm

BP = ~~28.43~~ 28.43 in Hg
 60 28.41
 120 28.39
 180 28.38
 230 28.35

X = 28.394

WOODSTOVE DATA SHEET #4-1: INITIAL FILTER WEIGHTS (TARE WEIGHTS)

Into Dessicator: Date 1/3/99 Time 12:00 By ATM Front Half Back Half

Manufacturer: Schleich & Schuell Size: 11cm Lot No.: ZP 95.1 Grade: #25 g/loss
 Order No. 06220

Filter #	First Wt	Date	Time	By	Second Wt	Date	Time	By	Third Wt	Date	Time	By
776	.7853	2/7/99	12:55	T.M.	.7853	2/10/99	1629	ATM				
777	.8127		12:56	T.M.	.8129		1628	ATM				
778	.8044		12:57	T.M.	.8040		1627	ATM				
779	.8036		12:58	T.M.	.8034		1626	ATM				
780	.7889		12:59	T.M.	.7888		1625	ATM				
781	.7894		1:00	T.M.	.7892		1625	ATM				
782	.7905		1:01	T.M.	.7903		1624	ATM				
783	.7967		1:02	T.M.	.7968		1623	ATM	←			
784	.8120		1:03	T.M.	.8118		1622	ATM				
785	.8166		1:04	T.M.	.8164		1621	ATM	←			
786	.7925		1:05	T.M.	.7923		1620	ATM				
787	.8064		1:06	T.M.	.8064		1619	ATM				
788	.7928		1:07	T.M.	.7926		1619	ATM				
789	.7774		1:08	T.M.	.7774		1618	ATM				
790	.7835		1:09	T.M.	.7835		1617	ATM				
791	.7981		1:10	T.M.	.7982		1616	ATM				
792	.8036		1:11	T.M.	.8035		1615	ATM				
793	.8116		1:12	T.M.	.8116		1614	ATM				
794	.8025		1:13	T.M.	.8024		1613	ATM				
795	.7766		1:14	T.M.	.7765		1613	ATM				
796	.7916		1:15	T.M.	.7915		1612	ATM				
797	.7755		1:16	T.M.	.7756		1611	ATM				
798	.8133		1:17	T.M.	.8133		1610	ATM				
799	.7949		1:18	T.M.	.7948		1610	ATM				
800	.8266	✓	1:19	T.M.	.8266	✓	1609	ATM				

←
-TORN
←

Checked by Jane [Signature]

Date: 2/21/99 Time 1405

QA REWEIGH

Filter #	WT	Date	Time	By
781	.7891	2/21/99	1412	Jm
789	.7772	2/21/99	1414	Jm
795	.7765	2/21/99	1415	Jm

BALANCE ROOM ENVIRONMENTAL CONDITIONS

WB	DB	%RH	Date	Time	By
62	76	45	2/21/99	1235	ATM
63	72	45	2/21/99	1300	ATM
65	80	44	2/21/99	1312	ATM

Post Weighing Second Scale Check
 0.0000 0.0010 0.0000 0.0000
 1.0000 1.0001 1.0000 1.0001

WOODSTOVE DATA SHEET #4-2:
INITIAL BEAKER WEIGHTS (TARE WEIGHTS)

Into Dessicator: Date: 1/4/99 Time: 1600 By: A.T.M. (9)

Beaker #	First Wt	Date	Time	By	Second Wt	Date	Time	By	Third Wt	Date	Time	By
1	65.4840	2/1/99	915	ATM	65.4838	2/3/99	1605	Jm				
2	66.1516		917	ATM	65.1515	2/3	1606	Jm				
3	67.8577		919	ATM	67.8571	2/3	1607	Jm	67.8571	2/7/99	1245	ATM
4	67.5891		920	ATM	67.5886	2/3	1612	Jm				
5	Broken											
6	67.4282		921	ATM	67.4282	2/3	1615	Jm				
7	65.5451		922	ATM	65.5453	2/3	1617	Jm				
8	60.0213		923	ATM	60.0213	2/3	1618	Jm	←	Blank		
9	66.9293		924	ATM	66.9294	2/3	1620	Jm				
10	66.0888		926	ATM	66.0885	2/3	1621	Jm				
11	65.6997		927	ATM	65.7015	2/3	1623	Jm	65.7016	2/7/99	1247	ATM
12	56.0653		928	ATM	56.0652	2/3	1625	Jm				
13	57.8945		929	ATM	57.8942	2/3	1627	Jm				

Checked By: A.T.M. (9) Date: 2/8/99 Time: 1705

QA REWEIGH

Beaker #	WT	Date	Time	By

BALANCE ROOM ENVIRONMENTAL CONDITIONS

WB	DB	%RH	Date	Time	By
55	69	39	2/1/99	0910	ATM
63	76	48	2/3/99	1555	ATM
62	76	45	2/7/99	1235	ATM

WOODSTOVE DATA SHEET #4-J: CONSTANT FINAL WEIGHTS

WST5-Form9, Pg1, Rev4/90
Unit Hi Valley Y TEC
Run # 4/20/99
Date: 4/20/99

Blank
3/13/99

Acetone Blank - 100 ml Acetone

Beaker #	Into Dessic	Date	Time	By	First	Date	Time	By	Second	Date	Time	By	Third	Date	Time	By
B	✓	3/18/99	0854	AM	66.0215	3/2/99	2237	ATM	66.0215	3/20/99	1832	ATM				

FINAL FILTER WEIGHTS

Filter #	Into Dessic	Date	Time	By	First	Date	Time	By	Second	Date	Time	By	Third	Date	Time	By

QA REWEIGH: FINAL WEIGHTS

Date	Beaker #	Final Wt	By
Date	Filter #	Final WT	By

SCALE ROOM ENVIRONMENTAL CONDITIONS

Session	Date	Time	By	WB	DB	%RH
1	3/18	2140	ATM	68	84	43
2	3/20	1800	ATM	64	84	32
3						
4						
5						

SCALE ROOM ENVIRONMENTAL CONDITIONS

Session	Date	Time	By	WB	DB	%RH
6						
7						
8						
9						
Comments						

WOODSTOVE DATA SHEET #4-4
SCALE QA SHEET

Scale Mettler
Model AE100
SN K04827

Dates From 1/9/99

Through _____

Level	Recalibrated	100g Weight	10g Weight	1.0g Weight	100mg Weight	20mg Weight	Date	Time	Tech	Wet Bulb	Dry Bulb	% RH
✓	Yes P.O.	99.9999	10.0001	1.0002	.1003	.0203	1/9/99	1243	ATM	58	70	48
✓	No	100.0002	10.0000	1.0000	.1000	.0200	1/14/99	1113	ATM	62	75	47
✓	Yes P.O.	99.9995	10.0002	1.0000	.0999	.0201	1/23/99	1100	ATM	63	77	43
✓	Yes	99.9999	10.0000	1.0000	.1000	.0201	1/24/99	1318	ATM	59	74	43
✓	Yes	99.9996	10.0002	1.0000	.1000	.0200	2/1/99	0910	ATM	55	69	39
✓	Yes	99.9997	10.0001	1.0001	.1002	.0201	2/2/99	0939	ATM	60	73	46
✓	Yes	99.9999	10.0001	1.0001	.1001	.0201	2/3/99	1555	ATM	63	76	48
✓	Yes	99.9999	10.0000	1.0001	.1001	.0201	2/7/99	1235	ATM	62	76	45
✓	Yes	99.9998	10.0000	1.0000	.1000	.0200	2/10/99	1600	ATM	63	77	45
✓	Yes	99.9998	10.0000	1.0001	.1000	.0200	2/19/99	0246	ATM	64	78	46
✓	No	99.9999	10.0000	1.0000	.1000	.0200	2/21/99	1312	ATM	65	80	44
✓	No	99.9997	10.0000	1.0001	.1000	.0200	3/5/99	1935	ATM	64	80	41
✓	Yes P.M.	99.9997	10.0000	1.0000	.1001	.0200	3/6/99	1135	ATM	64	80	43
✓	Yes	99.9947	10.0000	1.0001	.1000	.0200	3/13/99	1526	ATM	65	80	44
✓	Yes	99.9999	10.0001	1.0001	.1001	.0200	3/14/99	1355	ATM	63	78	43
✓	No	100.0001	10.0000	1.0000	.1000	.0200	3/15/99	1622	ATM	66	81	45
✓	Yes	99.9997	10.0000	1.0001	.1000	.0200	3/16/99	0025	ATM	65	82	09
✓	Yes	99.9996	10.0000	1.0001	.1001	.0200	3/17/99	1615	ATM	63	77	44
✓	Yes	99.9997	10.0000	1.0001	.1000	.0200	3/18/99	2140	ATM	68	84	43
✓	Yes	99.9998	10.0000	1.0000	.1000	.0200	3/20/99	1300	ATM	64	84	37
✓	Yes	99.9999	10.0000	1.0001	.1001	.0201	3/21/99	2215	ATM	61	74	47
✓	Yes	99.9997	10.0000	1.0000	.1001	.0200	3/22/99	0127	ATM	65	85	33
✓	Yes	99.9997	10.0000	1.0001	.1000	.0200	3/23/99	1115	ATM	69	84	41
✓	Yes	99.9997	10.0000	1.0002	.1001	.0201	3/24/99	1120	ATM	77	89	43
✓	Yes	99.9999	10.0000	1.0002	.1001	.0201	3/29/99	2038	ATM	69	72	45
✓	No	99.9999	10.0002	1.0002	.1001	.0202	3/30/99	0610	ATM	66	80	47
✓	No	99.9999	10.0000	1.0000	.1001	.0201	3/31/99	1000	ATM	64	80	41
✓	No	99.9996	10.0000	1.0000	.1001	.0201	4/3/99	1730	ATM	64	80	41
✓	Yes	99.9997	10.0001	1.0001	.1001	.0201	4/6/99	1030	ATM	61	75	44
QC Services	Audit	4/6/97	Scale checked	- wt.	Scale checked	- wt.						
✓	No	100.0003	10.0001	1.0001	.1001	.0201	4/6/99	1730	ATM			
✓	Yes	99.9999	10.0001	1.0001	.1001	.0200	4/7/99	1724	ATM	65	85	33
✓	No	99.9996	10.0000	1.0001	.1001	.0201	4/8/99	1346	ATM	67	80	50
✓	Yes	99.9997	10.0000	1.0000	.1000	.0200	4/16/99	1230	ATM	66	87	42
✓	Yes	99.9997	10.0000	1.0000	.1000	.0200	4/17/99	1625	ATM	68	89	43

Woodstove Particulate
Catch Processing Sheet
Woodstove Data Sheet #5
EPA M5G-1

Unit: High Valley XTSC
Run: EPA 6
Date: 3/30/99
Technicians: ATM
Revised 1/16/98-Data Sheet #5

Filters

Filter # (Front) 785 Beaker # 6 Final Wt. 67.4340g ✓
Final Wt. .8263g ✓ MI 50 Tare Wt. 67.4282g ✗
Tare Wt. .8164g ✗ Desc. Acetone Net Wt. .0058g ✓
Net Wt. .0099g ✓

Filter # (Rear) 783 Beaker # _____ Final Wt. _____ g
Final Wt. .7940g ✓ MI _____ Tare Wt. _____ g
Tare Wt. .7968g ✗ Desc. _____ Net Wt. _____ g
Net Wt. -.0028g ✓

Acetone Blank Calculation:

Blank Date: 3/13/99
Blank Beaker # 8 Final Wt. 66.0215 g
MI 100 Tare Wt. 66.0213 g
Desc. Acetone Net Wt. .0002 g
.0002 g ÷ 100 ml = .000002 g/ml

Blank Residue Value Calculation:

.000002 g/ml acetone X 50 ml acetone = .0001 g
Blank Residue Value

Total Particulate Catch Calculation

Filter: .0099g ✓
Filter: -.0028g ✓
Beakers: .0058g - .0001g = .0057g ✓
Total Catch Blank Residue Value
Total Catch = .0128g ✓

Unit HIGH VALLEY X-TRC
 Run # EPA #6
 Date 3/30/94
 Technician ATH, RLS,
 WST6-Form1, Rev8/96

MISCELLANEOUS TEST DATA
 WOODSTOVE DATA SHEET #8

Useable Firebox Dimensions: See QC Section Useable Volume: 2.713 ft³

Dilution Tunnel Draft (If applicable): Start 00.0 Stop 00.0

Test Chamber Air Velocity: Start: 00.0 Stop: 00.0 Avg: 00.0

Wet Bulb/ Start: WB: 64 °F DB: 75 °F 1.6 % Amb Moisture 54 %RH

Dry Bulb Stop: WB: 60 °F DB: 69 °F 1.45 % Amb Moisture 59 %RH

$\bar{X} = 1.5125$ % Ambient Moisture $\bar{X} = 56.5$ % Relative Humidity (RH)

Empty

Stove Wt: _____ lbs.

Empty

Stove Wt with Stack (Inc. Oil Seal) Wet: 607.6 lbs. Dry: 605.2 lbs.

Empty

Stove Wt with Stack and Ash Ash: 0 lbs. Total: 605.2 lbs.

Kindling Wt.

Paper: 0.7 lbs. Wood: 5.7 lbs.

Pre Burn Fuel Wt. 16.8 + 15.7 + 16.8 Total: 49.3 lbs. ✓

Total Kindling and Pre Burn Fuel Wt. ✓ ✓ 55.7 lbs. ✓

Coal Bed Wt-lbs: Range (4.3 - 3.5) 609.5 - 608.7 lbs. Actual: _____ lbs.

Allowable Amount of Charcoal that can be removed:

Coal Bed Wt. Range $\frac{4.35}{\text{Upper Wt.}} + \frac{3.48}{\text{Lower Wt.}} \times 12 \times .25 = \underline{0.9} lbs. ✓$

Test Fuel Wt-lbs: Ideal 19.0 lbs. Range: 17.1 - 20.8 lbs. Actual: 17.4 lbs. ✓

Test Fuel Size (pcs.) (.75 x 1.5 x 5" Flanges) 20 Pcs.

2 x 4's x 16⁷/₈" 4 Pcs 8.7 lbs. 50.00 % ✓

4 x 4's x 16⁷/₈" 2 Pcs 8.7 lbs. 50.00 % ✓

Est. Dry Burn Rate (Kg/Hr.) $\frac{17.4 - (17.4 \times .17234)}{2.2046} \times \frac{60}{230} = \underline{1.704} Est. Dry Burn Rate (Kg/Hr) ✓$

Est EPA Heat Output (HO_E) (19,140) x $\frac{63}{100} \times 1.704 = \underline{20,548} Est Heat Output (HO_E) BTU's/Hr ✓$

Comments:

Stove Operating Data
Woodstove Test Data Sheet #9
Cold Start

Unit: HIGH VALLEY X-TEC
Run: EPA #6
Date: 3/30/99
Technician(s): ATM PLS.
Data Sheet #9 - Rev 1/98-Pg.1

Fire Started: 0950 P.S.T.

Warm up and Preburn: Primary Air: Wide open from ignition until the start of preburn when the primary air control(s) was (were) adjusted to the run setting of 1 1/4". At the run setting until the start of the test.

Secondary Air: No Controls. Naturally drafted.

Secondary Burn/Cat Bypass: N/A

Charcoal Bed Preparation: Broke up, raked and leveled the coal bed prior to the addition of each warm up/pre burn fuel charge. Starting 1130 before the start of the test, broke up, raked and leveled the coal bed. In stove for 35 seconds.

Test: Door wide open during loading 1 min 11 sec, then closed

Primary Air: Wide open during the start of the test until 4:55. Adjusted to the run setting of 1 1/4" between 4:55 and 5:00. At the run setting of 1 1/4" open at 5:00 into the run.

Secondary Air: No Controls. Naturally drafted

Secondary Burn/Cat Bypass:

Fan: Off during warm up. On high during preburn. Off at the start of the test. Off for the 1st 30 minutes of the test.

Test Run Anomalies:

On high @ 30 mins into test. On high for the rest of the test.

↖ This run went faster than expected,

WOODSTOVE OPERATING DATA
 WOODSTOVE DATA SHEET #9A-1

Wood Data: Kindling: A mix of the below grades

	Size	Mill	Grade	Species
Pre Burn	<u>2x4</u>	<u>CANYON LBR.</u>	<u>STD. & BTR.</u>	<u>D. FIR, S. GRN.</u>
Test Fuel	<u>2x4</u>	<u>CANYON LBR.</u>	<u>#2 STD. & BTR.</u>	<u>D. FIR, S. GRN.</u>
	<u>4x4</u>	<u>STAND & 879</u>	<u>#2 STD. & BTR.</u>	<u>D. FIR, S. GRN.</u>

All grades WCLB Rules unless otherwise noted.

Warm up Information:

1st Warm up/Pre Burn Fuel charge (16.8 lbs) added at 10:12.
 2nd Warm up/Pre Burn Fuel charge (15.7 lbs) added at 11:15.
 3rd Warm up/Pre Burn Fuel charge (16.8 lbs) added at 12:35.
 4th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.
 5th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.
 6th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.
 7th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.
 8th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.

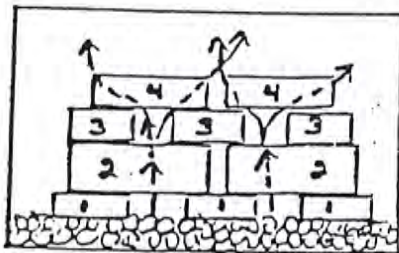
The coals were scooped out of the stove immediately prior to adding the 2.4 pre burn/warm up fuel charge. The stove lost 2.4 lbs. 3.0 lbs of coals were put back in after the scoop.

All pre burn/warm up fuel pieces were either 16 or _____ inches long. All preburn pieces/fuel charges were "ricked" in the stove. The pieces in the bottom layer in each rick contained 2 pcs that were 16 inches long and were loaded flat and perpendicular to the door. The pieces in the second layer in each rick were loaded on their side (edge) approximately parallel to the door and contained 4 pcs 16 inches long. The third layer (and fourth layer if present) was loaded flat, perpendicular to the door and contained 3 pcs 16 inches long. The majority of the pieces in each rick were in the second layer which had an approximate 0.5-1.0" space between pieces. (The loading directions indicate the direction of the longest dimension on each piece relative to the loading door opening.) Each pre burn/warm up fuel charge normally weighs within the weight range allowed for the actual test fuel charge

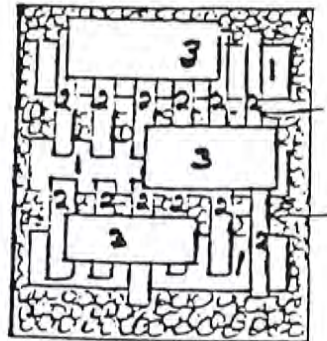
Warm up Information (cont.):

Each warm up/preburn fuel charge was ricked in exactly (as much as possible) the same manner and the weight of each rick was usually within the allowable weight range for the test fuel charge. The physical arrangement and alignment of each rick was designed to accomplish three (3) things: (1) The bottom layer was nestled firmly into the coal bed and was as close to being level with the bottom of the stove as possible, thus providing a stable loading platform for the rest of the rick, keeping it in a ricked state (as opposed to a col-lapsed or fallen down state) until the rick reached the charcoal stage and sags or collapses of its own accord. (2) It enhances the flow of primary air through the ricked preburn fuel charge, for the primary air would flow through the spaces between the pieces in the first layer and then up through the spaces between the pieces in the second, third and, if present, fourth layers. (3) It maximized, as much as possible, the surface to volume ratio of each preburn fuel charge, thereby allowing the fire immediate access to as much wood surface as possible and, thereby, insuring uniform charcoalization. All three of these enhance combustion and so get the stove as hot as possible during the warm up period, thereby maximizing the amount of heat (BTU's) stored in the stove. The actual preburn was not started until the stove surface temperatures had maximized and stabilized, thus indicating that the amount of heat stored in the stove had peaked. For this stove, the thermal storage was monitored using the TOP

surface temperature(s) and the peak value(s) obtained were 826 of.



Front View



Top View

The arrows indicate the direction of the air flow through the rick.

The primary air was adjusted to the run setting of 1 1/4" open 7.2 lbs above the upper charcoal bed weight.

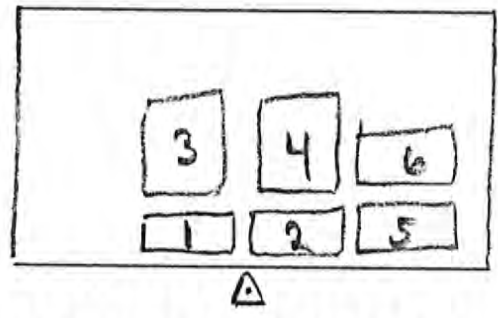
WOODSTOVE OPERATING DATA
WOODSTOVE DATA SHEET #9A-3

Unit HIGH VALLEY X-TEE
Run # EPA #6
Date 3/30/99
Technician ATH, JLS,
Page 3 of 3
WST5-Form2-Rev11/89

Additional Comments: Test Start Sequence: ① Turned fan off, ② Opened primary control wide open ③ Opened door ④ loaded fuel ⑤ cleared coals away from the LPAO ⑥ Photograph ⑦ Closed door,

Test Fuel Charge Loading Information:

Test Fuel Charge and Loading Sequence Diagram



FRONT of stove view
4 X 4's: 3 & 4
2 X 4's: 1, 2, 5 & 6
Loading Sequence: 1, 2, 3, 4, 5 & 6 last
Driest Pcs in Load 1 & 5

Loaded the test fuel charge on an essentially level, medium sized, hot coal bed (in appearance, color and temperature for a med high burn rate. Load 1111 Ignition NOISE Gas Balance by 2:30. Never lost balance. Good run. This run took off like a shot, And never slowed down, which is unusual with a falling barometer

FUEL MOISTURE
WOODSTOVE TEST DATA SHEET #10

Unit: HIGH VALLEY X-TEC
Run: EPA #6
Date: 3/30/99
Technician: ATM, PLS,
WST1-Form7-Rev11/89

Room Temperature: 50 °F

Correction Factor: +2

NOTE: Record readings to the nearest 0.5% moisture

Uncor Values are corrected for temperature: Yes No

Time Test Fuel Moisture Readings taken at: 1135

Calibration Checks: X Y 12.5 12.5 22.0 22.0

Pc #	Dimen	Use	Top		Bottom		Side		Piece Avg Corrected
			Uncor	Cor	Uncor	Cor	Uncor	Cor	
1	2x4x8'	K	14.5	15.4	15.0	15.9	14.5	15.4	15.567
2									
3	2x4x8'	P	21.5	23.1	22.0	23.7	22	23.7	23.500
4	"	P	22.5	24.3	23.0	24.9	22	23.7	24.300
5	"	P	21.5	23.1	21	22.6	20	21.4	22.367
6	"	P	18	19.2	19	20.3	19.5	20.9	20.133
7	"	P	19	20.3	22	23.7	20	21.4	21.800
8	"	P	20	21.4	19	20.3	20	21.4	21.033
9									133.133
10	2x4x16 1/2	T	20	21.4	20	21.4	19.5	20.9	21.233
11	"	T	18	19.2	18.5	19.8	18.5	19.8	19.600
12	"	T	18	19.2	18	19.2	18	19.2	19.200
13	"	T	21	22.6	22.5	24.3	21.5	23.1	23.333
14									
15	4x4x16 1/2	T	20.0	21.4	20.0	21.4	20.0	21.4	21.400
16	"	T	18.5	19.8	19.5	20.9	18.5	19.8	20.167
17									124.933
18									
19	FEET	T	19.5	20.9	19.5	20.9	20	21.4	21.067
20									OUT SPACERS

	Kindling	Pretest Fuel	Test Load
% Moisture - Dry Basis:	15.567% ✓	22.189% ✓	20.822% ✓
% Moisture - Wet Basis:	13.470% ✓	18.159% ✓	17.234% ✓

To obtain Wet from Dry: $\frac{100 \times \% \text{ Dry Rdg.}}{100 + \% \text{ Dry Rdg.}} = \% \text{ Moisture, Wet Basis}$

Acceptable Ranges: 16-20% wet; 19-25% dry
(17.5 - 22.5 on Meter [Uncor reading] at 70°F)

Key for Use: K= Kindling P= Pretest Fuel T= Test Fuel

WOOD DENSITY DETERMINATION
WOODSTOVE TEST DATA SHEET #11

Unit: HIGH VALLEY X-TEC
Run#: EDA#6
Date: 3/31/99
Technician: ATM PLS.
WST2-form11-Rev 6/90

Wood Piece: Nominal Dimensions: 3 1/2" x 3 1/2" x 1 1/2"
Depth (D): in 1.548 cm 3.9319 ✓
Width (W): in 3.512 cm 8.9205 ✓
Length (L): 3.444 cm ✓
3.369 cm "
3.448 cm "
3.407 cm "
Length \bar{X} = in 3.4170 ✓ cm 8.6792 ✓
Volume: 304.419 ✓ cm³
(D X W X L)

MOISTURE: Room Temperature: 55 °F Correction Factor: +1 1/2
Uncorrected Meter Readings Corrected for temperature: Yes No

NOTE: Record moisture meter readings to the nearest 0.5%

	Uncor	Cor	
Top:	17.0	18.1	%
Bottom:	18.5	19.8	%
Side:	17.0	18.1	%
\bar{X} :		18.667	% ✓

Avg % Moisture (Dry) 18.667 % ✓

Avg % Moisture (Wet) 15.730 %

Scale: Levelled In Out
Zeroed: In Out

Wet Weight: 177.1 g Dry Weight: 149.5 g

% Moisture Dried Basis: 15.584 % ✓
[1 - (Dry Wt ÷ Wet Wt)] X 100

Into Dryer Date 3/31/99 Time 1130 Temp 216 °F
Out of Dryer Date 4/19/99 Time 1504 Temp 214 °F

(Minimum Time in Dryer: 24 hrs.) ✓ Minimum Dryer Temp 100°C (212°F)

Density = 149.5 g ÷ 304.419 cm³ = .4911 g/cm³ ✓
(dry wt) (volume)

Pellet Fuel Moisture Content Determination

Tare Beaker Wt. _____ g
Wet Wt: _____ g - _____ g = _____ g
Gross Wet Wt. Tare Beaker Wt. Net Wet Wt.
Dry Wt: _____ g - _____ g = _____ g
Gross Dry Wt. Tare Beaker Wt. Net Dry Wt.
% Moisture Dried Basis: _____ %
[1 - (Net Dry Wt ÷ Net Wet Wt.)] X 100

Pre Burn T-tract wt.
7.2 lbs, 616.7 lbs.
Test Sheet wt. Range 609.5 - 608.7 lbs.

PRE BURN DATA
RECORD SHEET #13
WST2-Form16

BARDIURE
PRESSURE 17g
28.475

Unit: HIGH VALLEY X-TEC
Run: EPH ELG
Page: 1 of 1

Date: 3/30/99
Technician(s): ATH, PLS.

Hot Box On ✓

Minute	Scale Weight	Burn Rate	T/C#-3	Stove Top	Left Side	Back	Right Side	Bottom	Firebox	2nd Burn Catalyst	Room Temp	Static	Comments
0	616.7	0	578	826	537	535	578	518	887	1489	71	1085	Primary Air Set at 1 1/4"
5	616.1	.6	527	763	546	515	586	524	881	1559	70	1083	Secondary Air Set at 1 1/8"
10	615.2	.9	514	737	548	502	593	527	889	1611	71	1084	Fan: ON HIGH
15	614.1	1.1	513	731	552	495	600	527	912	1594	72	1085	TUNNEL ON AT: 1325
20	612.9	1.2	515	745	558	495	608	526	941	1558	72	1084	Buckets, Iced ✓
25	612.1	1.8	493	725	564	497	617	524	958	1420	71	1080	ANALYZERS SPANNED ✓
30	611.4	1.7	470	683	570	504	623	524	976	1427	72	1076	Pumps turned on at: 1335
35	610.8	1.6	436	631	574	515	631	524	983	1364	73	1072	AT
40	610.4	1.4	418	601	575	526	633	523	988	1315	73	1070	
45	610.1	1.3	397	565	571	535	630	524	973	1220	73	1068	check WB/DB: 88/112 ✓
50	609.8	1.3	378	532	564	538	626	524	965	1142	73	1065	
55	609.6	1.2	364	501	554	536	618	526	938	1099	73	1064	
60	609.5	1.1	351	480	543	534	612	528	911	1045	73	1061	Probe IN TUNNEL
65	609.3	1.2	336	451	528	523	602	529	898	1058	73	1061	Rake Combs Forward 539.4
70	609.1	1.2	341	451	517	501	592	527	872	1098	74	1060	526.6
75	609.0	1.1	339	449	499	478	576	522	854	1097	71	1059	504.8
80	608.9	1.1	335	444	490	460	561	516	839	1044	69	1059	
85	608.8	1.1	330	434	480	446	547	512	826	990	70	1057	
90	608.6	1.2	321	423	470	438	537	511	808	924	70	1055	475.8

T/C#	Minute	Stove Top	Left Side	Back	Right Side	Bottom	Firebox	2nd Burn	Room Temp	Tunnel	C. Gas Box	Impinger Out	5G-1 Filter	5G-1 Condenser	600- dat
0	10	473	470	438	537	511	808	924	70	92	253	39	72	39	257
5	30	545	450	410	510	505	745	1195	70	153	254	38	90	36	258
10	35	616	454	377	496	504	753	1522	70	141	259	38	90	36	259
15	40	650	458	365	494	499	781	1500	69	141	261	38	89	36	258
20	45	678	466	359	498	493	817	1458	69	142	257	38	89	36	257
25	50	707	477	360	505	486	860	1481	69	143	255	38	90	36	257
30	55	708	486	364	511	481	907	1568	69	141	254	38	89	36	254
35	1:00	685	504	362	526	477	922	1504	68	139	254	38	89	36	252
40	05	669	513	365	537	473	917	1368	68	137	253	38	89	36	251
45	10	655	518	370	547	471	913	1367	70	134	252	38	89	36	249
50	15	637	520	377	556	469	917	1366	70	133	251	38	89	36	248
55	20	629	521	387	565	468	926	1403	68	131	251	39	89	36	248
60	25	622	523	397	575	466	927	1364	70	130	250	39	89	37	247
65	30	607	525	403	581	464	924	1340	69	127	249	38	89	37	247
70	35	582	524	411	583	464	929	1272	70	124	248	39	88	37	246
75	40	557	519	426	582	465	934	1209	70	121	247	39	87	37	246
80	45	516	511	446	576	469	931	1162	69	117	245	39	86	37	245
85	50	502	508	452	572	471	926	1141	69	116	244	39	85	37	245
90	55	473	500	473	562	476	928	1138	69	113	243	39	84	37	246
95	1:00	446	493	469	549	481	914	1018	68	111	241	39	83	37	246
100	05	428	486	457	538	482	916	966	68	109	240	39	83	37	244
105	10	412	479	447	528	483	908	948	68	108	238	39	83	37	244
110	15	399	472	442	519	482	912	941	68	106	237	39	81	37	243
116	20	392	467	437	514	482	912	923	68	105	237	39	81	37	243
120	25	376	460	426	506	485	11062	13432	82	105	237	39	81	37	243
125	30	358	453	415	498	485	11062	13432	82	105	237	39	81	37	243
130	35	342	446	404	490	485	11062	13432	82	105	237	39	81	37	243
135	40	326	439	393	482	485	11062	13432	82	105	237	39	81	37	243
140	45	310	432	382	474	485	11062	13432	82	105	237	39	81	37	243
145	50	294	425	371	465	485	11062	13432	82	105	237	39	81	37	243
150	55	278	418	360	456	485	11062	13432	82	105	237	39	81	37	243
155	00	262	411	349	447	485	11062	13432	82	105	237	39	81	37	243
160	05	246	404	338	438	485	11062	13432	82	105	237	39	81	37	243
165	10	230	397	327	429	485	11062	13432	82	105	237	39	81	37	243
170	15	214	390	316	420	485	11062	13432	82	105	237	39	81	37	243
175	20	198	383	305	411	485	11062	13432	82	105	237	39	81	37	243
180	25	182	376	294	402	485	11062	13432	82	105	237	39	81	37	243
185	30	166	369	283	393	485	11062	13432	82	105	237	39	81	37	243
190	35	150	362	272	384	485	11062	13432	82	105	237	39	81	37	243
195	40	134	355	261	375	485	11062	13432	82	105	237	39	81	37	243
200	45	118	348	250	366	485	11062	13432	82	105	237	39	81	37	243
205	50	102	341	239	357	485	11062	13432	82	105	237	39	81	37	243
210	55	86	334	228	348	485	11062	13432	82	105	237	39	81	37	243
215	00	70	327	217	339	485	11062	13432	82	105	237	39	81	37	243
220	05	54	320	206	330	485	11062	13432	82	105	237	39	81	37	243
225	10	38	313	195	321	485	11062	13432	82	105	237	39	81	37	243
230	15	22	306	184	312	485	11062	13432	82	105	237	39	81	37	243
235	20	6	299	173	303	485	11062	13432	82	105	237	39	81	37	243
240	25	-10	292	162	294	485	11062	13432	82	105	237	39	81	37	243
245	30	-26	285	151	285	485	11062	13432	82	105	237	39	81	37	243
250	35	-42	278	140	276	485	11062	13432	82	105	237	39	81	37	243
255	40	-58	271	129	267	485	11062	13432	82	105	237	39	81	37	243
260	45	-74	264	118	258	485	11062	13432	82	105	237	39	81	37	243
265	50	-90	257	107	249	485	11062	13432	82	105	237	39	81	37	243
270	55	-106	250	96	240	485	11062	13432	82	105	237	39	81	37	243
275	00	-122	243	85	231	485	11062	13432	82	105	237	39	81	37	243
280	05	-138	236	74	222	485	11062	13432	82	105	237	39	81	37	243
285	10	-154	229	63	213	485	11062	13432	82	105	237	39	81	37	243
290	15	-170	222	52	204	485	11062	13432	82	105	237	39	81	37	243
295	20	-186	215	41	195	485	11062	13432	82	105	237	39	81	37	243
300	25	-202	208	30	186	485	11062	13432	82	105	237	39	81	37	243
305	30	-218	201	19	177	485	11062	13432	82	105	237	39	81	37	243
310	35	-234	194	8	168	485	11062	13432	82	105	237	39	81	37	243
315	40	-250	187	-3	159	485	11062	13432	82	105	237	39	81	37	243
320	45	-266	180	-12	150	485	11062	13432	82	105	237	39	81	37	243
325	50	-282	173	-21	141	485	11062	13432	82	105	237	39	81	37	243
330	55	-298	166	-30	132	485	11062	13432	82	105	237	39	81	37	243
335	00	-314	159	-39	123	485	11062	13432	82	105	237	39	81	37	243
340	05	-330	152	-48	114	485	11062	13432	82	105	237	39	81	37	243
345	10	-346	145	-57	105	485	11062	13432	82	105	237	39	81	37	243
350	15	-362	138	-66	96	485	11062	13432	82	105	237	39	81	37	243
355	20	-378	131	-75	87	485	11062	13432	82	105	237	39	81	37	243
360	25	-394	124	-84	78	485	11062	13432	82	105	237	39	81	37	243
365	30	-410	117	-93	69	485	11062	13432	82	105	237	39	81	37	243
370	35	-426	110	-102	60	485	11062	13432	82	105	237	39	81	37	243
375	40	-442	103	-111	51	485	11062	13432	82	105	237	39	81	37	243
380	45	-458	96	-120	42	485	11062	13432	82	105	237	39	81	37	243
385	50	-474	89	-129	33	485	11062	13432	82	105	237	39	81	37	243
390	55	-490	82	-138	24	485	11062	13432	82	105	237	39	81	37	243
395	00	-506	75	-147	15	485	11062	13432	82	105	237	39	81	37	243
400	05	-522	68	-156	6	485	11062	13432	82	105	237	39	81	37	243
405	10	-538	61	-165	-3	485	11062	13432	82	105	237	39	81	37	243
410	15	-554	54	-174	-12	485	11062	13432	82	105	237	39	81	37	243
415	20	-570	47	-183	-21	485	11062	13432	82	105	237	39	81	37	243
420	25	-586	40	-192	-30	485	11062	13432	82	105	237	39	81	37	243
425	30	-602	33	-201	-39	485	11062	13432	82	105	237	39	81	37	243
430	35	-618	26	-210	-48	485	11062	13432	82	105	237	39	81	37	243
435	40	-634	19	-219	-57	485	11062	13432	82	105	237	39	81	37	243
440	45	-650	12	-228	-66	485	11062	13432	82	105	237	39	81	37	243
445	50	-666	5	-237	-75	485	11062	13432	82	105	237	39	81	37	243
450	55	-682	-2	-246	-84	485	11062	13432	82	105	237	39	81	37	243
455	00	-698	-9	-255	-93	485	11062	13432	82	105	237	39	81	37	243
460	05	-714	-16	-264											

T/C#	Minute	Stove Top	Left Side	Back	Right Side	Bottom	Firebox	2nd Burn	Room Temp	Tunnel	C. Gas Box	Impinger Out	5G-1 Filter	5G-1 Condenser	Com-der
120	15	381	460	428	504	482	904	925	67	104	235	39	80	37	243
125	20	374	457	425	500	482	890	914	69	103	234	39	80	37	243
130	35	367	453	426	495	482	862	891	69	102	233	39	81	37	242
135	40	362	448	428	490	482	864	878	70	101	233	39	82	37	241
140	45	357	444	432	487	487	847	876	70	101	231	39	83	37	241
145	50	354	440	432	484	479	796	853	70	100	230	39	83	37	240
150	55	350	434	443	481	478	785	831	70	99	229	39	83	37	240
155	100	346	428	448	479	477	775	824	70	99	228	39	83	37	240
160	05	342	422	451	477	476	762	810	70	98	228	39	84	37	240
165	10	337	416	446	476	476	753	800	70	98	227	39	84	37	240
170	15	334	411	444	473	475	750	793	70	97	227	39	84	37	239
175	20	331	407	441	472	475	752	785	70	97	226	39	84	37	239
180	25	327	404	437	469	475	750	774	70	96	226	38	83	37	239
185	30	321	400	431	464	473	751	762	70	95	226	38	83	37	239
190	35	318	396	425	462	472	739	756	70	95	225	39	83	37	240
195	40	314	393	418	462	472	733	744	70	94	225	39	83	37	239
200	45	310	390	411	454	468	722	732	70	94	225	38	83	37	239
205	50	306	386	407	450	465	728	726	70	93	224	38	83	37	239
210	55	302	384	407	445	462	731	726	70	93	223	38	82	37	239
215	1800	299	382	403	441	458	717	713	70	92	223	38	82	37	239
220	05	296	379	400	437	455	708	705	70	92	223	38	81	37	238
225	10	293	377	398	433	451	702	698	70	92	223	38	81	37	238
230	15	290	375	396	431	449	692	692	70	91	222	38	81	37	238
235	20	287	372	393	428	446	685	685	70	91	222	38	81	37	238
240	25	284	370	391	426	444	678	678	70	91	222	38	81	37	238
245	30	281	367	388	423	441	671	671	70	91	222	38	81	37	238
250	35	278	364	385	420	438	664	664	70	91	222	38	81	37	238
255	40	275	361	382	417	435	657	657	70	91	222	38	81	37	238
260	45	272	358	379	414	432	650	650	70	91	222	38	81	37	238
265	50	269	355	376	411	429	643	643	70	91	222	38	81	37	238
270	55	266	352	373	408	426	636	636	70	91	222	38	81	37	238
275	00	263	349	370	405	423	629	629	70	91	222	38	81	37	238
280	05	260	346	367	402	420	622	622	70	91	222	38	81	37	238
285	10	257	343	364	399	417	615	615	70	91	222	38	81	37	238
290	15	254	340	361	396	414	608	608	70	91	222	38	81	37	238
295	20	251	337	358	393	411	601	601	70	91	222	38	81	37	238
300	25	248	334	355	390	408	594	594	70	91	222	38	81	37	238
305	30	245	331	352	387	405	587	587	70	91	222	38	81	37	238
310	35	242	328	349	384	402	580	580	70	91	222	38	81	37	238
315	40	239	325	346	381	399	573	573	70	91	222	38	81	37	238
320	45	236	322	343	378	396	566	566	70	91	222	38	81	37	238
325	50	233	319	340	375	393	559	559	70	91	222	38	81	37	238
330	55	230	316	337	372	390	552	552	70	91	222	38	81	37	238
335	00	227	313	334	369	387	545	545	70	91	222	38	81	37	238
340	05	224	310	331	366	384	538	538	70	91	222	38	81	37	238
345	10	221	307	328	363	381	531	531	70	91	222	38	81	37	238
350	15	218	304	325	360	378	524	524	70	91	222	38	81	37	238
355	20	215	301	322	357	375	517	517	70	91	222	38	81	37	238
360	25	212	298	319	354	372	510	510	70	91	222	38	81	37	238
365	30	209	295	316	351	369	503	503	70	91	222	38	81	37	238
370	35	206	292	313	348	366	496	496	70	91	222	38	81	37	238
375	40	203	289	310	345	363	489	489	70	91	222	38	81	37	238
380	45	200	286	307	342	360	482	482	70	91	222	38	81	37	238
385	50	197	283	304	339	357	475	475	70	91	222	38	81	37	238
390	55	194	280	301	336	354	468	468	70	91	222	38	81	37	238
395	00	191	277	298	333	351	461	461	70	91	222	38	81	37	238
400	05	188	274	295	330	348	454	454	70	91	222	38	81	37	238
405	10	185	271	292	327	345	447	447	70	91	222	38	81	37	238
410	15	182	268	289	324	342	440	440	70	91	222	38	81	37	238
415	20	179	265	286	321	339	433	433	70	91	222	38	81	37	238
420	25	176	262	283	318	336	426	426	70	91	222	38	81	37	238
425	30	173	259	280	315	333	419	419	70	91	222	38	81	37	238
430	35	170	256	277	312	330	412	412	70	91	222	38	81	37	238
435	40	167	253	274	309	327	405	405	70	91	222	38	81	37	238
440	45	164	250	271	306	324	398	398	70	91	222	38	81	37	238
445	50	161	247	268	303	321	391	391	70	91	222	38	81	37	238
450	55	158	244	265	300	318	384	384	70	91	222	38	81	37	238
455	00	155	241	262	297	315	377	377	70	91	222	38	81	37	238
460	05	152	238	259	294	312	370	370	70	91	222	38	81	37	238
465	10	149	235	256	291	309	363	363	70	91	222	38	81	37	238
470	15	146	232	253	288	306	356	356	70	91	222	38	81	37	238
475	20	143	229	250	285	303	349	349	70	91	222	38	81	37	238
480	25	140	226	247	282	300	342	342	70	91	222	38	81	37	238
485	30	137	223	244	279	297	335	335	70	91	222	38	81	37	238
490	35	134	220	241	276	294	328	328	70	91	222	38	81	37	238
495	40	131	217	238	273	291	321	321	70	91	222	38	81	37	238
500	45	128	214	235	270	288	314	314	70	91	222	38	81	37	238
505	50	125	211	232	267	285	307	307	70	91	222	38	81	37	238
510	55	122	208	229	264	282	300	300	70	91	222	38	81	37	238
515	00	119	205	226	261	279	293	293	70	91	222	38	81	37	238
520	05	116	202	223	258	276	286	286	70	91	222	38	81	37	238
525	10	113	199	220	255	273	279	279	70	91	222	38	81	37	238
530	15	110	196	217	252	270	272	272	70	91	222	38	81	37	238
535	20	107	193	214	249	267	265	265	70	91	222	38	81	37	238
540	25	104	190	211	246	264	258	258	70	91	222	38	81	37	238
545	30	101	187	208	243	261	251	251	70	91	222	38	81	37	238
550	35	98	184	205	240	258	244	244	70	91	222	38	81	37	238
555	40	95	181	202	237	255	237	237	70	91	222	38	81	37	238
560	45	92	178	199	234	252	230	230	70	91	222	38	81	37	238
565	50	89	175	196	231	249	223	223	70	91	222	38	81	37	238
570	55	86	172	193	228	246	216	216	70	91	222	38	81	37	238
575	00	83	169	190	225	243	209	209	70	91	222	38	81	37	238
580	05	80	166	187	222	240	202	202	70	91	222	38	81	37	238
585	10	77	163	184	219	237	195	195	70	91	222	38	81	37	238
590	15	74	160	181	216	234	188	188	70	91					

PRE AND POST TEST ZERO/SPAN CHECK
WOODSTOVE DATA SHEET #15-1

COVILLE

Site: Myren Consulting, Woodinville, WA Date: 3/30/99 Analyte: CO₂

Source: HIGH VALLEY X-TEC Run #: EPA #6

Zero Cyl #: 36919 Conc. 00.0 % CO₂ Cyl Press: 210 psi

Certified by: CASCADE AIRGAS Date: 4/24/96

Span Cyl #: 250-1060 Conc. 6.0 % CO₂ Cyl Press: 1425 psi

Certified by: OxARC Date: 8/22/97

Analyzer: Make: Horiba Model: PIR-2000 SN: 607024

Range: 0 - 25.0% CO₂ Analyzer Output: 0 - 1.0 v.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter:

EPA Span Value = 25.0% CO₂

EPA Control Limits = + 2.5% of 25.0% CO₂ = + 0.625% CO₂

Pre Run Audit: By: (ATM) PLS. Time: 1327 Temp: 70 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	00.0	.000	.02555	.02555	0.10
Span	24.0	.240	6.0	23.5	.236	5.8413	-.10871	-1.81

Comments:

Post Run Audit: By: (ATM) PLS. Time: 1900 Temp: 69 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	00.0	.000	.02555	.02555	0.10
Span	24.0	.240	6.0	23.5	.234	5.8416	-.15842	-2.64

Comments:

+ Conc. Difference = Act % - Exp (Std) %
 Zero % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$
 Span % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

PRE AND POST TEST ZERO/SPAN CHECK
WOODSTOVE DATA SHEET #15-2

Site: Myren Consulting, Woodinville, WA Date: 3/30/99 Analyte: O₂

Source: HIGH VALLEY X-TEC Run #: EPA # 6

Zero Cyl #: 36919 Conc. 00.0 % O₂ Cyl Press: 210 psi

Certified by: CASCADE AIRGAS Date: 4/24/96

Span Cyl #: 250-1060 Conc. 6.0 % O₂ Cyl Press: 1425 psi

Certified by: OXARC Date: 8/22/97

Analyzer: Make: Taylor Model: OA 137 SN: 137/4772

Range: 0 - 25.0% O₂ Analyzer Output: 0 - 100 mv.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter: _____

EPA Span Value = 25.0% O₂

EPA Control Limits = + 2.5% of 25.0% O₂ = + 0.625% O₂

Pre Run Audit: By: ATM, RLS, Time: 1327 Temp: 70 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ%
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	00.0	00.0	-0.055	-0.055	-0.06
Span	6.0	24.0	6.0	6.0	23.8	5.9555	-0.04455	-0.74

Comments:

Post Run Audit: By: ATM, RLS, Time: 1900 Temp.: 69 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ%
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	00.0	00.0	-0.055	-0.055	-0.06
Span	6.0	24.0	6.0	6.0	23.7	5.9304	-0.06964	-1.16

Comments:

+ Conc. Difference = Act % - Exp (Std) %

Zero % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$

Span % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

PRE AND POST TEST ZERO/SPAN CHECK
WOODSTOVE DATA SHEET #15-3

Site: Myren Consulting, Woodinville, WA Date: 3/30/99 Analyte: CO

Source: HIGH VALLEY X-TEC Run #: EPA #6

Zero Cyl #: 36919 Conc. 00.0 % CO Cyl Press: 210 psi

Certified by: CASCADE AIRGAS Date: 4/24/96

Span Cyl #: 250-1060 Conc. 1.26 % CO Cyl Press: 1425 psi

Certified by: OXARC Date: 8/22/97

Analyzer: Make: Infra Red Model: 702 D SN: 113

Range: 0 - 10.0% CO Analyzer Output: 0 - 100 mv.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter:

EPA Span Value = 5.0% CO

EPA Control Limits = +2.5% of 5.0% CO = + 0.125% CO

Pre Run Audit: By: ATH, RLS, Time: 1327 Temp: 70 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.00	00.0	-0.0091	-0.0091	-0.18
Span	1.26	25.2	1.26	1.25	24.7	1.2317	-0.0283	-2.25

Comments:

Post Run Audit: By: ATH, RLS, Time: 1900 Temp.: 69 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.00	00.1	-0.0040	-0.0040	-0.08
Span	1.26	25.2	1.26	1.24	24.5	1.2216	-0.03837	-3.05

Comments:

+ Conc. Difference = Act % - Exp (Std) %

Zero % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$

Span % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

Run: EPA #6
 Date: 3/30/99
 Technicians: ATH, RLS
 WST6-Form3-Rev11/89

QUALITY CHECKS
 WOODSTOVE DATA SHEET #16

Ambient = Tr: _____ °F T/C#30: _____ °F
 Thermocouple Check (at ambient): T/C#1: 48 °F; T/C#2: 49 °F;
 T/C #3: 49 °F; T/C #4: 49 °F; T/C #5: 48 °F;
 T/C #6: 49 °F; T/C #7: 49 °F; T/C #8: 49 °F;
 T/C #9: 50 °F; T/C #10: 50 °F; T/C #11: 49 °F;
 T/C #12: 48 °F; T/C #13: 49 °F; T/C #14: 50 °F;
 T/C #15: 49 °F; T/C #16: 49 °F; T/C #17: 49 °F;
 T/C #18: — °F; T/C #19: _____ °F; T/C #20: _____ °F;
 T/C #21: _____ °F; T/C #22: _____ °F; T/C #23: _____ °F;
 T/C #24: _____ °F; T/C #25: _____ °F; T/C #26: _____ °F;

Comments: lab quite cold - overnight fire went out early.

Thermocouple Readout: Pretest Zero/Span Check and Calibration:
 Zero (0°F) : 002 °F Adj to: — °F Post Test Check Zero (0°F): 001 °F % Difference +0.05
 Span (2000°F): 1998 °F Adj to: — °F Span (2000°F): 1999 °F -0.05
 (Allowable % Difference = 1.5%. Use formulas on Woodstove Data Sheet #15 to calculate % Difference)

Thermocouple Readout Pretest Linearity Check
 0°F = 002 °F; 200°F = 201 °F; 400°F = 401 °F;
 600°F = 599 °F; 800°F = 799 °F; 1000°F = 1000 °F;
 1200°F = 1199 °F; 1400°F = 1399 °F; 1600°F = 1598 °F;
 1800°F = 1797 °F; 2000°F = 1998 °F

Combustion Gas (CO₂, O₂, CO) Train Leak Check: Pre Post
 Draft (Static) Guage Zero Check: Pre Post

Scale Check Pre (Wt, #'s): 614.7 - 609.7 lbs = 5.0 lbs / 5.0 lbs OK (ATH)
 Post (Wt, #'s): 614.0 - 609.0 = 5.0 lbs / 5.0 lbs OK (ATH)

Stack cleaned prior to the run: Yes _____ No
 Tunnel cleaned prior to the run: Yes _____ No

HIVALLEYEPA1
MYREN CONSULTING CERTIFICATION TEST DATA

DILUTION TUNNEL CALCULATIONS
3/31/96

File Name:	HIVALLEYEPA1	PITOT	TNL	GAS	GAS	GAS	TUNNEL	PROP	dDGM
Stove Manufacturer:	HI VALLEY	DELTA P	TEMP	METER	METER	METER	VELOCIT	RATE	vol std
Model Number:	XTEC	(- INCH	(°F)	RDG	TEMP	DELTA H	(ft/min)	(%)	(ft3)
Lab Name:	MYREN	H2O.)		(ft3)	(°F)	(in.H2O)			
Test Date:	3/20/99	0	147	781.047	79	0.900	919.27		
Run Number:	EPA 1	10	187	786.422	79	0.900	904.90	100.6	5.047
Meter Box Y Factor:	1.003	20	188	791.928	80	0.900	905.60	104.7	5.160
Barometric pressure (in):	28.5367	30	177	797.402	81	0.900	897.88	102.0	5.121
Gas meter temp (ave):	83	40	173	802.986	82	0.900	895.06	104.1	5.214
delta H(ave):	0.900	50	161	808.506	83	0.900	886.54	101.1	5.145
Gas meter initial reading:	781.047	60	149	813.979	84	0.900	888.84	99.1	5.091
Gas meter final reading:	844.735	70	146	819.493	85	0.900	897.39	98.9	5.120
Front catch (acetone) mg:	5.1	80	135	825.069	85	0.900	889.21	97.3	5.178
first filter catch (mg):	10.8	90	131	830.649	85	0.900	886.22	97.6	5.181
second filter catch (mg):	-0.5	100	126	836.246	85	0.900	882.46	97.4	5.197
tunnel flow (ave cfm):	138.666	110	123	841.879	85	0.900	880.20	97.9	5.231
Emission Rate(g/hr):	2.165	115	121	844.735	85	0.900	878.69	99.2	2.652
Emission Rate(M5H) :	3.455						0.00	0.0	0.000
vs/VmTs:	0.0246	140					0.00	0.0	0.000
vs ave:	893.250	150					0.00	0.0	0.000
Tunnel average temp (°f):	151.077	160					0.00	0.0	0.000
Test time(min):	115	170					0.00	0.0	0.000
Fuel Load(lb. wet):	17.2	180					0.00	0.0	0.000
Wood moisture(%wet):	17.616	190					0.00	0.0	0.000
Burn rate(dry kg/hr):	3.353	200					0.00	0.0	0.000
Samp vol(scfl):	59.336	210					0.00	0.0	0.000
front filter number	774	220					0.00	0.0	0.000
back filter number	773	230					0.00	0.0	0.000
acetone beaker number	11	240					0.00	0.0	0.000
PRELIMINARY RESULTS		250					0.00	0.0	0.000
FINAL RESULTS	AUDITED	260					0.00	0.0	0.000
DATA SUMMARY		270					0.00	0.0	0.000
MODEL :	XTEC	280					0.00	0.0	0.000
RUN:	EPA 1	290					0.00	0.0	0.000
DATE:	3/20/99	300					0.00	0.0	0.000
DBR:	3.353	310					0.00	0.0	0.000
GPH UNADJ	2.165	320					0.00	0.0	0.000
ADJ	3.455143662	330					0.00	0.0	0.000
		340					0.00	0.0	0.000
		350					0.00	0.0	0.000

DATE 3/20/99

PAGE 1 OF 1

MODEL # HIGH VALLEY X-TEC RUN # EPA # 1

METER BOX # 511 M

METER Y 1.003


FILTER # (F) 774 (R) 77

PRE-TEST LEAK RATE = .000 CFM @ -16.0 IN. HG .642/.642

FILTER SIZE: 110 MM

POST TEST LEAK RATE = .000 CFM @ -14.0 IN. HG .084/.084

PROBE LENGTH 24" Glass

TIME		METER READING CU.FT.	PITOT dp	TNL TEMP. (°F)	METER TEMP. (°F)	GAS. METER dh	VAC IN. Hg	VELOCITY TRAVERSE			
CLOCK	ELAPSED							POINT	LOCATION	ΔP	TEMP
1440	00	781.047	-044	147	79	90	0	N-1	0.5"	7028	175
	50	786.422	-040	187	79	90	0	2	1.5"	7042	178
1500	20	791.928	-040	188	80	90	0	3	4.5"	7046	179
	10	797.402	-040	177	81	90	0	4	5.5"	7045	178
	20	802.986	-040	173	82	90	0	W-1	0.5"	7042	184
	30	808.506	-040	161	83	90	0	2	1.5"	7047	185
	40	813.979	-041	149	84	90	0	3	4.5"	7042	186
	50	819.493	-042	146	85	90	0	4	5.5"	7040	186
1600	80	825.019	-042	135	85	90	0		7.5"	7042	181
	10	830.649	-042	131	85	90	0	Pre-test leak checked <input checked="" type="checkbox"/> Post-test <input checked="" type="checkbox"/>			
	20	836.246	-042	126	85	90	0	Cp = <u>0.99</u>			
	30	841.879	-042	123	85	90	0	→ 			
1635	115	844.735	-042	121	85	90	0	* = point of Avg. delta p			
	50	(63.688)						Qs = $\left(\frac{\sqrt{\Delta P \times BP}}{T(^{\circ}R)} \right) \times 3167.2$			
1700	40							<u>137.033</u> cfm			
	50							BP = <u>START 28.57</u> in Hg			
	60							60 28.53			
	70							115 28.51			
	80							180			
	90							240			
								300			

28.5367

WOODSTOVE DATA SHEET #4-1: INITIAL FILTER WEIGHTS (TARE WEIGHTS)

Into Dessicator: Date 1/3/99 Time 12:00 By ATM Front Half Back Half

Manufacturer: Schleicher & Schuell Size: 11 cm Lot. No.: ZB951 Grade: # 25g/las
Order No. 06220

Filter #	First Wt	Date	Time	By	Second Wt	Date	Time	By	Third Wt	Date	Time	By
751	.7787	1/23/99	1115	ATM	.7786	2/2/99	1051	T.M.				
752	.8115		1116	ATM	.8115		1050	ATM				
753	.8063		1117		.8061		1049	ATM				
754	.8044		1118		.8044		1048	ATM				
755	.7882		1119		.7878		1047	ATM				
756	.7831		1120		.7827		1046	ATM				
757	.7893		1121		.7886		1045	ATM	.7886	2/2/99	1430	Jm
758	.8025		1122		.8023		1044	ATM				
759	.7960		1123		.7956		1044	ATM	.7957	2/2/99	1240	T.M.
760	.7915		1124		.7914		1043	ATM				
761	.8115		1125		.8116		1042	ATM				
762	.7689		1126		.7687		1041	ATM				
763	.7894		1127		.7893		1040	ATM				
764	.7793		1128		.7792		1039	ATM				
765	.7910		1129		.7907		1038	ATM				
766	.7957		1130		.7954		1037	ATM				
767	.8028		1131		.8024		1036	ATM				
768	.8048		1132		.8044		1036	ATM				
769	.7722		1133		.7716		1035	ATM	.7715	2/2/99	1240	T.M.
770	.7895		1134		.7897		1034	ATM				
771	.7693		1135		.7691		1034	ATM				
772	.7895		1136		.7893		1033	ATM				
773	.8073		1137		.8070		1030	ATM	← ✓			
774	.8181		1138		.8177		1031	ATM	← ✓			
775	.8056	✓	1139	✓	.8051	✓	1030	ATM				

Checked by Jm 7/1/99 Date: 2/2/99 Time 1430

QA REWEIGH

Filter #	WT	Date	Time	By
758	.8021	2/2/99	1431	Jm
762	.7685	2/2/99	1432	Jm
767	.8028	2/2/99	1433	Jm

BALANCE ROOM ENVIRONMENTAL CONDITIONS

WB	DB	%RH	Date	Time	By
62	77	42	1/22/99	1100	ATM
60	73	46	2/2/99	0939	ATM
62	76	45	2/2/99	1235	ATM
65	80	44	2/19/99	1312	ATM

Post Weighing Security Scale Check
 1st 2nd 3rd
 0.0000 0.0000 -0.0002 0.0000
 1.0000 1.0000 0.9998 1.0001

WOODSTOVE DATA SHEET #4-4
SCALE QA SHEET

Dates From 1/19/99

Scale Mettler

Through _____

Model AE10(
SN K04827

Level	Recall- brated	100g Weight	10g Weight	1.0g Weight	100mg Weight	20mg Weight	Date	Time	Tech	Wet Bulb	Dry Bulb	% RH
✓	Yes	99,9999	10,0000	1,0000	1,0000	0,0200	1/9/99	1243	ATM	58	70	48
✓	No	100,0002	10,0000	1,0000	1,0000	0,0200	1/14/99	1113	ATM	62	75	47
✓	YES	99,9999	10,0002	1,0000	0,9999	0,0201	1/23/99	1100	ATM	63	77	42
✓	YES	99,9999	10,0000	1,0000	1,0000	0,0201	1/24/99	1318	ATM	59	74	45
✓	YES	99,9999	10,0002	1,0000	1,0000	0,0200	2/1/99	0910	ATM	55	69	39
✓	YES	99,9999	10,0000	1,0000	1,0000	0,0201	2/2/99	0937	ATM	60	73	46
✓	YES	99,9999	10,0000	1,0000	1,0000	0,0200	2/3/99	1555	ATM	63	76	47
✓	YES	99,9999	10,0000	1,0000	1,0000	0,0201	2/7/99	1235	ATM	62	76	45
✓	YES	99,9998	10,0000	1,0000	1,0000	0,0200	2/10/99	1600	ATM	63	77	45
✓	YES	99,9998	10,0000	1,0000	1,0000	0,0200	2/19/99	0246	ATM	64	78	46
✓	No	99,9999	10,0000	1,0000	1,0000	0,0200	2/21/99	1312	ATM	65	80	44
✓	No	99,9999	10,0000	1,0000	1,0000	0,0200	3/5/99	1935	ATM	64	80	41
✓	YES	99,9997	10,0000	1,0000	1,0000	0,0200	3/6/99	1135	ATM	64	79	43
✓	YES	99,9997	10,0000	1,0000	1,0000	0,0200	3/13/99	1526	ATM	65	80	44
✓	YES	99,9999	10,0000	1,0000	1,0000	0,0200	3/14/99	1325	ATM	63	78	45
✓	No	100,0001	10,0000	1,0000	1,0000	0,0200	3/15/99	1623	ATM	66	81	45
✓	Yes	99,9997	10,0000	1,0000	1,0000	0,0200	3/16/99	0225	ATM	65	82	39
✓	Yes	99,9996	10,0000	1,0000	1,0000	0,0200	3/17/99	1615	ATM	62	77	42
✓	Yes	99,9997	10,0000	1,0000	1,0000	0,0200	3/18/99	2140	ATM	68	84	43
✓	Yes	99,9997	10,0000	1,0000	1,0000	0,0200	3/20/99	1300	ATM	64	84	32
✓	Yes	99,9999	10,0000	1,0000	1,0000	0,0201	3/21/99	2215	ATM	61	74	47
✓	Yes	99,9997	10,0000	1,0000	1,0000	0,0200	3/22/99	2122	ATM	65	85	33
✓	Yes	99,9997	10,0000	1,0000	1,0000	0,0200	3/23/99	1115	ATM	69	87	46
✓	Yes	99,9997	10,0000	1,0000	1,0000	0,0201	3/24/99	1120	ATM	77	89	43
✓	Yes	99,9999	10,0000	1,0000	1,0000	0,0201	3/29/99	2038	ATM	87	92	45
✓	No	99,9999	10,0002	1,0000	1,0000	0,0202	3/30/99	0610	ATM	66	80	47
✓	No	99,9999	10,0000	1,0000	1,0000	0,0201	3/31/99	1800	Yes	67	80	41
✓	No	99,9996	10,0000	1,0000	1,0000	0,0201	4/5/99	1730	ATM	64	80	41
✓	Yes	99,9997	10,0000	1,0000	1,0000	0,0201	4/6/99	1030	ATM	61	75	44
QC	Successful	Fluid	4/6/99	50.0000	5.0000	0.0201	4/6/99	1730	ATM			
✓	No	100,0003	10,0001	1,0001	1,0001	0,0201	4/6/99	1730	ATM			

Unit HIGH VALLEY X-TEC
 Run # EPA #1
 Date 3/20/99
 Technician ATH, RLS,
 WST6 Form 1, Rev 8/96

MISCELLANEOUS TEST DATA
 WOODSTOVE DATA SHEET #8

Useable Firebox Dimensions: See QC Section Useable Volume: 2.713 ft³

Dilution Tunnel Draft (If applicable): Start 00.0 Stop 00.0

Test Chamber Air Velocity: Start: 00.0 Stop: 00.0 Avg: 00.0

Wet Bulb/ Start: WB: 58 °F DB: 73 °F 1.15 % Amb Moisture 39 %RH

Dry Bulb Stop: WB: 59 °F DB: 72 °F 1.25 % Amb Moisture 45 %RH

$\bar{X} = 1.20$ % Ambient Moisture $\bar{X} = 42$ % Relative Humidity (RH)

Empty Stove Wt: 514.0 lbs.

Empty Stove Wt with Stack (Inc. Oil Seal) Wet: 606.3 lbs. Dry: 604.5 lbs.

Empty Stove Wt with Stack and Ash Ash: 0 lbs. Total: 604.5 lbs. ✓

Kindling Wt. Paper: 0.3 lbs. Wood: 5.0 lbs.

Pre Burn Fuel Wt. 14.9 + 15.8 + 16.0 + 4.5 + 5.1 Total: 56.3 lbs.

Total Kindling and Pre Burn Fuel Wt 61.6 lbs.

Coal Bed Wt-lbs: Range (608.8 - 608.0) lbs. Actual: 608.0 lbs.

Allowable Amount of Charcoal that can be removed: (3.5)

Coal Bed Wt. Range 4.3 Upper Wt. + 3.5 Lower Wt. $12 \times .25 =$.9 lbs. ✓

Test Fuel Wt-lbs: Ideal 19.0 lbs. Range: 17.1 - 20.8 lbs. Actual: 17.2 lbs.

Test Fuel Size (pcs.) (.75 x 1.5 x 5" Flanges) 20 Pcs.

2 x 4's x 17.0 " 4 Pcs 9.5 lbs. 55.2 % ✓

4 x 4's x 17.0 " 2 Pcs 7.7 lbs. 44.8 % ✓

Est. Dry Burn Rate (Kg/Hr.) $\frac{17.2}{2.2046} - \frac{(17.2 \times 17.616)}{115} \times \frac{60}{115} =$ 3.351 Est. Dry Burn Rate (Kg/Hr)

Est EPA Heat Output (HO_E) (Avg BTU's/Hr) $(19,140) \times \frac{63}{100} \times \frac{3.351}{115} =$ 410,407 Est Heat Output (HO_E) BTU's/Hr

Comments:

Stove Operating Data
Woodstove Test Data Sheet #9
Cold Start

Unit: HIGH VALLEY X-TEC
Run: EPA #1
Date: 3/20/99
Technician(s): ATH, PLS.
Data Sheet #9 - Rev 1/98-Pg.2

Fire Started: 1030 P.S.T

Warm up and Preburn: Primary Air: Wide open from ignition until the start of preburn when the primary air control(s) was (were) adjusted to the run setting of WIDE OPEN. At the run setting until the start of the test.

Secondary Air: No Controls, Naturally drafted.

Secondary Burn/Cat Bypass: N/A

Charcoal Bed Preparation: Broke up, raked and leveled the coal bed prior to the addition of each warm up/pre burn fuel charge. Starting 1:30 before the start of the test, broke up, raked and leveled the coal bed. In stove for 35 seconds.

Test: Door wide open during loading 1 min 05 sec, then

Primary Air: Wide open during the ~~start~~ of the test until High Burn. Adjusted to the run setting of High Burn between High Burn and High Burn. At the run setting of Wide Open at 0:00 into the run.

Secondary Air: No Controls, Naturally drafted

Secondary Burn/Cat Bypass: N/A

Fan: ON OFF during the warm up, ON OFF high during the preburn, ON OFF at the start of the test, ON OFF for the first 5 minutes of the test, ON OFF high at 5 minutes into the test, ON OFF for the rest of the test.

Test Run Anomalies:

WOODSTOVE OPERATING DATA
 WOODSTOVE DATA SHEET #9A-1

Wood Data: Kindling: A mix of the below grades

	Size	Mill	Grade	Species
Pre Burn	<u>2x4</u>	<u>CANYON LBR.</u>	<u>STD. & BTR.</u>	<u>D. FIR, S. GRN.</u>
Test Fuel	<u>2x4</u>	<u>CANYON LBR.</u>	<u>#2 STD. & BTR.</u>	<u>D. FIR, S. GRN.</u>
	<u>4x4</u>	<u>STAND. & R79</u>	<u>#2 STD. & BTR.</u>	<u>D. FIR, S. GRN.</u>

All grades WCLB Rules unless otherwise noted.

Warm up Information:

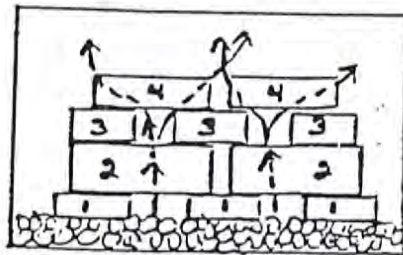
- 1st Warm up/Pre Burn Fuel charge (14.9 lbs) added at 1048.
- 2nd Warm up/Pre Burn Fuel charge (15.8 lbs) added at 1153.
- 3rd Warm up/Pre Burn Fuel charge (16.0 lbs) added at 1254.
- 4th Warm up/Pre Burn Fuel charge (4.5 lbs) added at 1345.
- 5th Warm up/Pre Burn Fuel charge (5.1 lbs) added at 1407.
- 6th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.
- 7th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.
- 8th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.

The coals were scooped out of the stove immediately prior to adding the 3rd pre burn/warm up fuel charge. The stove lost 1.8 lbs. Put 3.0 lbs of coals back in after the scoop.

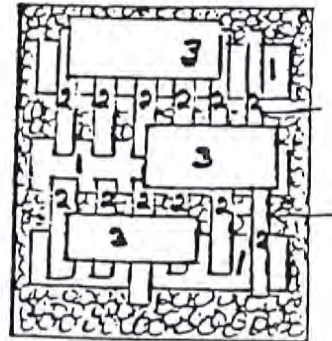
All pre burn/warm up fuel pieces were either 16" or _____ inches long. All preburn pieces/fuel charges were "ricked" in the stove. The pieces in the bottom layer in each rick contained 2 pcs that were 16 inches long and were loaded flat and perpendicular to the door. The pieces in the second layer in each rick were loaded on their side (edge) approximately parallel to the door and contained 4 pcs 16 inches long. The third layer (and fourth layer if present) was loaded flat, perpendicular to the door and contained 3 pcs 16 inches long. The majority of the pieces in each rick were in the second layer which had an approximate 0.5-1.0" space between pieces. (The loading directions indicate the direction of the longest dimension on each piece relative to the loading door opening.) Each pre burn/warm up fuel charge normally weighs within the weight range allowed for the actual test fuel charge

Warm up Information (cont.):

Each warm up/preburn fuel charge was ricked in exactly (as much as possible) the same manner and the weight of each rick was usually within the allowable weight range for the test fuel charge. The physical arrangement and alignment of each rick was designed to accomplish three (3) things: (1) The bottom layer was nestled firmly into the coal bed and was as close to being level with the bottom of the stove as possible, thus providing a stable loading platform for the rest of the rick, keeping it in a ricked state (as opposed to a collapsed or fallen down state) until the rick reached the charcoal stage and sags or collapses of its own accord. (2) It enhances the flow of primary air through the ricked preburn fuel charge, for the primary air would flow through the spaces between the pieces in the first layer and then up through the spaces between the pieces in the second, third and, if present, fourth layers. (3) It maximized, as much as possible, the surface to volume ratio of each preburn fuel charge, thereby allowing the fire immediate access to as much wood surface as possible and, thereby, insuring uniform charcoalization. All three of these enhance combustion and so get the stove as hot as possible during the warm up period, thereby maximizing the amount of heat (BTU's) stored in the stove. The actual preburn was not started until the stove surface temperatures had maximized and stabilized, thus indicating that the amount of heat stored in the stove had peaked. For this stove, the thermal storage was monitored using the TOP surface temperature(s) and the peak value(s) obtained were 905 of.



Front View



Top View

The arrows indicate the direction of the air flow through the rick.

The primary air was adjusted to the run setting of Wide Open 21.3 lbs above the upper charcoal bed weight.

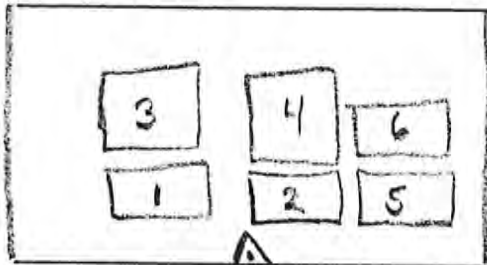
WOODSTOVE OPERATING DATA
WOODSTOVE DATA SHEET #9A-3

Unit HIGH VALLEY X-TE
Run # EPA #1
Date 3/20/99
Technician ATM, RLS,
Page 3 of 3
WST5-Form2-Rev11789

Additional Comments: Test Start Sequence: ① Turned fan off
② Opened door ③ Loaded fuel, ④ clear coals from
in front of the LPAO ⑤ Photograph ⑥ closed door

Test Fuel Charge Loading Information:

Test Fuel Charge and Loading Sequence Diagram



FRONT of stove view
4 X 4's: 3, 4
2 X 4's: 1, 2, 5 & 6
Loading Sequence: 1, 2, 3, 4, 5 & 6 last
Driest Pcs in Load 1 & 2

Loaded the test fuel charge on an essentially level, medium
sized, average to hot coal bed (in appearance, color and temperature
for a high burn rate. (Stove was very hot a start, last
flames from preburn fuel had just gone out.)

Load 1105 Ignition at 0135
Grv Balance 2119 100% @ 4100
CO Spike to 0.27% @ N 12100.

FUEL MOISTURE
WOODSTOVE TEST DATA SHEET #10

Unit: HIGH VALLEY X-TEC
Run: EPA #1
Date: 3/20/99
Technician: ATH, PLS.
WST1-Form7-Rev11/89

Room Temperature: 69 °F

Correction Factor: 0

NOTE: Record readings to the nearest 0.5% moisture

Uncor Values are corrected for temperature: Yes No

Time Test Fuel Moisture Readings taken at: 1210

Calibration Checks: X Y 12.5 18.5 22.0 22.2

Pc #	Dimen	Use	Top		Bottom		Side		Piece Avg Corrected
			Uncor	Cor	Uncor	Cor	Uncor	Cor	
1	2x4x8'	K	12.5	13.3	12.0	12.8	12.0	12.8	(12.967) ✓
2									
3									
4	2x4x8'	P	22.0	23.7	22.5	24.3	22.5	24.3	24.100 ✓
5	"	P	19.0	20.3	18.5	19.8	19.0	20.3	20.133 ✓
6	"	P	22.5	24.3	22.5	24.3	22.0	23.7	24.100 ✓
7	"	P	20.5	22.0	21.0	22.6	20.5	22.0	22.200 ✓
8	"	P	22.0	23.7	22.5	24.3	22.0	23.7	23.900 ✓
9									(114.433) ✓
10									
11	2x4x17.0"	T	18.0	19.2	18.0	19.2	18.5	19.8	19.400 ✓
12	"	T	19.5	20.9	19.5	20.9	19.0	20.3	20.700 ✓
13	"	T	21.0	22.6	21.0	22.6	20.0	21.4	22.200 ✓
14	"	T	22.0	23.7	22.0	23.7	22.0	23.7	23.700 ✓
15									
16	4x4x17.0"	T	18.0	19.2	18.0	19.2	18.0	19.2	19.200 ✓
17	"	T	21.5	23.1	21.5	23.1	21.5	23.1	23.100 ✓
18									(128.300) ✓
19	FEET	T	19.0	20.3	18.5	19.8	18.5	19.8	(19.967) ✓
20									(OUT SPACERS) ✓

	Kindling	Pretest Fuel	Test Load
% Moisture - Dry Basis:	12.967% ✓	22.887% ✓	21.383% ✓
% Moisture - Wet Basis:	11.478% ✓	18.624% ✓	17.616% ✓

To obtain Wet from Dry: $\frac{100 \times \% \text{ Dry Rdg.}}{100 + \% \text{ Dry Rdg.}} = \% \text{ Moisture, Wet Basis}$

Acceptable Ranges: 16-20% wet; 19-25% dry
(17.5 - 22.5 on Meter [Uncor reading] at 70°F)

Key for Use: K= Kindling P= Pretest Fuel T= Test Fuel

WOOD DENSITY DETERMINATION
WOODSTOVE TEST DATA SHEET #11

Unit: HIGH VALLEY-X-TEC
Run#: RPA #1
Date: 3/20/99
Technician: ATM, PLS.
WST2-form11-Rev 6/90

Wood Piece: Nominal Dimensions: 3 1/2" x 3 1/2" x 1 1/2"
Depth (D): in 1.555 cm 3.9497 ✓
Width (W): in 3.515 cm 8.9281 ✓
Length (L): 3.503 cm in
3.492 cm in
3.500 cm in
3.482 cm in
Length \bar{X} = in 3.4943 cm 8.8755 ✓
Volume: 312.980 cm³ ✓
(D X W X L)

MOISTURE: Room Temperature: 69 °F Correction Factor: 0

Uncorrected Meter Readings Corrected for temperature: Yes No

NOTE: Record moisture meter readings to the nearest 0.5%

	Uncor	Cor	%
Top:	<u>22.0</u>	<u>23.7</u>	<u>%</u>
Bottom:	<u>22.0</u>	<u>23.7</u>	<u>%</u>
Side:	<u>22.0</u>	<u>23.7</u>	<u>%</u>
\bar{X} :		<u>23.700</u>	<u>%</u>

Avg % Moisture (Dry) 23.700 % ✓

Avg % Moisture (Wet) 19.159 % ✓

Scale: Leveled In Out

Zeroed: In Out

Wet Weight: 158.8 g Dry Weight: 131.6 g

% Moisture Dried Basis: 17.128 % ✓
[1 - (Dry Wt ÷ Wet Wt)] X 100

	Date	Time	Temp	°F
Into Dryer	<u>3/20/99</u>	<u>1155</u>	<u>213</u>	°F
Out of Dryer	<u>3/29/99</u>	<u>1415</u>	<u>218</u>	°F

(Minimum Time in Dryer: 24 hrs.) Minimum Dryer Temp 100°C (212°F)

Density = 131.6 g ÷ 312.980 cm³ = 0.4205 g/cm³ ✓
(dry wt) (volume)

Pellet Fuel Moisture Content Determination

Tare Beaker Wt. _____ g
Wet Wt: _____ g - _____ g = _____ g
Gross Wet Wt. Tare Beaker Wt. Net Wet Wt.
Dry Wt: _____ g - _____ g = _____ g
Gross Dry Wt. Tare Beaker Wt. Net Dry Wt.

% Moisture Dried Basis: _____ %
[1 - (Net Dry Wt ÷ Net Wet Wt.)] X 100

TEMPERATURES
 RECORD SHEET #14
 WST2-Form14 Rev7/96

Site: HIGH VALLEY X-TEC Date: 3/20/99
 Run: EPA #1 Technician(s): ATM, PLS.
 Page: 1 of 1

T/C#	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
Minute/Time	Stove Top	Left Side	Back	Right Side	Bottom	Firebox	2nd Burn Catalyst	Room Temp	Tunnel	C. Gas Box	Impinger Out	5G-1 Filter	5G-1 Condenser	Con- dar	
0	589	583	564	637	561	1052	1211	78	147	248	44	88	58	248	
5	625	585	552	624	567	1057	1296	79	181	248	45	89	39	248	
10	770	589	476	616	560	1000	1330	78	187	257	45	89	39	248	
15	841	590	439	609	545	1040	1504	78	190	257	45	89	39	248	
20	860	591	422	611	528	1062	1395	78	188	257	44	89	39	250	
25	840	594	418	618	573	1058	1430	79	182	252	45	89	39	250	
30	796	597	420	630	501	1050	1502	79	177	257	45	89	40	250	
35	765	597	430	643	494	1058	1464	79	176	249	45	89	40	249	
40	779	597	448	657	487	1092	1447	79	173	248	44	89	40	250	
45	746	597	470	667	483	1066	1428	78	167	248	44	89	40	257	
50	705	593	492	670	480	1058	1305	79	161	250	44	89	39	252	
55	669	587	507	670	480	1041	1291	79	157	250	44	89	39	257	
60	8978	7100	5638	7652	6199	11228	16603	943							
60	638	568	521	670	481	1025	1206	76	149	250	44	88	38	250	
65	606	567	540	665	481	1013	1162	76	148	249	44	88	39	250	
70	591	560	568	658	487	1009	1170	75	146	250	45	88	39	250	
75	564	560	580	649	498	989	1082	75	139	250	45	87	39	250	
80	531	557	573	637	509	964	1026	76	135	250	45	86	39	250	
85	503	537	553	626	576	933	990	75	133	250	45	86	39	250	
90	480	528	538	616	523	913	965	75	131	250	46	85	39	250	
95	463	516	534	604	529	906	949	74	128	250	46	85	39	249	
100	448	507	527	595	533	901	932	74	126	249	46	85	39	250	
105	435	497	578	587	532	890	933	72	124	249	46	84	39	249	
110	425	490	508	579	530	879	915	71	123	249	46	84	39	248	
116	413	480	499	572	530	861	887	69	121	248	46	84	39	248	
120	6097	6363	6459	7458	6149	11283	12817	888							
125	15075	13463	13093	15110	12348	23911	18820	1831							
130	1288	1214	1214	1220	1252	1201	1217	121							

AVG. STOPNE TEMP. CHANGE START STOP AT

PRE AND POST TEST ZERO/SPAN CHECK
WOODSTOVE DATA SHEET #15-1

Site: Myren Consulting, Woodinville, WA Date: 3/20/99 Analyte: CO₂

Source: HIGH VALLEY X-TEC Run #: EPA #1

Zero Cyl #: 36919 Conc. 00.0 % CO₂ Cyl Press: 250 psi

Certified by: CASCADE AIRGAS Date: 4/24/96

Span Cyl #: 250-1060 Conc. 6.0 % CO₂ Cyl Press: 1480 psi

Certified by: OXARC Date: 8/22/97

Analyzer: Make: Horiba Model: PIR-2000 SN: 607024

Range: 0 - 25.0% CO₂ Analyzer Output: 0 - 1.0 v.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter:

EPA Span Value = 25.0% CO₂

EPA Control Limits = + 2.5% of 25.0% CO₂ = + 0.625% CO₂

Pre Run Audit: By: RLS, ATM Time: 1320 Temp: 78 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	00.0	.000	.0256	+0.0256	+0.10
Span	24.0	.240	6.0	06.0	.240	5.991	-0.0093	-0.15

Comments:

Post Run Audit: By: RLS, ATM Time: 1650 Temp: 73 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	00.0	.000	.0256	+0.0256	+0.10
Span	24.0	.240	6.0	05.9	.239	5.966	-0.0341	-0.57

Comments:

+ Conc. Difference = Act % - Exp (Std) %

Zero % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$

Span % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

PRE AND POST TEST ZERO/SPAN CHECK
WOODSTOVE DATA SHEET #15-2

Site: Myren Consulting, Woodinville, WA Date: 3/20/99 Analyte: O₂

Source: HIGH VALLEY X-TEC Run #: EPA #1

Zero Cyl #: 36919 Conc. 00.0 % O₂ Cyl Press: 250 psi

Certified by: CASCADE AIRGAS Date: 4/24/96

Span Cyl #: 250-1060 Conc. 6.0 % O₂ Cyl Press: 1480 psi

Certified by: OxARC Date: 8/22/97

Analyzer: Make: Taylor Model: OA 137 SN: 137/4772

Range: 0 - 25.0% O₂ Analyzer Output: 0 - 100 mv.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter:

EPA Span Value = 25.0% O₂

EPA Control Limits = + 2.5% of 25.0% O₂ = + 0.625% O₂

Pre Run Audit: By: RLS, ATM Time: 1320 Temp: 78 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ%
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	00.0	00.0	-0.155	-0.155	-0.06
Span	6.0	24.0	6.0	06.0	23.9	5.981	-0.195	-0.32

Comments:

Post Run Audit: By: RLS, ATM Time: 1650 Temp.: 73 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ%
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	00.0	00.0	-0.155	-0.155	-0.06
Span	6.0	24.0	6.0	06.0	23.9	5.981	-0.195	-0.32

Comments:

+ Conc. Difference = Act % - Exp (Std) %

Zero % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$

Span % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

PRE AND POST TEST ZERO/SPAN CHECK
WOODSTOVE DATA SHEET #15-3

Site: Myren Consulting, Woodinville, WA Date: 3/20/99 Analyte: CO

Source: HIGH VALLEY X-TEC Run #: EPA # 1

Zero Cyl #: 36919 Conc. 00.0 % CO Cyl Press: 250 psi

Certified by: CASCADE AIRGAS Date: 4/24/96

Span Cyl #: 250-1060 Conc. 1.26 % CO Cyl Press: 1480 psi

Certified by: OXARC Date: 8/22/97

Analyzer: Make: Infra Red Model: 702 D SN: 113

Range: 0 - 10.0% CO Analyzer Output: 0 - 100 mv.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter:

EPA Span Value = 5.0% CO

EPA Control Limits = +2.5% of 5.0% CO = + 0.125% CO

Pre Run Audit: By: RLS, ATM Time: 1320 Temp: 78 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.00	00.0	0.0091	-0.0091	-0.18
Span	1.26	25.2	1.26	1.26	24.8	1.2467	-0.0140	-1.11

Comments:

Post Run Audit: By: RLS, ATM Time: 1650 Temp.: 73 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.00	00.0	0.0091	-0.0091	-0.18
Span	1.26	25.2	1.26	1.25	24.7	1.2417	-0.0183	-1.45

Comments:

+ Conc. Difference = Act % - Exp (Std) %

Zero % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$

Span % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

Unit: HIGH VALLEY X-TEC
 Run: EPA #1
 Date: 3/20/99
 Technicians: ATH, PLS.
 WST6-Form3-Rev11/89

QUALITY CHECKS
 WOODSTOVE DATA SHEET #16

Ambient = Tr: _____ °F T/C#30: _____ °F
 Thermocouple Check (at ambient): T/C#1: 73 °F; T/C#2: 75 °F;
 T/C #3: 619 °F; T/C #4: 410 °F; T/C #5: 102 °F;
 T/C #6: 103 °F; T/C #7: 106 °F; T/C #8: 87 °F;
 T/C #9: 208 °F; T/C #10: 1293 °F; T/C #11: 69 °F;
 T/C #12: 74 °F; T/C #13: 72 °F; T/C #14: 65 °F;
 T/C #15: 68 °F; T/C #16: 69 °F; T/C #17: 71 °F;
 T/C #18: _____ °F; T/C #19: _____ °F; T/C #20: _____ °F;
 T/C #21: _____ °F; T/C #22: _____ °F; T/C #23: _____ °F;
 T/C #24: _____ °F; T/C #25: _____ °F; T/C #26: _____ °F;

Comments: STOVE ALREADY LIT.

Thermocouple Readout: Pretest Zero/Span Check and Calibration:
 Zero Adj Post Test Check % Difference
 (0°F) : 000 °F to: 000 °F Zero (0°F): 000 °F +0
 Span Adj Span
 (2000°F): 1999 °F to: 2000 °F (2000°F): 2000 °F 0

(Allowable % Difference = 1.5%. Use formulas on Woodstove Data Sheet #15 to calculate % Difference)

Thermocouple Readout Pretest Linearity Check

0°F = 000 °F; 200°F = 200 °F; 400°F = 399 °F;
 600°F = 599 °F; 800°F = 800 °F; 1000°F = 1000 °F;
 1200°F = 1200 °F; 1400°F = 1400 °F; 1600°F = 1600 °F
 1800°F = 1800 °F; 2000°F = 2000 °F

Combustion Gas (CO₂, O₂, CO) Train Leak Check: Pre Post
 Draft (Static) Gauge Zero Check: Pre Post

Scale Check Pre (Wt, #'s): 608.6 - 613.6 5.0 lbs, OK (PLS)
 Post (Wt, #'s): 608.0 - 613.0 5.0 lbs, OK (PLS)

Stack cleaned prior to the run: Yes No _____
 Tunnel cleaned prior to the run: Yes No _____

DILUTION TUNNEL CALCULATIONS
3/31/96

MYREN CONSULTING CERTIFICATION TEST DATA

File Name: hivalleyepa5

Stove Manufacturer: HI VALLEY

Model Number: XTEC

Lab Name: MYREN

Test Date: 3/29/99

Run Number: EPA 5

Meter Box Y Factor: 1.003

Barometric pressure (in): 28.4

Gas meter temp (ave): 80

delta H(ave): 0.900

Gas meter initial reading: 444.104

Gas meter final reading: 616.826

Front catch (acetone) mg: 5.9

first filter catch (mg): 12.7

second filter catch (mg): -0.5

tunnel flow (ave cfm): 140.918

Emission Rate(g/hr): 0.953

Emission Rate(M5H) : 1.749

vs/MtTs: 0.0093

vs ave: 834.763

Tunnel average temp (°f): 99.250

Test time(min): 310

Fuel Load(lb. wet): 17.2

Wood moisture(%wet): 17.492

Burn rate(dry kg/hr): 1.246

Samp vol(scf): 160.913

front filter number: 782

back filter number: 781

acetone beaker number: 4

PRELIMINARY RESULTS

FINAL RESULTS

AUDITED

DATA SUMMARY

MODEL : XTEC

RUN: EPA 5

DATE: 3/29/99

DBR: 1.246

GPH UNADJ: 0.953

ADJ: 1.749288386

RUN TIME (min)	PITOT DELTAP (- INCH H2O)	TNL TEMP (°F)	GAS METER RDG (ft3)	GAS METER TEMP (°F)	GAS METER DELTA H (in.H2O)	TUNNEL VELOCIT (ft/min)	PROP RATE (%)	dDGM vol std (ft3)
0	0.040	105	444.104	71	0.900	847.65		
10	0.040	126	449.655	72	0.900	863.26	104.5	5.255
20	0.038	121	455.168	74	0.900	837.81	100.6	5.200
30	0.038	123	460.677	75	0.900	839.25	103.8	5.186
40	0.037	123	466.182	77	0.900	828.13	103.1	5.163
50	0.037	122	471.703	78	0.900	827.42	104.5	5.168
60	0.037	121	477.227	79	0.900	826.71	104.2	5.162
70	0.037	118	482.747	79	0.900	824.57	103.7	5.158
80	0.037	115	488.298	80	0.900	822.43	103.8	5.177
90	0.038	110	493.848	81	0.900	829.84	103.0	5.167
100	0.039	107	499.403	82	0.900	838.47	101.4	5.162
110	0.039	104	504.966	82	0.900	836.25	100.0	5.169
120	0.039	101	510.537	82	0.900	834.02	99.9	5.177
130	0.039	99	516.106	82	0.900	832.53	99.7	5.175
140	0.040	96	521.684	82	0.900	840.87	99.5	5.183
150	0.040	95	527.273	82	0.900	840.12	98.6	5.194
160	0.040	93	532.865	82	0.900	838.60	98.4	5.196
170	0.040	91	538.447	82	0.900	837.08	98.0	5.187
180	0.040	90	544.045	82	0.900	836.32	98.3	5.202
190	0.040	89	549.635	82	0.900	835.56	98.1	5.194
200	0.040	88	555.238	82	0.900	834.80	98.2	5.207
210	0.040	86	560.835	82	0.900	833.28	97.8	5.201
220	0.040	86	566.432	82	0.900	833.28	98.0	5.201
230	0.040	85	572.037	82	0.900	832.51	98.0	5.208
240	0.040	85	577.715	82	0.900	832.51	99.3	5.276
250	0.040	86	583.238	82	0.900	833.28	96.8	5.132
260	0.040	86	588.838	82	0.900	833.28	98.1	5.204
270	0.040	86	594.431	82	0.900	833.28	97.9	5.197
280	0.040	85	600.135	82	0.900	832.51	99.7	5.300
290	0.040	85	605.695	82	0.900	832.51	97.3	5.167
300	0.040	85	611.225	82	0.900	832.51	96.7	5.139
310	0.040	84	616.826	82	0.900	831.75	97.8	5.205
320						0.00	0.0	0.000
330						0.00	0.0	0.000
340						0.00	0.0	0.000
350						0.00	0.0	0.000

DATE 3/29/99

PAGE 1 OF 2

MODEL # HIGH VALLEY X-TEC

RUN # EPA # 5

METER BOX # 571 M

METER Y 1.003

FILTER # (F) 782 (R) 781

PRE TEST LEAK RATE = .0015 CFM @ -15.5 IN. HG .655/.6565

FILTER SIZE: 110 MM

POST TEST LEAK RATE = .001 CFM @ -10.0 IN. HG

PROBE LENGTH 24" GLASS

TIME		METER READING CU. FT.	PITOT dp	TNL TEMP. (°F)	METER TEMP. (°F)	GAS METER dh	VAC IN. Hg	VELOCITY TRAVERSE			
CLOCK	ELAPSED							POINT	LOCATION	ΔP	TEMP
1570	00	444.104	-040	105	71	.90	0	N-1	0.5"	-.035	115
20	10	449.655	-040	126	72	.90	0	2	1.5"	-.044	116
30	20	455.168	-038	121	74	.90	0	3	4.5"	-.041	116
40	30	460.677	-038	123	75	.90	0	4	5.5"	-.035	115
50	40	466.182	-037	123	77	.90	0	W-1	0.5"	-.035	116
1600	50	471.703	-037	122	78	.90	0	2	1.5"	-.043	116
10	60	477.227	-037	121	79	.90	0	3	4.5"	-.040	116
20	70	482.747	-037	118	79	.90	0	4	5.5"	-.036	117
30	80	488.298	-037	115	80	.90	0	Avg. <u>.03863</u> <u>115.88</u>			
40	90	493.848	-038	110	81	.90	0	Pilot Leak Check Pre <input checked="" type="checkbox"/> Post <input checked="" type="checkbox"/>			
50	100	499.403	-039	107	82	.90	0	Cp = <u>0.99</u> N			
1700	10	504.966	-039	104	82	.90	0	→ W 1 2 <u>3</u> 4			
10	20	510.537	-039	101	82	.90	0	* - point of Avg. delta p			
20	30	516.106	-039	99	82	.90	0	Qs = $\left(\frac{\sqrt{(\Delta P \times BP)}}{T(^{\circ}R)}\right) \times 3167.2 =$			
30	40	521.684	-040	96	82	.90	0	<u>138.779</u> cfm			
40	50	527.273	-040	95	82	.90	0	BP = <u>START 28.42</u> in Hg			
50	60	532.865	-040	93	82	.90	0	60 <u>28.41</u>			
1800	70	538.447	-040	91	82	.90	0	120 <u>28.40</u>			
10	80	544.045	-040	90	82	.90	0	180 <u>28.39</u>			
20	90	549.635	-040	89	82	.90	0	240 <u>28.38</u>			
								300 <u>28.40</u>			

13.4 - .3

$\bar{X} = 28.400$

DATE 3/29/99

PAGE 2 OF 2

MODEL # HIGH VALLEY X-TEC

RUN # EPA # 5

METER BOX # 571 M

METER Y 1,003


FILTER # (F) 782 (R) 781

PRE TEST LEAK RATE = .0015 CFM @ -15.5 IN. HG. .6557/.6565

FILTER SIZE: 110 MM

POST TEST LEAK RATE = .001 CFM @ -10.0 IN. HG. .835/.836

PROBE LENGTH 24" GLASS

TIME		METER READING CU. FT.	PITOT dp	TNL TEMP. (°F)	METER TEMP. (°F)	GAS METER dh	VAC IN. Hg	VELOCITY TRAVERSE			
CLOCK	ELAPSED							POINT	LOCATION	ΔP	TEMP
1830	2:00	555.238	-040	88	82	.90	0	N-1	0.5"	-035	115
40	10	560.835	-040	86	82	.90	0	2	1.5"	-044	116
50	20	566.432	-040	86	82	.90	0	3	4.5"	-041	116
1900	30	572.037	-040	85	82	.90	0	4	5.5"	-035	115
10	40	577.715	-040	85	82	.90	0	W-1	0.5"	-035	116
20	50	583.238	-040	86	82	.90	0	2	1.5"	-043	116
30	60	588.838	-040	86	82	.90	0	3	4.5"	-040	116
40	70	594.431	-040	86	82	.90	0	4	5.5"	-036	117
50	80	600.135	-040	85	82	.90	0	Avg. <u>.03863</u> <u>115.9</u>			
2000	90	605.695	-040	85	82	.90	0	Pilot Leak Check Pre <input checked="" type="checkbox"/> Post <input checked="" type="checkbox"/>			
10	3:00	611.225	-040	85	82	.90	0	Cp = <u>0.99</u> N 1 2 3 4			
20	10	616.826	-040	84	82	.90	0	→ W 1 2 			
30	20							*-point of Avg. delta p			
40	30							Qs = $\left(\frac{\sqrt{(\Delta P \times BP)}}{T(^{\circ}R)}\right) \times 3167.2 =$			
50	40							<u>138,279</u> cfm			
2100	50							BP = Static <u>28.42</u> in Hg			
10	60							60 <u>28.41</u>			
20	70							120 <u>28.40</u>			
30	80							180 <u>28.39</u>			
40	90							240 <u>28.38</u>			
								300 <u>28.40</u>			

$\bar{X} = 28.40$

WOODSTOVE DATA SHEET #4-4
SCALE QA SHEET

Scale Mettler
Model AE100
SN K04827

Dates From 1/9/99
Through _____

Level	Recalibrated	100g Weight	10g Weight	1.0g Weight	100mg Weight	20mg Weight	Date	Time	Tech	Wet Bulb	Dry Bulb	% RH
✓	Yes	99.9999	10.0001	1.0002	1.003	.0203	1/9/99	1243	ATM	58	70	48
✓	No	100.0002	10.0000	1.0000	1.000	.0200	1/14/99	1113	ATM	62	75	47
✓	YES	99.9998	10.0002	1.0000	.9999	.0201	1/23/99	1100	ATM	63	77	43
✓	YES	99.9998	10.0000	1.0000	1.000	.0201	1/24/99	1318	ATM	59	74	45
✓	YES	99.9996	10.0002	1.0000	1.000	.0200	2/1/99	0910	ATM	55	69	39
✓	YES	99.9997	10.0001	1.0001	1.002	.0201	2/2/99	0939	ATM	60	73	46
✓	YES	99.9999	10.0001	1.0001	1.001	.0201	2/3/99	1555	ATM	63	76	48
✓	YES	99.9999	10.0000	1.0001	1.001	.0201	2/7/99	1235	ATM	62	76	45
✓	YES	99.9998	10.0000	1.0000	1.000	.0200	2/10/99	1600	ATM	63	77	45
✓	YES	99.9998	10.0000	1.0001	1.000	.0200	2/19/99	0246	ATM	64	78	46
✓	No	99.9999	10.0000	1.0000	1.000	.0200	2/21/99	1312	ATM	65	80	44
✓	No	99.9997	10.0000	1.0001	1.000	.0200	3/5/99	1935	ATM	64	80	41
✓	YES	99.9997	10.0000	1.0000	1.001	.0200	3/6/99	1135	ATM	64	79	43
✓	YES	99.9997	10.0000	1.0001	1.000	.0200	3/13/99	1526	ATM	65	80	44
✓	YES	99.9999	10.0001	1.0001	1.001	.0200	3/14/99	1355	ATM	63	78	43
✓	No	100.0001	10.0000	1.0000	1.000	.0200	3/16/99	1622	ATM	66	81	45
✓	Yes	99.9997	10.0000	1.0001	1.000	.0200	3/16/99	2025	ATM	65	82	39
✓	Yes	99.9996	10.0000	1.0001	1.001	.0200	3/17/99	1615	ATM	63	77	44
✓	Yes	99.9997	10.0000	1.0001	1.000	.0200	3/18/99	2140	ATM	68	84	43
✓	Yes	99.9998	10.0000	1.0000	1.000	.0200	3/20/99	1300	ATM	64	84	32
✓	Yes	99.9999	10.0000	1.0001	1.001	.0201	3/21/99	2215	ATM	61	74	47
✓	Yes	99.9997	10.0000	1.0000	1.001	.0200	3/22/99	2127	ATM	65	85	33
✓	Yes	99.9997	10.0000	1.0001	1.000	.0200	3/23/99	1115	ATM	69	84	46
✓	Yes	99.9998	10.0000	1.0002	1.001	.0201	3/24/99	1120	ATM	77	89	43
✓	Yes	99.9999	10.0000	1.0002	1.001	.0201	3/29/99	2038	ATM	89	72	45
✓	No	99.9999	10.0002	1.0002	1.001	.0201	3/30/99	0610	ATM	66	80	47
✓	No	99.9999	10.0000	1.0000	1.001	.0201	3/31/99	1200	Sum	64	80	41
✓	No	99.9996	10.0000	1.0000	1.001	.0201	4/3/99	1730	ATM	64	80	41
✓	Yes	99.9998	10.0001	1.0001	1.001	.0201	4/6/99	1030	ATM	61	75	44
QC Services	Audit	4/6/97	-	-	-	-	Scale checked					
✓	No	100.0003	10.0001	1.0001	1.001	.0201	4/6/99	1730	ATM			33
✓	Yes	99.9999	10.0001	1.0001	1.001	.0200	4/7/99	1724	ATM	65	85	33
✓	No	99.9996	10.0000	1.0001	1.001	.0201	4/8/99	1346	ATM	67	80	50
✓	Yes	99.9997	10.0000	1.0000	1.000	.0200	4/16/99	1230	ATM	66	82	42
✓	Yes	99.9997	10.0000	1.0000	1.000	.0200	4/17/99	1625	ATM	68	84	43

Woodstove Particulate
 Catch Processing Sheet
 Woodstove Data Sheet #5
 EPA M5G-1

Unit: Hi Valley
 Run: EPA 5
 Date: 3/29/99
 Technicians: ATM
 Revised 1/16/98-Data Sheet #5

Filters

Filter # (Front) 782 Beaker # 4
 Final Wt. .8030 g MI 60
 Tare Wt. .7903 g Desc. Acetone
 Net Wt. .0127 g

Final Wt. 67.5946 g ✓
 Tare Wt. 67.5886 g ✓
 Net Wt. .0060 g ✓

Filter # (Rear) 781 Beaker # _____
 Final Wt. .7887 g MI _____
 Tare Wt. .7892 g Desc. _____
 Net Wt. -.0005 g ✓

Final Wt. _____ g
 Tare Wt. _____ g
 Net Wt. _____ g

Acetone Blank Calculation: Blank Date: 3/13/99
 Blank Beaker # 8 Final Wt. 66.0215 g
 MI 100 Tare Wt. 66.0213 g
 Desc. Acetone Net Wt. .0002 g
.0002 g ÷ 100 ml = .000002 g/ml

Blank Residue Value Calculation:
.000002 g/ml acetone X 60 ml acetone = .00012 g
 Blank Residue Value

Total Particulate Catch Calculation

Filter: .0127 g
 Filter: -.0005 g
 Beakers: .0060 g - .0001 g = .0059 g
 Total Catch Blank Residue Value
 Total Catch = .0181 g

Unit HIGH VALLEY X-TEC
 Run # EPA # 5
 Date 3/29/99
 Technician ATM, PLS.
 WST6-Form1, Rev8/96

MISCELLANEOUS TEST DATA
 WOODSTOVE DATA SHEET #8

Useable Firebox Dimensions: See QC Section Useable Volume: 2.713 ft³

Dilution Tunnel Draft (If applicable): Start 00.0 Stop 00.0

Test Chamber Air Velocity: Start: 00.0 Stop: 00.0 Avg: 00.0

Wet Bulb/ Start: WB: 55 °F DB: 67 °F 1.0 % Amb Moisture 45 %RH

Dry Bulb Stop: WB: 59 °F DB: 72 °F 1.25 % Amb Moisture 45 %RH

$\bar{x} = 1.125$ % Ambient Moisture $\bar{x} = 45$ % Relative Humidity (RH)

Empty

Stove Wt:

514.0 lbs.

Empty

Stove Wt with Stack (Inc. Oil Seal) Wet: 607.5 lbs. Dry: 605.0 lbs.

Empty

Stove Wt with Stack and Ash Ash: 0 lbs. Total: 605.0 lbs.

Kindling Wt.

Paper: 0.3 lbs. Wood: 5.0 lbs.

Pre Burn Fuel Wt. 16.6 + 17.3 + 16.2 + 5.1 Total: 55.2 lbs. ✓

Total Kindling and Pre Burn Fuel Wt 60.5 lbs. ✓

Coal Bed Wt-lbs: Range (609.3 - 608.5) 4.3 - 3.5 lbs. Actual: 3.5 lbs. ✓

Allowable Amount of Charcoal that can be removed:

Coal Bed Wt. Range $\frac{4.3}{\text{Upper Wt.}} + \frac{3.5}{\text{Lower Wt.}} \times 12 \times .25 = \underline{1.9}$ lbs. ✓

Test Fuel Wt-lbs: Ideal 19.0 lbs. Range: 17.1 - 20.8 lbs. Actual: 17.2 lbs.

Test Fuel Size (pcs.) (.75 x 1.5 x 5" Flanges) 20 Pcs.

2 x 4's x 17 1/8 " 4 Pcs 9.0 lbs. 52.3 % ✓

4 x 4's x 17 1/8 " 2 Pcs 8.2 lbs. 47.7 % ✓

Est. Dry Burn Rate (Kg/Hr.) $\frac{17.2 - (17.2 \times .17492)}{2.2046} \times \frac{60}{310} = \underline{1.246}$ Est. Dry Burn Rate (Kg/Hr)

Est EPA Heat Output (HO_E) (Avg BTU's/Hr) $(19,140) \times \frac{63}{100} \times 1.246 = \underline{15,023}$ Est Heat Output (HO_E) BTU's/Hr

Comments:

Stove Operating Data
Woodstove Test Data Sheet #9
Cold Start

Unit: HIGH VALLEY X-TEC
Run: EPA #5
Date: 3/29/99
Technician(s): ATM RLS,
Data Sheet #9 - Rev 1/98-Pg.1

Fire Started: 0945 P.S.T.

Warm up and Preburn: Primary Air: Wide open from ignition until the start of preburn when the primary air control(s) was (were) adjusted to the run setting of 1 1/16" OPEN. At the run setting until the start of the test.

Secondary Air: No Controls, Naturally drafted

Secondary Burn/Cat Bypass: N/A

Charcoal Bed Preparation: Broke up, raked and leveled the coal bed prior to the addition of each warm up/pre burn fuel charge. Starting 1:30 before the start of the test, broke up, raked and leveled the coal bed. In stove for 25 seconds.

Test: Door wide open during loading 1 min 10 sec, then closed

Primary Air: Wide open during the start of the test until 4:30. Adjusted to the run setting of 1 1/16" between 4:25 and 4:30. At the run setting of 1 1/16" at 4:30 into the run.

Secondary Air: No Controls, Naturally drafted, Stand

Secondary Burn/Cat Bypass: N/A

Fan: OFF, Fan Confirmation Test

Test Run Anomalies:

The FCT should have been run at either 1" or 7/8" - perhaps even 3/4".

WOODSTOVE OPERATING DATA
 WOODSTOVE DATA SHEET #9A-1

Wood Data: Kindling: A mix of the below grades

	Size	Mill	Grade	Species
Pre Burn	<u>2x4</u>	<u>CANYON LBR.</u>	<u>STD. & BTR.</u>	<u>D. FIR, S. GRN.</u>
Test Fuel	<u>2x4</u>	<u>CANYON LBR.</u>	<u>#2 STD. & BTR.</u>	<u>D. FIR, S. GRN.</u>
	<u>4x4</u>	<u>STAND. & 879</u>	<u>#2 STD. & BTR.</u>	<u>D. FIR, S. GRN.</u>

All grades WCLB Rules unless otherwise noted.

Warm up Information:

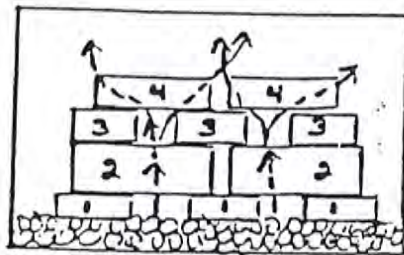
1st Warm up/Pre Burn Fuel charge (16.6 lbs) added at 1005.
 2nd Warm up/Pre Burn Fuel charge (17.3 lbs) added at 1115.
 3rd Warm up/Pre Burn Fuel charge (16.2 lbs) added at 1223.
 4th Warm up/Pre Burn Fuel charge (5.1 lbs) added at 1341.
 5th Warm up/Pre Burn Fuel charge (____ lbs) added at ____.
 6th Warm up/Pre Burn Fuel charge (____ lbs) added at ____.
 7th Warm up/Pre Burn Fuel charge (____ lbs) added at ____.
 8th Warm up/Pre Burn Fuel charge (____ lbs) added at ____.

The coals were scooped out of the stove immediately prior to adding the 3rd pre burn/warm up fuel charge. The stove lost 2.5 lbs. 3.0 lbs of coals back in after scoop.

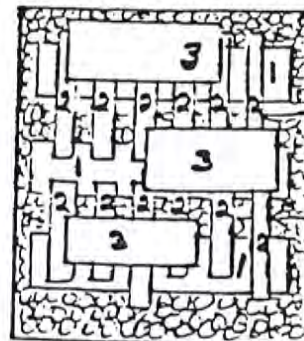
All pre burn/warm up fuel pieces were either 16 or _____ inches long. All preburn pieces/fuel charges were "ricked" in the stove. The pieces in the bottom layer in each rick contained 2 pcs that were 16 inches long and were loaded flat and perpendicular to the door. The pieces in the second layer in each rick were loaded on their side (edge) approximately parallel to the door and contained 4 pcs 16 inches long. The third layer (and fourth layer if present) was loaded flat, perpendicular to the door and contained 3 pcs 16 inches long. The majority of the pieces in each rick were in the second layer which had an approximate 0.5-1.0" space between pieces. (The loading directions indicate the direction of the longest dimension on each piece relative to the loading door opening.) Each pre burn/warm up fuel charge normally weighs within the weight range allowed for the actual test fuel charge

Warm up Information (cont.):

Each warm up/preburn fuel charge was ricked in exactly (as much as possible) the same manner and the weight of each rick was usually within the allowable weight range for the test fuel charge. The physical arrangement and alignment of each rick was designed to accomplish three (3) things: (1) The bottom layer was nestled firmly into the coal bed and was as close to being level with the bottom of the stove as possible, thus providing a stable loading platform for the rest of the rick, keeping it in a ricked state (as opposed to a collapsed or fallen down state) until the rick reached the charcoal stage and sags or collapses of its own accord. (2) It enhances the flow of primary air through the ricked preburn fuel charge, for the primary air would flow through the spaces between the pieces in the first layer and then up through the spaces between the pieces in the second, third and, if present, fourth layers. (3) It maximized, as much as possible, the surface to volume ratio of each preburn fuel charge, thereby allowing the fire immediate access to as much wood surface as possible and, thereby, insuring uniform charcoalization. All three of these enhance combustion and so get the stove as hot as possible during the warm up period, thereby maximizing the amount of heat (BTU's) stored in the stove. The actual preburn was not started until the stove surface temperatures had maximized and stabilized, thus indicating that the amount of heat stored in the stove had peaked. For this stove, the thermal storage was monitored using the TOP surface temperature(s) and the peak value(s) obtained were 940 of.



Front View



Top View

The arrows indicate the direction of the air flow through the rick.

The primary air was adjusted to the run setting of 1/16" open 6.0 lbs above the upper charcoal bed weight.

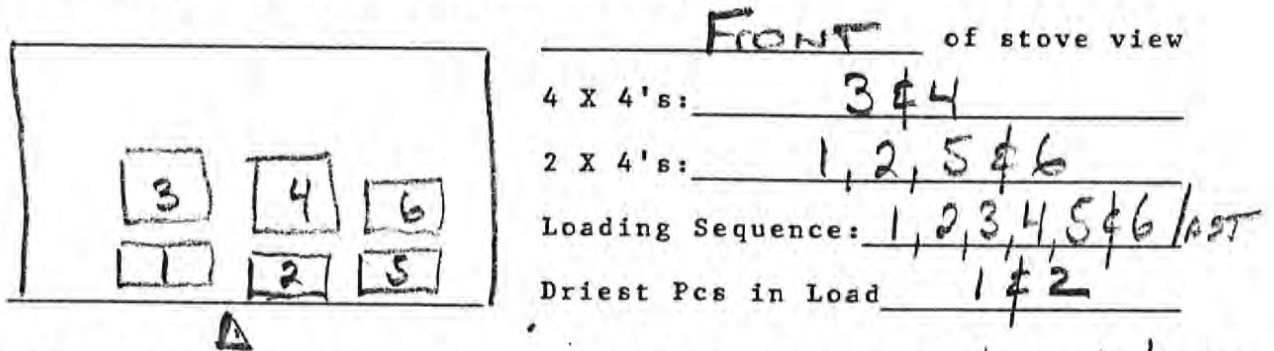
WOODSTOVE OPERATING DATA
WOODSTOVE DATA SHEET #9A-3

Unit HIGH VALLEY X-TEC
Run # EPA #5
Date 3/29/99
Technician ATH, RLS
Page 3 of 3
WST5-Form2-Rev11/89

Additional Comments: Test Start Sequence: ① Opened primary air control wide open. ② Opened door. ③ Loaded test fuel charge into the stove ④ cleared coals from left front of LPAO ⑤ Photograph ⑥ closed door

Test Fuel Charge Loading Information:

Test Fuel Charge and Loading Sequence Diagram



Loaded the test fuel charge on an essentially level, medium to large sized, hot coal bed (in appearance, color and temperature for a Med. Low burn rate. Load 1110. Denition NO145, Gas Balance 2105. Set PAC at 4130. Maintained gas balance, VC to baffle with secondaries on the top of the VC. 2nd's also on top of 3 & 4. VC on h. side of h. stack and in right canyon as well as in left canyon. 7:50 secondaries full width of fuel load.

FUEL MOISTURE
WOODSTOVE TEST DATA SHEET #10

Unit: HIGH VALLEY X-TEC
Run: EPA #5
Date: 3/29/99
Technician: ATM, PLS.
WST1-Form7-Rev11/89

Room Temperature: 69 °F

Correction Factor: 0

NOTE: Record readings to the nearest 0.5% moisture
Uncor Values are corrected for temperature: Yes No
Time Test Fuel Moisture Readings taken at: 1120 ✓
Calibration Checks: X Y 12.5 12.5 22.0 22.2

Pc #	Dimen	Use	Top		Bottom		Side		Piece Avg Corrected
			Uncor	Cor	Uncor	Cor	Uncor	Cor	
1	2x4x8'	K	12.5	13.3	12.5	13.3	12.0	12.8	(13.133)
2									
3									
4	2x4x8'	P	22.0	23.7	22.0	23.7	21.5	23.1	23.500
5	"	P	21.5	23.1	21.5	23.1	21.5	23.1	23.100
6	"	P	21.0	22.6	21.0	22.6	21.0	22.6	22.600
7	"	P	21.5	23.1	22.0	23.7	21.5	23.1	23.300
8	"	P	21.5	23.1	22.0	23.7	21.5	23.1	23.300
9									(115.800)
10									
11	2x4x17 1/2"	T	18.0	19.2	18.0	19.2	18.0	19.2	19.200
12	"	T	18.5	19.8	18.0	19.2	18.0	19.2	19.400
13	"	T	19.0	20.3	19.0	20.3	19.5	20.9	20.500
14	"	T	22.0	23.7	22.0	23.7	22.0	23.7	23.700
15									
16	4x4x17 1/2"	T	19.5	20.9	19.5	20.9	19.0	20.3	20.700
17	"	T	22.0	23.7	22.0	23.7	22.0	23.7	23.700
18									(127.200)
19	FEET	T	19.0	20.3	19.0	20.3	18.5	19.8	(20.133)
20									(OUT SPACERS)

	Kindling	Pretest Fuel	Test Load
% Moisture - Dry Basis:	13.133 % ✓	23.160 % ✓	21.200 % ✓
% Moisture - Wet Basis:	11.609 % ✓	18.805 % ✓	17.492 % ✓

To obtain Wet from Dry: $\frac{100 \times \% \text{ Dry Rdg.}}{100 + \% \text{ Dry Rdg.}} = \% \text{ Moisture, Wet Basis}$

Acceptable Ranges: 16-20% wet; 19-25% dry
(17.5 - 22.5 on Meter [Uncor reading] at 70°F)

Key for Use: K= Kindling P= Pretest Fuel T= Test Fuel

WOOD DENSITY DETERMINATION
WOODSTOVE TEST DATA SHEET #11

Unit: HIGH VALLEY X-TEC
Run#: EPA #5
Date: 3/29/99
Technician: ATM, RLS.
WST2-Form11-Rev 6/90

Wood Piece: Nominal Dimensions: 3 1/2" x 3 1/2" x 1 1/2"
Depth (D): in. 1.560 cm 3.962 ✓
Width (W): in. 3.540 cm 8.992 ✓
Length (L): 3.530 cm in, ✓
3.530 cm " ✓
3.536 cm " ✓
3.542 cm " ✓
Length \bar{X} = in. 3.535 cm 8.978 ✓
Volume: 319.853 cm³ ✓
(D X W X L)

MOISTURE: Room Temperature: 69 °F Correction Factor: 0
Uncorrected Meter Readings Corrected for temperature: Yes No

NOTE: Record moisture meter readings to the nearest 0.5%

	Uncor	Cor	%
Top:	<u>20.0</u>	<u>21.4</u>	%
Bottom:	<u>20.0</u>	<u>21.4</u>	%
Side:	<u>20.5</u>	<u>22.0</u>	%
\bar{X} :		<u>21.600</u>	% ✓

Avg % Moisture (Dry) 21.600 % ✓
Avg % Moisture (Wet) 17.763 % ✓
Scale: Levelled In Out
Zeroed: In Out

Wet Weight: 176.3 g Dry Weight: 146.3 g

% Moisture Dried Basis: 17.016 % ✓
[1 - (Dry Wt ÷ Wet Wt)] X 100

	Date	Time	Temp	OF
Into Dryer	<u>3/29/99</u>	<u>1140</u>	<u>214</u>	OF
Out of Dryer	<u>4/5/99</u>	<u>1130</u>	<u>215</u>	OF

(Minimum Time in Dryer: 24 hrs.) Minimum Dryer Temp. 100°C (212°F)

Density = 146.3 g (dry wt) ÷ 319.853 cm³ (volume) = 0.4574 g/cm³ ✓

Pellet Fuel Moisture Content Determination

Tare Beaker Wt. _____ g
Wet Wt: _____ g - _____ g = _____ g
Gross Wet Wt. Tare Beaker Wt. Net Wet Wt.
Dry Wt: _____ g - _____ g = _____ g
Gross Dry Wt. Tare Beaker Wt. Net Dry Wt.
% Moisture Dried Basis: _____ %
[1 - (Net Dry Wt ÷ Net Wet Wt.)] X 100

Minute Time	Scale lbs left	Burn Rate	CO ₂		O ₂		Tel		CO		T/C(1)/T/C(2)		T/C(3)		SO ₂ v.	Static Press.	Comments
			v.	%CO ₂	v.	%O ₂			v.	%CO	Wet Bulb	Dry Bulb	% H ₂ O	Calc W/B			
0																-0.53	Flow
5	625.7	17.2	1.83	4.57	58.7	14.71			33.3	1.67	2.7	83	118	2.6	108	-0.86	SO ₂ 1.5
10	624.6	16.1	1.40	10.14	37.3	9.34	Gas BTL		2.3	6.13	78.0	100	130	5.4	123	-0.72	SO ₂ 1.5
15	623.8	15.3	1.35	8.87	43.4	10.87			10.3	0.53	16.7	124	144	12.5	139	-0.75	SO ₂ 1.5
20	622.9	14.4	1.42	10.46	37.5	9.39			4.7	0.25	41.9	129	146	14	142	-0.76	SO ₂ 1.5
25	622.1	13.6	1.45	11.28	35.8	8.97			7.5	0.38	29.7	131	148	15	144	-0.77	
30	621.2	12.7	1.47	11.83	33.8	8.46			4.1	0.22	53.8	132	149	15.5	146	-0.77	
35	620.3	11.8	1.52	12.75	30.3	7.59			3.4	0.18	70.8	133	150	16	147	-0.78	
40	619.4	10.9	1.50	12.53	31.9	7.99			2.1	0.12	104.4	132	150	15.5	147	-0.77	
45	618.6	10.1	1.47	11.83	34.1	8.54			2.6	0.14	84.5	131	149	14.5	147	-0.77	
50	617.7	9.2	1.48	12.06	33.0	8.26			3.2	0.17	70.9	130	148	14	143	-0.76	
55	617.0	8.5	1.47	11.83	34.0	8.57			3.2	0.17	69.6	129	148	14	143	-0.75	
60	616.2	7.7	1.47	11.88	34.2	8.56			2.0	0.11	108.0	128	147	13.5	142	-0.75	
65	615.5	7.0	1.49	11.68	34.9	8.74			2.9	0.16	73.0	126	145	13	142	-0.89	Flow
70	614.9	6.4	1.45	11.21	36.7	9.19			2.8	0.16	70.1	124	144	12.5	140	-0.74	SO ₂ 1.5
75	614.2	5.7	1.42	10.59	39.0	9.77			3.0	0.16	66.7	122	141	12	139	-0.72	SO ₂ 1.5
80	613.7	5.2	1.40	10.04	41.0	10.27			2.9	0.16	62.8	119	138	10	134	-0.71	SO ₂ 1.5
85	613.2	4.7	1.36	9.15	43.9	11.00			5.5	0.29	31.5	116	135	9.5	133	-0.71	SO ₂ 1.5
90	612.8	4.3	1.32	8.03	47.7	11.95			6.6	0.35	22.9	111	132	8.5	131	-0.69	
95	612.5	4.0	1.29	7.26	50.8	12.73			8.7	0.45	16.1	107	130	7.2	128	-0.68	
100	612.2	3.7	1.28	7.11	51.1	12.80			9.7	0.50	14.2	103	128	6.3	123	-0.65	
105	612.0	3.5	1.26	6.66	52.6	13.18	Out BTL		14.1	0.72	9.3	100	126	5.5	121	-0.65	
110	611.8	3.3	1.28	5.69	55.8	13.98			18.3	0.93	6.1	96	123	4.8	118	-0.61	
115	611.6	3.1	1.27	5.42	56.2	14.08			22.6	1.15	4.7	92	121	4.0	114	-0.60	
120	611.5	3.0	1.22	5.57	56.2	14.08			21.2	1.08	5.2	89	119	3.6	112	-0.58	
125																-0.79	SO ₂ 1.5

BURN RATE AND FLUE GAS DATA
 WORK OVER DATA SHEET #12
 WST2-Form 14 Rev 1/88
 ENO WT. 608.5 lbs

Unit: HIGH VALLEY X-TEC Date: 3/29/99
 Run: EPA #5 Technician(s): A.T.I. / JEN
 Page: 3 of 3

Minute Time	Scale Wt	lbs left	Burn Rate	CO2		O2		CO		T/C(1)T/C(2)		T/C(3)		Stack	SO2 v.	Static Press.	Comments
				v.	%CO2	v.	%O2	v.	%CO	Wet Bulb	Dry Bulb	% H2O	Calc W/B				
240	609.3	.8	.1	.160	4.00	62.9	15.76	21.9	1.10	3.6	74	99	1.9	101	.225	-045	Flow
245	609.3	.8	0	.156	3.90	63.0	15.79	23.1	1.17	3.3	74	98	2	100	.223	-044	SO2 1.5
250	609.2	.7	.1	.149	3.73	63.6	15.94	24.4	1.22	3.1	74	98	2	100	.222	-044	SO2 1.5
255	609.1	.6	.1	.144	3.60	63.9	16.02	26.4	1.33	2.7	73	98	1.9	100	.220	-043	SO2 1.5
260	609.1	.6	0	.145	3.63	63.7	15.97	27.2	1.36	2.7	74	98	2	100	.218	-043	SO2 1.5
265	609.0	.5	.1	.149	3.73	63.5	15.92	26.1	1.30	2.9	74	98	2	100	.217	-042	SO2 1.5
270	608.9	.4	.1	.153	3.83	63.4	15.89	24.4	1.23	3.1	74	98	2	100	.216	-042	SO2 1.5
275	608.9	.4	0	.157	3.93	62.9	15.76	24.8	1.26	3.1	74	98	2	100	.216	-042	SO2 1.5
280	608.8	.3	.1	.161	4.03	62.4	15.64	24.9	1.27	3.2	74	98	2	100	.214	-041	SO2 1.5
285	608.7	.2	.1	.157	3.93	62.7	15.71	26.2	1.32	3.0	74	98	2	100	.213	-041	SO2 1.5
290	608.7	.2	0	.142	3.55	63.8	15.99	28.9	1.45	2.5	73	98	1.9	100	.212	-041	SO2 1.5
295	608.7	.2	0	.122	3.06	62.8	16.49	31.1	1.58	1.9	74	97	2	100	.211	-041	SO2 1.5
300	609.6	.1	.1	.106	2.66	67.7	16.97	29.8	1.50	1.8	73	97	1.9	100	.208	-041	SO2 1.5
305	609.6	.1	0	.100	2.51	68.3	17.12	29.6	1.51	1.7	73	97	1.9	100	.206	-040	SO2 1.5
310	609.5	0	.1	.098	2.46	68.6	17.19	28.1	1.45	1.7	73	96	1.9	100	.205	-041	SO2 1.5
315														<u>(619)</u>		<u>(122)</u>	<u>CO 1.5</u>
320														<u>(322.6)</u>		<u>(1632)</u>	
325														<u>(1806.5)</u>		<u>(3.518)</u>	
330																	
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Pre Burn wt. 60.0 lbs. NP
 Test Start wt. Range 609.2 - 608.5 lbs.
 T/C#-3

PRE BURN DATA
 RECORD SHEET #13
 WST2-Form16

28.47
 BARD. OF -
 PRESSURE -
 28.42

50 W/4

Unit: HIGH VALLEY X-TEC Date: 3/27/99
 Run: EPA #5 Technician(s): ATH, PLS.
 Page: 1 of 2

Hot Box On

Minute Time	Scale Weight	Burn Rate	Stack	Stove Top	Left Side	Back	Right Side	Bottom	Firebox	2nd Burn Catalyst	Room Temp	Static	Comments
0:15	615.2	0	644	902	540	498	572	557	874	1579	69	-096	Primary Air Set at 1 1/16 OPEN
5:35	614.2	1.0	539	827	548	499	576	563	868	1478	69	-087	Secondary Air Set at 1 1/16 X 3"
10:00	613.2	1.0	498	775	549	494	574	567	876	1468	70	-083	Fan: OFF
15:05	612.3	.9	470	735	550	503	578	565	888	1396	70	-080	TUNNEL ON AT: 1253
20:10	611.6	.7	442	694	549	509	580	562	884	1343	71	-077	Buckets I.A.E.D
25:15	611.0	.6	421	654	545	511	582	559	877	1350	71	-075	ANALYZERS SPANNED
30:20	610.5	.5	403	621	539	512	582	552	876	1272	71	-072	Pumps turned on at: 1330
35:25	610.0	.5	389	592	535	511	582	545	876	1246	72	-070	AT
40:30	609.7	.3	371	561	527	511	582	538	878	1196	73	-066	
45:35	609.4	.3	356	536	520	511	579	534	880	1176	72	-065	Check WB/DB: 17/137 536.0
50:40	609.2	.2	344	515	511	510	575	530	878	1140	73	-064	528.2
55:45	613.9	.4	348	507	501	508	568	529	819	1254	73	-069	ADD FUEL 5.1 lbs. Probe IN TUNNEL
60:50	613.3	.6	382	561	488	491	557	528	812	1240	73	-072	525.0
65:55	612.6	.7	384	581	482	481	547	525	805	1232	73	-071	523.2
70:00	612.1	.5	377	580	476	475	540	524	795	1191	73	-070	519.0
75:05	611.6	.5	376	572	472	473	535	523	793	1219	74	-070	515.0
80:10	611.1	.5	379	572	469	472	532	523	802	1286	73	-070	513.6
85:15	610.5	.6	391	596	467	494	531	524	810	1347	73	-071	518.4
90:20	610.0	.5	394	609	468	478	531	525	817	1304	73	-072	522.2
95:25	609.7	.3	378	597	469	481	532	527	824	1230	73	-070	521.2
100:30	609.4	.3	355	557	465	481	529	527	814	1077	72	-065	510.6
105:35	609.3	.1	336	515	459	478	522	527	804	1032	73	-064	500.2
110:40	609.1	.2	323	487	452	473	515	526	795	1014	72	-062	490.6
115:45	609.0	.1	311	462	445	468	507	524	780	973	72	-060	481.2

Pre Burn wt: 163.1
 Test Star wt: 165.
 609.2 - 608.5

PRE BURN DATA
 RECORD SHEET #13
 Range WST2-Form16

Unit: HIGH VALLEY X-TEC
 Run: EPA #5 of 2
 Page: 2 of 2

Date: 3/29/99
 Technician(s): ATH, PLS.

Minute	Scale Weight	Burn Rate	Stack	Stove Top	Left Side	Back	Right Side	Bottom	Firebox	2nd Burn	Room Temp	Static	Comments
120	608.9	.1	304	445	438	462	499	523	770	980	72	7059	Primary Air Set at 1/16 OPEN
125	608.8	.1	298	431	434	456	491	521	773	968	72	7057	Secondary Air Set at 1" X 3"
130	608.7	.1	290	415	431	450	483	518	752	910	73	7055	Fan: OFF
135	608.6	.1	281	401	423	444	476	515	742	895	73	7054	TUNNEL ON AT: 1253
140	608.5	.1	272	386	414	437	467	510	731	880	73	7053	Buckets Tied 442.8
145													ANALYZERS SPANNED
150													Pumps turned on at: 1330
155													AT
160													Check WB/DB: 112/137
165													Probe IN TUNNEL
170													
175													
180													
185													
190													

Hot Box ON

T/C#	Minute	Stove Top	Left Side	Back	Right Side	Bottom	Firebox	2nd Burn Gate	Room Temp	Tunnel	C. Gas Box	Impinger Out	5G-1 Filter	5G-1 Condenser	Con- dar
0	15	386	414	437	467	510	731	880	73	105	250	40	85	50	257
5	15	407	414	426	462	505	673	1031	74	147	250	41	86	37	257
10	20	495	409	387	450	505	642	1311	75	126	257	41	86	37	257
15	25	536	403	364	443	501	653	1416	75	121	257	41	87	37	257
20	30	587	402	357	441	494	661	1466	75	121	257	41	87	38	250
25	35	611	405	344	443	486	679	1485	74	122	257	41	87	38	250
30	40	637	411	340	446	480	720	1507	74	123	257	41	87	38	250
35	45	658	419	340	452	475	728	1473	73	124	257	41	87	38	250
40	50	645	426	343	459	471	738	1418	74	123	257	41	87	38	250
45	55	637	434	347	468	469	758	1400	74	123	257	42	87	38	250
50	60	631	442	354	479	469	770	1452	74	122	257	42	87	38	250
55	05	620	449	365	490	467	790	1391	74	121	250	42	87	38	250
		(6860)	(5028)	(4398)	(550)	(5832)	(8543)	(16230)	(889)						
60	10	625	457	377	500	465	792	1379	74	121	250	42	87	38	250
65	15	611	467	395	509	463	809	1367	74	119	250	42	87	38	250
70	20	594	476	410	515	462	821	1340	73	118	250	42	87	38	250
75	25	576	484	422	520	461	837	1323	74	116	250	42	87	38	250
80	30	558	488	432	523	462	834	1271	74	115	250	42	86	38	257
85	35	543	489	437	525	464	834	1253	74	113	250	42	86	38	257
90	40	524	485	440	524	467	828	1215	73	110	250	42	86	38	257
95	45	501	478	445	520	471	826	1165	73	108	250	43	86	38	257
100	50	484	472	450	515	475	822	1116	73	107	250	43	86	38	257
105	55	468	467	454	506	479	810	1081	73	105	250	43	86	38	257
110	60	452	462	450	496	481	806	1034	72	104	250	43	86	38	250
116	05	437	453	447	487	482	801	1006	73	102	250	43	86	38	250
		(6373)	(5178)	(5159)	(6140)	(5632)	(9820)	(14550)	(880)						

13,533 10,706 9557 11,640 11,414 18,363 30,780 1719

107
42x

T/C#	Minute Time	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
		Stove Top	Left Side	Back	Right Side	Bottom	Firebox	2nd Burn Catalyst	Room Temp	Tunnel	C. Gas Box	Impinger Out	5G-1 Filter	5G-1 Condenser	Condr	
120	15	424	448	447	480	483	794	996	72	101	250	44	86	38	250	
125	15	413	442	449	475	485	788	919	72	100	250	44	86	38	250	
130	20	402	435	448	470	487	781	895	72	99	250	44	86	38	250	
135	25	392	428	443	465	485	773	879	71	98	250	44	86	38	250	
140	30	382	422	438	459	482	754	864	71	96	250	44	86	38	250	
145	35	373	415	432	453	477	747	835	71	96	250	44	86	38	250	
150	40	365	407	426	446	474	738	825	71	95	251	44	86	38	250	
155	45	359	402	421	440	471	728	809	70	94	251	44	86	39	251	
160	50	351	395	416	435	469	719	802	70	93	251	45	85	39	251	
165	55	345	390	412	431	468	706	798	70	92	251	45	85	39	251	
170	1800	341	384	409	426	462	714	783	70	91	251	45	84	38	251	
175	05	336	379	408	422	465	687	767	70	91	251	45	83	38	251	
180	10	331	375	408	419	463	670	759	69	90	251	45	83	39	251	
185	15	327	370	409	415	461	667	752	69	89	251	45	82	39	251	
190	20	323	366	408	412	460	659	734	69	89	250	45	82	39	250	
195	25	319	361	408	408	458	657	727	68	88	250	46	81	39	250	
200	30	315	357	408	405	454	644	730	68	88	250	46	81	39	250	
205	35	313	353	411	402	450	637	740	68	87	250	46	80	39	250	
210	40	312	349	424	402	447	629	748	68	86	251	46	80	39	250	
215	45	311	346	436	403	444	625	744	67	86	251	46	79	39	250	
220	50	311	344	443	405	441	619	742	67	86	251	44	79	39	250	
225	55	309	341	451	405	438	616	737	67	85	251	43	78	39	250	
230	1900	309	340	455	406	436	609	732	67	85	251	43	78	39	251	
235	05	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
240	10	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
245	15	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
250	20	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
255	25	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
260	30	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
265	35	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
270	40	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
275	45	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
280	50	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
285	55	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
290	1900	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
295	05	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
300	10	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
305	15	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
310	20	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
315	25	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
320	30	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
325	35	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
330	40	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
335	45	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
340	50	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
345	55	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
350	1900	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
355	05	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
360	10	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
365	15	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
370	20	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
375	25	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
380	30	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
385	35	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
390	40	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
395	45	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
400	50	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
405	55	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
410	1900	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
415	05	308	336	458	407	433	602	722	67	85	251	43	78	39	251	
420	10	308	336	458	407	433	602	722	67	85	251	43	78			

Unit: HIGH VALLEY X-TEC Date: 3/29/99
 Run: EPA #5 Technicián(s): ATI, PLS,
 Page: 3 of 3

Minute	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
Time	Stove Top	Left Side	Back Side	Right Side	Bottom	Firebox	2nd Burn	Room Temp	Tunnel	C. Gas Box	Impinger Out	5G-1 Filter	5G-1 Condenser	Gen- dat	
240	306	334	453	408	428	603	715	67	85	251	43	72	39	251	
245	304	333	444	407	426	611	707	68	86	251	43	77	39	251	
250	302	331	438	406	424	613	693	67	86	251	43	77	39	251	
255	300	330	431	405	421	608	684	67	86	251	43	77	39	251	
260	298	329	426	403	419	608	682	68	86	251	43	77	39	251	
265	296	327	426	401	417	610	681	68	86	251	43	77	39	251	
270	294	326	425	398	415	613	676	68	86	251	43	77	39	250	
275	292	324	426	396	413	619	674	67	86	251	43	78	39	250	
280	290	324	429	392	409	620	664	67	85	251	43	77	39	251	
285	289	324	429	390	407	622	658	67	85	251	43	77	39	250	
290	287	325	429	387	402	619	640	67	85	251	43	77	39	250	
295	286	325	425	384	400	614	632	67	85	251	43	77	39	250	
300	283	323	414	380	398	590	620	67	85	251	44	77	39	251	
305	280	321	402	376	398	574	608	67	85	251	44	77	39	250	
310	277	318	395	373	398	564	600	67	84	251	44	77	39	250	
315	275	316	392	371	396	564	600	67	84	251	44	77	39	250	
320	273	314	390	369	394	564	600	67	84	251	44	77	39	250	
325	271	312	388	367	392	564	600	67	84	251	44	77	39	250	
330	269	310	386	365	390	564	600	67	84	251	44	77	39	250	
335	267	308	384	363	388	564	600	67	84	251	44	77	39	250	
340	265	306	382	361	386	564	600	67	84	251	44	77	39	250	
345	263	304	380	359	384	564	600	67	84	251	44	77	39	250	
350	261	302	378	357	382	564	600	67	84	251	44	77	39	250	
355	259	300	376	355	380	564	600	67	84	251	44	77	39	250	
360	257	298	374	353	378	564	600	67	84	251	44	77	39	250	
365	255	296	372	351	376	564	600	67	84	251	44	77	39	250	
370	253	294	370	349	374	564	600	67	84	251	44	77	39	250	
375	251	292	368	347	372	564	600	67	84	251	44	77	39	250	
380	249	290	366	345	370	564	600	67	84	251	44	77	39	250	
385	247	288	364	343	368	564	600	67	84	251	44	77	39	250	
390	245	286	362	341	366	564	600	67	84	251	44	77	39	250	
395	243	284	360	339	364	564	600	67	84	251	44	77	39	250	
400	241	282	358	337	362	564	600	67	84	251	44	77	39	250	
405	239	280	356	335	360	564	600	67	84	251	44	77	39	250	
410	237	278	354	333	358	564	600	67	84	251	44	77	39	250	
415	235	276	352	331	356	564	600	67	84	251	44	77	39	250	
420	233	274	350	329	354	564	600	67	84	251	44	77	39	250	
425	231	272	348	327	352	564	600	67	84	251	44	77	39	250	
430	229	270	346	325	350	564	600	67	84	251	44	77	39	250	
435	227	268	344	323	348	564	600	67	84	251	44	77	39	250	
440	225	266	342	321	346	564	600	67	84	251	44	77	39	250	
445	223	264	340	319	344	564	600	67	84	251	44	77	39	250	
450	221	262	338	317	342	564	600	67	84	251	44	77	39	250	
455	219	260	336	315	340	564	600	67	84	251	44	77	39	250	
460	217	258	334	313	338	564	600	67	84	251	44	77	39	250	
465	215	256	332	311	336	564	600	67	84	251	44	77	39	250	
470	213	254	330	309	334	564	600	67	84	251	44	77	39	250	
475	211	252	328	307	332	564	600	67	84	251	44	77	39	250	
480	209	250	326	305	330	564	600	67	84	251	44	77	39	250	
485	207	248	324	303	328	564	600	67	84	251	44	77	39	250	
490	205	246	322	301	326	564	600	67	84	251	44	77	39	250	
495	203	244	320	299	324	564	600	67	84	251	44	77	39	250	
500	201	242	318	297	322	564	600	67	84	251	44	77	39	250	
505	199	240	316	295	320	564	600	67	84	251	44	77	39	250	
510	197	238	314	293	318	564	600	67	84	251	44	77	39	250	
515	195	236	312	291	316	564	600	67	84	251	44	77	39	250	
520	193	234	310	289	314	564	600	67	84	251	44	77	39	250	
525	191	232	308	287	312	564	600	67	84	251	44	77	39	250	
530	189	230	306	285	310	564	600	67	84	251	44	77	39	250	
535	187	228	304	283	308	564	600	67	84	251	44	77	39	250	
540	185	226	302	281	306	564	600	67	84	251	44	77	39	250	
545	183	224	300	279	304	564	600	67	84	251	44	77	39	250	
550	181	222	298	277	302	564	600	67	84	251	44	77	39	250	
555	179	220	296	275	300	564	600	67	84	251	44	77	39	250	
560	177	218	294	273	298	564	600	67	84	251	44	77	39	250	
565	175	216	292	271	296	564	600	67	84	251	44	77	39	250	
570	173	214	290	269	294	564	600	67	84	251	44	77	39	250	
575	171	212	288	267	292	564	600	67	84	251	44	77	39	250	
580	169	210	286	265	290	564	600	67	84	251	44	77	39	250	
585	167	208	284	263	288	564	600	67	84	251	44	77	39	250	
590	165	206	282	261	286	564	600	67	84	251	44	77	39	250	
595	163	204	280	259	284	564	600	67	84	251	44	77	39	250	
600	161	202	278	257	282	564	600	67	84	251	44	77	39	250	
605	159	200	276	255	280	564	600	67	84	251	44	77	39	250	
610	157	198	274	253	278	564	600	67	84	251	44	77	39	250	
615	155	196	272	251	276	564	600	67	84	251	44	77	39	250	
620	153	194	270	249	274	564	600	67	84	251	44	77	39	250	
625	151	192	268	247	272	564	600	67	84	251	44	77	39	250	
630	149	190	266	245	270	564	600	67	84	251	44	77	39	250	
635	147	188	264	243	268	564	600	67	84	251	44	77	39	250	
640	145	186	262	241	266	564	600	67	84	251	44	77	39	250	
645	143	184	260	239	264	564	600	67	84	251	44	77	39	250	
650	141	182	258	237	262	564	600	67	84	251	44	77	39	250	
655	139	180	256	235	260	564	600	67	84	251	44	77	39	250	
660	137	178	254	233	258	564	600	67	84	251	44	77	39	250	
665	135	176	252	231	256	564	600	67	84	251	44	77	39	250	
670	133	174	250	229	254	564	600	67	84	251	44	77	39	250	
675	131	172	248	227	252	564	600	67	84	251	44	77	39	250	
680	129	170	246	225	250	564	600	67	84	251	44	77	39	250	
685	127	168	244	223	248	564	600	67	84	251	44	77	39	250	
690	125	166	242	221	246	564	600	67	84	251	44	77	39	250	
695	123	164	240	219	244	564	600	67	84	251	44	77	39	250	
700	121	162	238	217	242	564	600	67	84	251	44	77	39	250	
705	119	160	236	215	240	564	600	67	84	251	44	77	39	250	
710	117	158	234	213	238	564	600	67	84	251	44	77	39	250	
715	115	156	232	211	236	564	600	67	84	251	44	77	39		

PRE AND POST TEST ZERO/SPAN CHECK
WOODSTOVE DATA SHEET #15-1

Site: Myren Consulting, Colville, WA Date: 3/29/99 Analyte: CO2

Source: High Valley XTEC Run #: EPA #5

Zero Cyl #: 36919 Conc. 00.0 % CO₂ Cyl Press: 220 psi

Certified by: Cascade Airgas Date: 4/24/96

Span Cyl #: 250-1060 Conc. 6.0 % CO₂ Cyl Press: 1480 psi

Certified by: Oxarc Date: 8/22/97

Analyzer: Make: Horiba Model: PIR-2000 SN: 607024

Range: 0 - 25.0% CO2 Analyzer Output: 0 - 1.0 v.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter:

EPA Span Value = 25.0% CO₂

EPA Control Limits = + 2.5% of 25.0% CO₂ = + 0.625% CO₂

Pre Run Audit: By: ATM / RLS Time: 1315 Temp: 71 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	00.0	.000	0256	+0.0256	+0.10
Span	24.0	.240	6.0	6.0	.236	5.8913	-0.1087	-1.81

Comments:

Post Run Audit: By: ATM / RLS Time: 2129 Temp: 66 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	00.0	.000	0256	+0.0256	+0.10
Span	24.0	.240	6.0	23.5	.235	5.866	-0.1336	-2.23

Comments:

+ Conc. Difference = Act % - Exp (Std) %

Zero % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$

Span % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

PRE AND POST TEST ZERO/SPAN CHECK
WOODSTOVE DATA SHEET #15-2

Colville, WA

Site: Myren Consulting, Woodinville, WA Date: 3/29/99 Analyte: O₂

Source: High Valley XTEC Run #: EPA #5

Zero Cyl #: 36919 Conc. 00.0 % O₂ Cyl Press: 220 psi

Certified by: Cascade Airgas Date: 4/24/96

Span Cyl #: 250-1060 Conc. 6.0 % O₂ Cyl Press: 1480 psi

Certified by: Oxarc Date: 8/22/97

Analyzer: Make: Taylor Model: OA 137 SN: 137/4772

Range: 0 - 25.0% O₂ Analyzer Output: 0 - 100 mv.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter:

EPA Span Value = 25.0% O₂

EPA Control Limits = + 2.5% of 25.0% O₂ = + 0.625% O₂

Pre Run Audit: By: ATM / RLS Time: 1315 Temp: 71 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ%
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	00.0	00.0	00.155	-0.155	-0.06
Span	6.0	24.0	6.0	6.0	23.8	5.955	-0.0445	-0.74

Comments:

Post Run Audit: By: ATM / RLS Time: 2129 Temp.: 66 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ%
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	00.0	00.0	00.155	-0.155	-0.06
Span	6.0	24.0	6.0	6.0	23.8	5.955	-0.0445	-0.74

Comments:

+ Conc. Difference = Act % - Exp (Std) %

Zero % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$

Span % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

PRE AND POST TEST ZERO/SPAN CHECK
WOODSTOVE DATA SHEET #15-3

Colville

Site: Myren Consulting, Woodinville, WA Date: 3/29/99 Analyte: CO

Source: High Valley XTEC Run #: EPA #5

Zero Cyl #: 36919 Conc. 00.0 % CO Cyl Press: 220 psi

Certified by: Cascade Airgas Date: 4/24/96

Span Cyl #: 250-1060 Conc. 1.26 % CO Cyl Press: 1480 psi

Certified by: Oxarc Date: 8/22/97

Analyzer: Make: Infra Red Model: 702 D SN: 113

Range: 0 - 10.0% CO Analyzer Output: 0 - 100 mv.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter: _____

EPA Span Value = 5.0% CO

EPA Control Limits = +2.5% of 5.0% CO = + 0.125% CO

Pre Run Audit: By: ATM/RLS Time: 1315 Temp: 71 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.00	00.0	-0.0091	-0.0091	-0.18
Span	1.26	25.2	1.26	1.24	25.1	1.2518	-0.0082	-0.65

Comments:

Post Run Audit: By: ATM/RLS Time: 2129 Temp.: 66 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.00	00.1	-0.0040	-0.0040	-0.08
Span	1.26	25.2	1.26	1.22	24.4	1.2166	-0.0434	-3.44

Comments:

+ Conc. Difference = Act % - Exp (Std) %

Zero % Differece = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$

Span % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

Unit: HIGH VALLEY X-100
 Run: EPA #5
 Date: 3/29/99
 Technicians: ATH, RLS
 WST6-Form3-Rev11/89

QUALITY CHECKS
 WOODSTOVE DATA SHEET #16

Ambient = Tr: _____ °F T/C#30: _____ °F
 Thermocouple Check (at ambient): T/C#1: 59 °F; T/C#2: 59 °F;
 T/C #3: 58 °F; T/C #4: 57 °F; T/C #5: 58 °F;
 T/C #6: 57 °F; T/C #7: 57 °F; T/C #8: 57 °F;
 T/C #9: 61 °F; T/C #10: 58 °F; T/C #11: 60 °F;
 T/C #12: 61 °F; T/C #13: 58 °F; T/C #14: 57 °F;
 T/C #15: 61 °F; T/C #16: 59 °F; T/C #17: 59 °F;
 T/C #18: _____ °F; T/C #19: _____ °F; T/C #20: _____ °F;
 T/C #21: _____ °F; T/C #22: _____ °F; T/C #23: _____ °F;
 T/C #24: _____ °F; T/C #25: _____ °F; T/C #26: _____ °F;

Comments: _____

Thermocouple Readout: Pretest Zero/Span Check and Calibration:
 Zero (0°F) : 002 °F Adj to: 000 °F Post Test Check Zero (0°F): 002 °F % Difference +0.10
 Span (2000°F): 1999 °F Adj to: 2000 °F Span (2000°F): 2000 °F 0.00
 (Allowable % Difference = 1.5%. Use formulas on Woodstove Data Sheet #15 to calculate % Difference)

Thermocouple Readout Pretest Linearity Check

0°F = 000 °F; 200°F = 200 °F; 400°F = 399 °F;
 600°F = 599 °F; 800°F = 800 °F; 1000°F = 1000 °F;
 1200°F = 1199 °F; 1400°F = 1400 °F; 1600°F = 1599 °F;
 1800°F = 1800 °F; 2000°F = 2000 °F

Combustion Gas (CO₂, O₂, CO) Train Leak Check: Pre Post
 Draft (Static) Gauge Zero Check: Pre Post

Scale Check Pre (Wt, #'s): 607.5 - 612.5 5.0 lbs, OK (PLS.)
 Post (Wt, #'s): 635.6 - 630.6 5.0/5.0 lbs OK (ATH)

Stack cleaned prior to the run: Yes _____ No
 Tunnel cleaned prior to the run: Yes _____ No

DATE 3/23/99

PAGE 1 OF 2

MODEL # XTEC

RUN # EPA 4

METER BOX # 511-M

METER Y 1.003

FILTER # (F) 780 (R) 77

PRE TEST LEAK RATE = .001 CFM @ -15.0 IN. HG .297/.298

FILTER SIZE: 110mm

POST TEST LEAK RATE = .000 CFM @ -15.0 IN. HG .085/.085

PROBE LENGTH 24" glass

TIME		METER READING CU.FT.	PITOT dp	TNL TEMP. (°F)	METER TEMP. (°F)	GAS METER dh	VAC IN. Hg	VELOCITY TRAVERSE			
CLOCK	ELAPSED							POINT	LOCATION	ΔP	TEMP
1235	00	284.704	-040	109	72	.90	0	N-1	0.5"	-033	112
45	10	290.182	-040	132	74	.90	0	2	1.5"	-041	113
55	20	295.698	-040	127	75	.90	0	3	4.5"	-039	113
1305	30	301.198	-040	130	77	.90	0	4	5.5"	-035	113
15	40	306.728	-039	127	78	.90	0	W-1	0.5"	-036	114
25	50	312.241	-039	124	79	.90	0	2	1.5"	-041	114
35	60	317.749	-039	123	80	.90	0	3	4.5"	-040	114
45	70	323.258	-040	119	81	.90	0	4	5.5"	-036	114
55	80	328.788	-040	115	82	.90	0	Avg. <u>-0376</u> <u>113</u>			
1405	90	334.319	-040	111	82	.90	0	Pilot Leak Check Pre <input checked="" type="checkbox"/> Post <input checked="" type="checkbox"/>			
15	100	339.866	-040	109	82	.90	0	Cp = <u>0.99</u>	N		
25	10	345.413	-040	106	82	.90	0		1		
35	20	350.981	-040	103	83	.90	0		2		
45	30	356.533	-040	101	83	.90	0		3		
55	40	362.095	-040	99	83	.90	0		4		
1505	50	367.667	-040	98	83	.90	0				
15	60	373.227	-040	97	83	.90	0				
25	70	378.801	-040	96	84	.90	0				
35	80	384.368	-040	95	84	.90	0				
45	90	389.973	-040	94	84	.90	0				

→ W 1 2 3/4
3
4

*-point of Avg. delta p

$$QS = \left(\frac{\sqrt{(\Delta P \times BP)}}{T(^{\circ}R)} \right) \times 3167.2 =$$

137.063 cfm

BP = Start 28.54 in Hg
60 28.53
120 28.51
180 28.51
240 28.51
285 28.51
28.5183 ✓

10.6 -1.9

DATE 3/23/99

PAGE 2 OF 2

MODEL # HIGH VALLEY X-TEC RUN # EPA #4

METER BOX # 511-M

METER Y 1.003

FILTER # (F) 780 (R) 77

PRE TEST LEAK RATE = .001 CFM @ -15.0 IN. HG, 297/1,298

FILTER SIZE: 110 MM

POST TEST LEAK RATE = .000 CFM @ -15.0 IN. HG, 085/1.085

PROBE LENGTH 24" GLASS

TIME		METER READING CU.FT.	PITOT dp	TNL TEMP. (°F)	METER TEMP. (°F)	GAS METER dh	VAC IN. Hg	VELOCITY TRAVERSE			
CLOCK	ELAPSED							POINT	LOCATION	ΔP	TEMP
1555	00	395.519	-040	94	84	.90	0	N-1	0.5"	.033	112
1605	10	401.176	-040	93	84	.90	0	2	1.5"	.041	113
15	20	406.783	-040	92	84	.90	0	3	4.5"	.039	113
25	30	412.372	-040	91	84	.90	0	4	5.5"	.035	113
35	40	417.978	-040	91	84	.90	0	W-1	0.5"	.036	114
45	50	423.578	-040	90	84	.90	0	2	1.5"	.041	114
55	60	429.183	-040	89	84	.90	0	3	4.5"	.040	114
1705	70	434.801	-040	88	84	.90	0	4	5.5"	.036	114
15	80	440.417	-040	86	84	.90	0	Avg. <u>.0376</u>			<u>113</u>
25	0805	443.231	-040	86	84	.90	0	Pilot Leak Check Pre <input checked="" type="checkbox"/> Post <input checked="" type="checkbox"/>			
35	00	(158.527)						Cp = <u>0.99</u>			
	10							N 1 2 → W 1 2 <u>3</u> 4 3 4			
	20							* = point of Avg. delta p			
	30							Qs = $\left(\frac{\sqrt{(\Delta P \times BP)}}{T(^{\circ}R)} \right) \times 3167.2 =$			
	40							<u>137.063</u> cfm			
	50							BP = <u>START 28.54</u> in Hg			
	60							60 28.53			
	70							120 28.51			
	80							180 28.51			
	90							240 28.51			
								285 28.51			

$\bar{x} = 28.5183$

WOODSTOVE DATA SHEET #4-1: INITIAL FILTER WEIGHTS (TARE WEIGHTS)

Into Dessicator: Date 1/3/99 Time 12:00 By ATM Front Half Back Half

Manufacturer: Schleicher & Schuell Size: 11cm Lot No.: ZB 95.1 Grade: #25 g/lbss
Order No. 06220

Filter #	First Wt	Date	Time	By	Second Wt	Date	Time	By	Third Wt	Date	Time	By
776	.7853	2/7/99	12:55	T.M.	.7853	2/10/99	1629	ATM				
777	.8127		12:56	T.M.	.8129		1628	ATM				
778	.8044		12:57	T.M.	.8040		1627	ATM				
779	.8036		12:58	T.M.	.8034		1626	ATM				
780	.7859		12:59	T.M.	.7888		1625	ATM				
781	.7894		1:00	T.M.	.7892		1625	ATM				
782	.7905		1:01	T.M.	.7903		1624	ATM				
783	.7967		1:02	T.M.	.7968		1623	ATM				
784	.8120		1:03	T.M.	.8118		1622	ATM				
785	.8166		1:04	T.M.	.8164		1621	ATM				
786	.7925		1:05	T.M.	.7923		1620	ATM				
787	.8064		1:06	T.M.	.8064		1619	ATM				
788	.7928		1:07	T.M.	.7926		1619	ATM				
789	.7774		1:08	T.M.	.7774		1618	ATM				
790	.7835		1:09	T.M.	.7835		1617	ATM				
791	.7981		1:10	T.M.	.7982		1616	ATM				
792	.8036		1:11	T.M.	.8035		1615	ATM				
793	.8116		1:12	T.M.	.8116		1614	ATM				
794	.8025		1:13	T.M.	.8024		1613	ATM				
795	.7766		1:14	T.M.	.7765		1613	ATM				
796	.7916		1:15	T.M.	.7915		1612	ATM				
797	.7755		1:16	T.M.	.7756		1611	ATM				
798	.8133		1:17	T.M.	.8133		1610	ATM				
799	.7949		1:18	T.M.	.7948		1610	ATM				
800	.8266	✓	1:19	T.M.	.8266	✓	1609					

Checked by Jim Thompson

Date: 2/21/99 Time 1405

QA REWEIGH

Filter #	WT	Date	Time	By
781	.7851	2/21/99	1412	Jim
789	.7772	2/21/99	1414	Jim
795	.7765	2/21/99	1415	Jim

BALANCE ROOM ENVIRONMENTAL CONDITIONS

WB	DB	%RH	Date	Time	By
62	76	45	2/21/99	1235	ATM
63	73	45	2/21/99	1600	ATM
65	80	44	2/21/99	1312	ATM

Post Weighing Secondary Scale Check
 0.0000 0.0010 0.0020 0.0000
 1.0000 1.0001 1.0000 1.0001

WOODSTOVE DATA SHEET #4-3: CONSTANT FINAL WEIGHTS

Acetone Blank - 100 ml / Accutone

WST5-Form9 Pg1, Rev4/90
 Unit High Valley XTTC
 Run # EPA-4
 Date: 3/23/99

Beaker #	Into Dessic	Date	Time	By	First	Date	Time	By	Second	Date	Time	By	Third	Date	Time	By
8	✓	3/18/99	0854	AM	66.0215	3/19/99	2237	ATM	66.0215	3/20/99	1832	ATM				

Blank
 3/13/99

FINAL FILTER WEIGHTS

Filter #	Into Dessic	Date	Time	By	First	Date	Time	By	Second	Date	Time	By	Third	Date	Time	By

QA REWEIGH: FINAL WEIGHTS

Date	Beaker #	Final Wt	By

SCALE ROOM ENVIRONMENTAL CONDITIONS

Weighing Session	Date	Time	By	WB	DB	%RH
1	3/18	2140	ATM	68	84	43
2	3/20	1300	ATM	64	84	32
3						
4						
5						

SCALE ROOM ENVIRONMENTAL CONDITIONS

Scale #	Date	Time	By	WB	DB	%RH
6						
7						
8						
9						
Comments						

WOODSTOVE DATA SHEET #4-4
SCALE QA SHEET

Scale Mettler

Model AE100
SN K04827

Dates From 1/9/99

Through _____

Level	Recalibrated	100g Weight	10g Weight	1.0g Weight	100mg Weight	20mg Weight	Date	Time	Tech	Wet Bulb	Dry Bulb	% RH
✓	Yes P.O.	99.9999	10.0001	1.0002	1.003	.0203	1/9/99	1243	ATM	58	70	48
✓	No	100.0002	10.0000	1.0000	1.000	.0200	1/14/99	1113	ATM	62	75	47
✓	Yes P.O.	99.9999	10.0002	1.0000	0.999	.0201	1/23/99	1100	ATM	63	77	42
✓	Yes	99.9999	10.0000	1.0000	1.000	.0201	1/24/99	1318	ATM	59	74	45
✓	Yes	99.9996	10.0002	1.0000	1.000	.0200	2/1/99	0910	ATM	55	69	39
✓	Yes	99.9997	10.0001	1.0001	1.002	.0201	2/2/99	0939	ATM	60	73	46
✓	Yes	99.9999	10.0001	1.0001	1.001	.0200	2/3/99	1555	ATM	63	76	48
✓	Yes	99.9999	10.0000	1.0001	1.001	.0201	2/7/99	1235	ATM	62	76	45
✓	Yes	99.9998	10.0000	1.0000	1.000	.0200	2/10/99	1600	ATM	63	77	45
✓	Yes	99.9998	10.0000	1.0001	1.000	.0200	2/19/99	0246	ATM	64	78	46
✓	No	99.9999	10.0000	1.0000	1.000	.0200	2/21/99	1912	ATM	65	80	44
✓	No	99.9997	10.0000	1.0001	1.000	.0200	3/5/99	1935	ATM	64	80	41
✓	Yes P.O.	99.9997	10.0000	1.0000	1.001	.0200	3/6/99	1135	ATM	64	80	43
✓	Yes	99.9997	10.0000	1.0001	1.000	.0200	3/13/99	1526	ATM	65	80	44
✓	Yes	99.9999	10.0001	1.0001	1.001	.0200	3/14/99	1355	ATM	63	78	43
✓	No	100.0001	10.0000	1.0000	1.000	.0200	3/18/99	1622	ATM	66	81	45
✓	Yes	99.9997	10.0000	1.0001	1.000	.0200	3/18/99	2025	ATM	65	82	39
✓	Yes	99.9996	10.0000	1.0001	1.000	.0200	3/17/99	1615	ATM	62	77	42
✓	Yes	99.9997	10.0000	1.0001	1.000	.0200	3/18/99	2140	ATM	68	84	43
✓	Yes	99.9997	10.0000	1.0000	1.000	.0200	3/20/99	1300	ATM	64	84	32
✓	Yes	99.9999	10.0000	1.0001	1.001	.0201	3/21/99	2215	ATM	61	74	47
✓	Yes	99.9997	10.0000	1.0000	1.001	.0200	3/22/99	2127	ATM	65	85	33
✓	Yes	99.9997	10.0000	1.0001	1.000	.0200	3/23/99	1115	ATM	69	84	46
✓	Yes	99.9997	10.0000	1.0002	1.001	.0201	3/24/99	1120	ATM	77	89	43
✓	Yes	99.9999	10.0000	1.0002	1.001	.0201	3/29/99	2038	ATM	89	72	45
✓	No	99.9999	10.0002	1.0002	1.001	.0202	3/30/99	0610	ATM	66	80	47
✓	No	99.9999	10.0000	1.0000	1.001	.0201	3/31/99	1200	Sum	64	80	41
✓	No	99.9996	10.0000	1.0000	1.001	.0201	4/3/99	1730	ATM	64	80	41
✓	Yes	99.9998	10.0001	1.0001	1.001	.0201	4/6/99	1030	ATM	61	75	44
QC Services	Audit	4/6/97										
✓	No	100.0003	10.0001	1.0001	1.001	.0201	4/6/99	1720	ATM			
✓	Yes	99.9999	10.0001	1.0001	1.001	.0200	4/7/99	1724	ATM	65	85	33
✓	No	99.9996	10.0000	1.0001	1.001	.0201	4/8/99	1346	ATM	67	80	50
✓	Yes	99.9997	10.0000	1.0000	1.000	.0200	4/16/99	1230	ATM	66	82	42
✓	Yes	99.9997	10.0000	1.0000	1.000	.0200	4/17/99	1625	ATM	68	84	43

Woodstove Particulate
 Catch Processing Sheet
 Woodstove Data Sheet #5
 EPA M5G-1

Unit: High Valley XTEC
 Run: EPA 4
 Date: 3/23/99
 Technicians: ATM
 Revised 1/16/98-Data Sheet #5

Filters

Filter # (Front) 780 Beaker # 3
 Final Wt. .7988 g MI 50
 Tare Wt. .7888 g Desc. Acetone
 Net Wt. .0100 g

Final Wt. 67.8637 g ✓
 Tare Wt. 67.8571 g ✓
 Net Wt. .0066 g ✓

Filter # (Rear) 779 Beaker # _____
 Final Wt. .8012 g MI _____
 Tare Wt. .8034 g Desc. _____
 Net Wt. -.0022 g ✓

Final Wt. _____ g
 Tare Wt. _____ g
 Net Wt. _____ g

Acetone Blank Calculation: Blank Date: 3/13/99
 Blank Beaker # 8 Final Wt. 66.0215 g ✓
 MI 100 Tare Wt. 66.0213 g ✓
 Desc. Acetone Net Wt. 1.0002 g
1.0002 g ÷ 100 ml = .000002 g/ml

Blank Residue Value Calculation:

.000002 g/ml acetone X 50 ml acetone = .0001 g
 Blank Residue Value

Total Particulate Catch Calculation

Filter: .0100 g ✓
 Filter: -.0022 g ✓
 Beakers: .0066 g - .0001 g = .0065 g ✓
 Total Catch Blank Residue Value
 Total Catch = .0143 g ✓

Run # EPA # 4
 Date 3/23/99
 Technician ATM, RLS
 WST6-Form1, Rev8/96

MISCELLANEOUS TEST DATA
 WOODSTOVE DATA SHEET #8

Useable Firebox Dimensions: See QC Section Useable Volume: 2.713 ft³

Dilution Tunnel Draft (If applicable): Start 00.0 Stop 00.0

Test Chamber Air Velocity: Start: 00.0 Stop: 00.0 Avg: 00.0

Wet Bulb/ Start: WB: 55 °F DB: 67 °F 1.05 % Amb Moisture 45 %RH

Dry Bulb Stop: WB: 58 °F DB: 69 °F 1.40 % Amb Moisture 51 %RH

$\bar{X} = 1.225$ % Ambient Moisture $\bar{X} = 48$ % Relative Humidity (RH)

Empty Stove Wt: _____ lbs.

Empty Stove Wt with Stack (Inc. Oil Seal) Wet: 606.3 lbs. Dry: 604.4 lbs.

Empty Stove Wt with Stack and Ash Ash: 0 lbs. Total: 604.4 lbs.

Kindling Wt. Paper: 0.3 lbs. Wood: 5.0 lbs.

Pre Burn Fuel Wt. 17.9 + 17.5 + 16.5 Total: 51.9 lbs. ✓

Total Kindling and Pre Burn Fuel Wt 57.2 lbs. ✓

Coal Bed Wt-lbs: Range (608.7 - 607.9) 4.3 - 3.5 lbs. Actual: (3.5) lbs.

Allowable Amount of Charcoal that can be removed:

Coal Bed Wt. Range 4.3 + 3.5 12% .25 = .9 lbs.
 Upper Wt. Lower Wt.

Test Fuel Wt-lbs: Ideal 19.0 lbs. Range: 17.1 - 20.8 lbs. Actual: 17.3 lbs.

Test Fuel Size (pcs.) (.75 x 1.5 x 5" Flanges) 20 Pcs.

2 x 4's x 15^{5/8} " 6 Pcs 9.2 lbs. 53.2 % ✓

4 x 4's x 15^{5/8} " 2 Pcs 8.1 lbs. 46.8 % ✓

Est. Dry Burn Rate (Kg/Hr.) $\frac{17.3 - (17.3 \times .1715)}{2.2046} \times \frac{60}{285} = \frac{1.368}{}$ Est. Dry Burn Rate (Kg/Hr) ✓

Est EPA Heat Output (HO_E) (19,140) x $\frac{63}{100} \times \frac{1.368}{}$ = 16,491.4 Est Heat Output (HO_E) BTU's/Hr ✓

Comments:

Stove Operating Data
Woodstove Test Data Sheet #9
Cold Start

Unit: HIGH VALLEY X-TEC
Run: EPA #4
Date: 3/23/99
Technician(s): ATH, RLS,
Data Sheet #9 - Rev 1/98-Pg.2

Fire Started: 0833 P.S.T.

Warm up and Preburn: Primary Air: Wide open from ignition until the start of preburn when the primary air control(s) was (were) adjusted to the run setting of 1/4" OPEN. At the run setting until the start of the test.

Secondary Air: No Controls. Naturally drafted.

Secondary Burn/Cat Bypass: N/A

Charcoal Bed Preparation: Broke up, raked and leveled the coal bed prior to the addition of each warm up/pre burn fuel charge. Starting 1130 before the start of the test, broke up, raked and leveled the coal bed. In stove for 35 seconds.

Test: Door wide open during loading 1 min 00 sec, then closed.

Primary Air: Wide open during the start of the test until 4:55. Adjusted to the run setting of 1/4" between 4:55 and 5:00. At the run setting of 1/4" at 5:00 into the run.

Secondary Air: No Controls. Naturally drafted.

Secondary Burn/Cat Bypass: N/A

Fan: ON / OFF during the warm up, ON / OFF high during the preburn, ON / OFF at the start of the test, ON / OFF for the first 30 minutes of the test, ON / OFF high at 30 minutes into the test, ON / OFF for the rest of the test.

Test Run Anomalies: Very good start & run.

WOODSTOVE OPERATING DATA
 WOODSTOVE DATA SHEET #9A-1

Wood Data: Kindling: A mix of the below grades

	Size	Mill	Grade	Species
Pre Burn	<u>2x4</u>	<u>CANYON LBR.</u>	<u>STD. & BTR.</u>	<u>D. FIR, S. GRN.</u>
Test Fuel	<u>2x4</u>	<u>CANYON LBR.</u>	<u>#2 STD. & BTR.</u>	<u>D. FIR, S. GRN.</u>
	<u>4x4</u>	<u>STAND #879</u>	<u>#2 STD. & BTR.</u>	<u>D. FIR, S. GRN.</u>

All grades WCLB Rules unless otherwise noted.

Warm up Information:

1st Warm up/Pre Burn Fuel charge (17.9 lbs) added at 0845.
 2nd Warm up/Pre Burn Fuel charge (17.5 lbs) added at 0933.
 3rd Warm up/Pre Burn Fuel charge (16.5 lbs) added at 1046.
 4th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.
 5th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.
 6th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.
 7th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.
 8th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.

The coals were scooped out of the stove immediately prior to adding the 3 ^{pre} pre burn/warm up fuel charge. The stove lost 1.9 lbs. 3.0 lbs of coals back in after scoop.

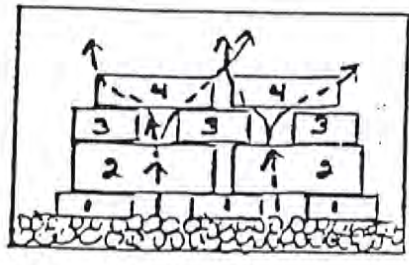
All pre burn/warm up fuel pieces were either 16 or _____ inches long. All preburn pieces/fuel charges were "ricked" in the stove. The pieces in the bottom layer in each rick contained 2 pcs that were 16 inches long and were loaded flat and perpendicular to the door. The pieces in the second layer in each rick were loaded on their side (edge) approximately parallel to the door and contained 4 pcs 16 inches long. The third layer (and fourth layer if present) was loaded flat, perpendicular to the door and contained 3 pcs 16 inches long. The majority of the pieces in each rick were in the second layer which had an approximate 0.5-1.0" space between pieces. (The loading directions indicate the direction of the longest dimension on each piece relative to the loading door opening.) Each pre burn/warm up fuel charge normally weighs within the weight range allowed for the actual test fuel charge

WOODSTOVE OPERATING DATA
WOODSTOVE DATA SHEET #9A-2

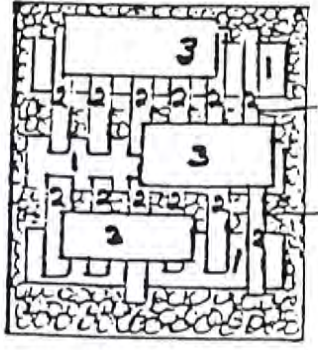
Run # EDA #4
Date 3/23/99
Technician ATM, PLS.
Page 2 of 3
WST7-Form2-A, Rev 6/90

Warm up Information (cont.):

Each warm up/preburn fuel charge was ricked in exactly (as much as possible) the same manner and the weight of each rick was usually within the allowable weight range for the test fuel charge. The physical arrangement and alignment of each rick was designed to accomplish three (3) things: (1) The bottom layer was nestled firmly into the coal bed and was as close to being level with the bottom of the stove as possible, thus providing a stable loading platform for the rest of the rick, keeping it in a ricked state (as opposed to a collapsed or fallen down state) until the rick reached the charcoal stage and sags or collapses of its own accord. (2) It enhances the flow of primary air through the ricked preburn fuel charge, for the primary air would flow through the spaces between the pieces in the first layer and then up through the spaces between the pieces in the second, third and, if present, fourth layers. (3) It maximized, as much as possible, the surface to volume ratio of each preburn fuel charge, thereby allowing the fire immediate access to as much wood surface as possible and, thereby, insuring uniform charcoalization. All three of these enhance combustion and so get the stove as hot as possible during the warm up period, thereby maximizing the amount of heat (BTU's) stored in the stove. The actual preburn was not started until the stove surface temperatures had maximized and stabilized, thus indicating that the amount of heat stored in the stove had peaked. For this stove, the thermal storage was monitored using the TOP surface temperature(s) and the peak value(s) obtained were 960 of.



Front View



Top View

The arrows indicate the direction of the air flow through the rick.

The primary air was adjusted to the run setting of 1/4" open 6.0 lbs above the upper charcoal bed weight.

WOODSTOVE OPERATING DATA
WOODSTOVE DATA SHEET #9A-3

Unit HIGH VALUE X-TEC
Run # EPA #4
Date 3/23/99
Technician ATM, RLS
Page 3 of 3
WST5-Form2-Rev11/89

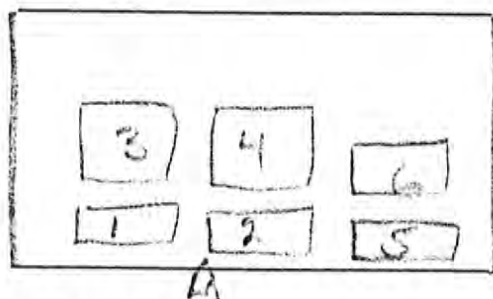
Additional Comments:

Test Start Sequence:

- ① Turned Fan Off
② Opened primary air control wide open
③ Opened door
④ loaded fuel
⑤ clear coals away from in front of / PAO
⑥ Photograph
⑦ closed door

Test Fuel Charge Loading Information:

Test Fuel Charge and Loading Sequence Diagram



FRONT

of stove view

4 X 4's: 3 & 4

2 X 4's: 1, 2, 5 & 6

Loading Sequence: 1, 2, 3, 4, 5 & 6 last

Driest Pcs in Load 2 & 5

Loaded the test fuel charge on an essentially level, medium to mostly sized, hot coal bed (in appearance, color and temperature for a med Hi burn rate. Load: 1100 Igniter 10:55 So. 11:15 VC to baffle 11:35 2nd igniting at top of the VC 11:50 2nd Tube igniting 01:11 Front Tube igniting. 01:50 - 01:25 Gas Balance 01:00 Flames decreased. Maintained two VC's, one in each canyon, 2nds on top of both VC's, 2nd tube stayed lit. Next loss gas balance.

FUEL MOISTURE
WOODSTOVE TEST DATA SHEET #10

Unit: HIGH VALLEY X-TEC
Run: EPA #4
Date: 3/23/99
Technician: ATM, RLS,
WST1-Form7-Rev11/89

Room Temperature: 69 °F

Correction Factor: 0

NOTE: Record readings to the nearest 0.5% moisture
Uncor Values are corrected for temperature: Yes No
Time Test Fuel Moisture Readings taken at: 1035 ✓
Calibration Checks: X Y 12.5 12.5 22.0 22.2

Pc #	Dimen	Use	Top		Bottom		Side		Piece Avg Corrected
			Uncor	Cor	Uncor	Cor	Uncor	Cor	
1	2x4x8'	K	12.5	13.3	12.5	13.3	12.0	12.8	(13.133)
2									
3									
4	2x4x8'	P	20.5	22.0	20.0	21.4	20.0	21.4	21.600
5	"	P	21.0	22.6	21.5	23.1	21.5	23.1	22.933
6	"	P	21.0	22.6	21.5	23.1	21.5	23.1	22.933
7	"	P	21.5	23.1	21.5	23.1	21.5	23.1	23.100
8	"	P	22.0	23.7	22.0	23.7	21.5	23.1	23.500
9									(114.066)
10									
11	2x4x15 1/8"	T	18.0	19.2	18.0	19.2	18.0	19.2	19.200
12	"	T	18.5	19.8	18.5	19.8	18.5	19.8	19.800
13	"	T	20.5	22.0	20.0	21.4	19.5	20.9	21.433
14	"	T	21.0	22.6	21.5	23.1	21.0	22.6	22.767
15									
16	4x4x15 1/8"	T	18.5	19.8	18.5	19.8	19.0	20.3	19.967
17	"	T	20.0	21.4	20.0	21.4	20.5	22.0	21.600
18									(124.767)
19	FEET	T	18.5	19.8	18.5	19.8	19.0	20.3	(19.967)
20									(OUT SPACERS)

	Kindling	Pretest Fuel	Test Load
% Moisture - Dry Basis:	13.133%	22.813%	20.795%
% Moisture - Wet Basis:	11.609%	18.571%	17.215%

To obtain Wet from Dry: $\frac{100 \times \% \text{ Dry Rdg.}}{100 + \% \text{ Dry Rdg.}} = \% \text{ Moisture, Wet Basis}$

Acceptable Ranges: 16-20% wet; 19-25% dry
(17.5 - 22.5 on Meter [Uncor reading] at 70°F)

Key for Use: K= Kindling P= Pretest Fuel T= Test Fuel

WOOD DENSITY DETERMINATION
WOODSTOVE TEST DATA SHEET #11

Unit: HIGH VALLEY-X-TEC
Run#: EPA # 4
Date: 3/23/99
Technician: ATM, RLS,
WST2-form11-Rev 6/90

Wood Piece: Nominal Dimensions: 3 1/2" x 3 1/2" x 1 1/2"
Depth (D): in 1.549 cm 3.934 ✓
Width (W): in 3.507 cm 8.908 ✓
Length (L): 3.531 cm ✓
3.551 cm ✓
3.565 cm ✓
3.554 cm ✓
Length \bar{X} = in 3.5503 cm 9.018 ✓
Volume: 316.027 cm³ ✓
(D X W X L)

MOISTURE: Room Temperature: 70 °F Correction Factor: 0

Uncorrected Meter Readings Corrected for temperature: Yes No

NOTE: Record moisture meter readings to the nearest 0.5%

	Uncor	Cor
Top:	<u>22.0</u>	<u>23.7</u> %
Bottom:	<u>21.5</u>	<u>23.1</u> %
Side:	<u>21.5</u>	<u>23.1</u> %
\bar{X} :		<u>23.300</u> % ✓

Avg. % Moisture (Dry) 23.300 % ✓

Avg % Moisture (Wet) 18.897 % ✓

Scale: Leveled In Out

Zeroed: In Out

Wet Weight: 203.9 g Dry Weight: 169.5 g

% Moisture Dried Basis: 16.871 % ✓
[1 - (Dry Wt ÷ Wet Wt)] X 100

Into Dryer Date 3/23/99 Time 1025 Temp 219 °F
Out of Dryer Date 3/29/99 Time 1415 Temp 218 °F

(Minimum Time in Dryer: 24 hrs.) Minimum Dryer Temp 100°C (212°F)

Density = $\frac{169.5}{(dry\ wt)}$ g ÷ $\frac{316.027}{(volume)}$ cm³ = 0.5363 g/cm³ ✓

Pellet Fuel Moisture Content Determination

Tare Beaker Wt. _____ g
Wet Wt: _____ g - _____ g = _____ g
Gross Wet Wt. Tare Beaker Wt. Net Wet Wt.
Dry Wt: _____ g - _____ g = _____ g
Gross Dry Wt. Tare Beaker Wt. Net Dry Wt.

% Moisture Dried Basis: _____ %
[1 - (Net Dry Wt ÷ Net Wet Wt.)] X 100

BU STATE AND FLUE GAS DATA
 WOODSTOVE DATA SHEET #12
 WST2-Form 14 Rev 1/88
 Envoy Wt.: 607.9 lbs.

Unit: HIGH VALLEY X-TEC
 Run: EPA # 4
 Page: 1 of 3

Date: 3/23/99
 Technician(s): ATM, PLS.

Minute Time	Scale Wt	lbs Left	Burn Rate	CO ₂		O ₂		Tel	CO	T/C(1)/T/C(2)			T/C(3)			Static Press.	Comments	
				v.	%CO ₂	v.	%O ₂			Bal	Wet Bulb	Dry Bulb	% H ₂ O	Calc W/B	Stack			SO ₂ v.
0	1235	125.2	17.3	22.6	5.64	56.5	14.16		1.20	4.7	8.4	12.5	2.5	110	305		-0.59	Flow
5	40	124.2	16.3	4.35	10.84	36.0	9.02	GAS BAL.	0.38	28.5	10.3	14.9	5.9	127	387		-0.85	SO ₂ 1.5
10	45	123.4	15.5	1.38	9.50	42.3	10.60		0.80	11.9	12.4	15.1	12	140	407		-0.76	SO ₂ 1.5
15	50	122.4	14.5	1.47	11.73	35.3	8.84		0.49	23.9	13.1	15.4	15	144	410		-0.79	SO ₂ 1.5
20	55	121.5	13.6	1.48	12.03	34.1	8.54		0.34	35.4	13.2	15.4	15.5	146	414		-0.80	SO ₂ 1.5
25	1500	120.4	12.5	1.52	13.07	30.4	7.61		0.21	62.3	13.3	15.2	16	148	424		-0.81	
30	05	119.4	11.5	1.58	14.14	24.2	6.06		0.16	91.5	13.4	15.7	16.5	149	439		-0.82	
35	10	118.5	10.6	1.57	14.27	26.0	6.57		0.20	71.3	13.4	16.0	16.5	149	444		-0.81	
40	15	117.5	9.6	1.57	14.29	25.4	6.36		0.17	84.1	13.3	16.1	15.5	147	443		-0.81	
45	20	116.7	8.8	1.53	12.78	31.3	7.84		0.22	58.1	13.0	15.9	14	144	430		-0.80	
50	25	115.8	7.9	1.54	13.50	27.7	6.93		0.26	57.9	13.0	15.9	14	144	428		-0.78	
55	30	115.0	7.1	1.52	13.07	29.5	7.39		0.15	87.2	12.8	15.8	13	142	422		-0.77	
60	35	114.2	6.3	1.50	12.70	31.0	7.76		0.18	70.6	12.6	15.7	12.5	141	417		-0.75	SO ₂ 1.5
65	40	113.6	5.7	1.46	11.57	35.5	8.89		0.24	48.0	12.3	15.5	11.5	140	405		-0.73	SO ₂ 1.5
70	45	113.1	5.2	1.43	10.76	37.7	9.44		0.16	67.3	12.0	15.2	10.5	137	394		-0.71	SO ₂ 1.5
75	50	112.6	4.7	1.39	9.74	42.0	10.52		0.24	40.6	11.6	15.0	9	133	382		-0.70	SO ₂ 1.5
80	55	112.2	4.3	1.34	8.55	46.6	11.68		0.33	25.9	11.1	14.6	7.7	130	365		-0.67	
85	1400	111.9	4.0	1.38	7.93	48.6	12.18		0.38	20.9	10.6	14.2	6.5	125	351		-0.66	
90	05	111.7	3.8	1.29	7.41	50.1	12.55		0.50	14.8	10.2	13.9	5.5	122	340		-0.64	
95	10	111.5	3.6	1.28	6.98	57.5	12.90		0.62	11.3	9.9	13.7	5	120	331		-0.63	
100	15	111.3	3.4	1.27	6.91	57.8	12.98		0.65	10.6	9.7	13.5	4.5	119	324		-0.62	
105	20	111.1	3.2	1.25	6.26	54.6	13.68	OUT BAL.	0.78	8.0	9.4	13.3	4	116	317		-0.60	
110	25	111.0	3.1	1.21	5.29	57.4	14.38		1.13	4.7	9.0	13.1	3.3	113	308		-0.60	
115	30	110.8	2.9	1.22	5.57	56.2	14.08		1.11	5.0	8.8	12.8	3.1	112	301		-0.59	
120	35	110.7	2.8	1.22	5.57	56.2	14.08		1.11	5.0	8.8	12.8	3.1	112	301		-0.59	

1230

1250

2100

1200

BU RATE AND FLUE GAS DATA
 WOODSTOVE DATA SHEET #12
 WST2-Form 14 Rev 1/88
 ENO WT: 607.9 lbs.

Minute	Scale Wt	lbs left	Burn Rate	CO ₂		O ₂		CO		T/C(1)T/C(2)		T/C(3)		Static Press.	Comments		
				v.	%CO ₂	v.	%O ₂	TeI	Wet Bulb	Dry Bulb	% H ₂ O	Calc W/B	Stack			S0 ₂ v.	PPM
120	610.7	2.8	.1	.217	5.42	56.7	14.21	24.5	1.24	4.4	86	126	2.8	110	294		Flow
125	610.6	2.7	.1	.214	5.34	57.0	14.28	25.0	1.26	4.2	85	125	2.6	109	288		S0 ₂ 1.5
130	610.5	2.6	.1	.215	5.37	56.9	14.26	24.8	1.25	4.3	85	124	2.7	108	284		CO ₂ 1.5
135	610.4	2.5	.1	.198	4.95	58.7	14.71	25.1	1.28	3.9	84	124	2.5	108	279		CO ₂ 1.5
140	610.3	2.4	.1	.203	5.07	58.1	14.56	22.7	1.15	4.4	83	123	2.4	107	275		CO ₂ 1.5
145	610.2	2.3	.1	.212	5.29	57.5	14.41	22.5	1.14	4.6	83	122	2.4	107	272		CO ₂ 1.5
150	610.1	2.2	.1	.212	5.29	57.6	14.44	22.9	1.16	4.6	82	121	2.3	106	269		CO ₂ 1.5
155	610.0	2.1	.1	.208	5.20	58.1	14.56	21.3	1.08	4.8	82	120	2.3	106	266		CO ₂ 1.5
160	609.9	2.0	.1	.207	5.17	58.3	14.61	21.4	1.09	4.7	82	119	2.3	105	264		CO ₂ 1.5
165	609.8	1.9	.1	.205	5.12	58.3	14.61	22.9	1.16	4.4	81	119	2.2	105	262		CO ₂ 1.5
170	609.7	1.8	.1	.211	5.27	57.6	14.44	23.7	1.20	4.4	81	119	2.2	104	259		CO ₂ 1.5
175	609.6	1.7	.1	.216	5.39	57.1	14.31	23.8	1.20	4.5	82	119	2.3	104	258		CO ₂ 1.5
180	609.5	1.6	.1	.207	5.17	58.0	14.54	23.7	1.19	4.3	82	119	2.3	104	256		CO ₂ 1.5
185	609.4	1.5	.1	.206	5.15	58.1	14.56	24.1	1.23	4.2	82	119	2.3	104	254		CO ₂ 1.5
190	609.3	1.4	.1	.201	5.02	58.7	14.71	24.3	1.23	4.1	81	119	2.2	104	252		CO ₂ 1.5
195	609.2	1.3	.1	.188	4.70	59.9	15.01	25.9	1.32	3.6	81	118	2.2	104	250		CO ₂ 1.5
200	609.1	1.2	.1	.183	4.57	60.2	15.09	27.2	1.36	3.4	81	118	2.2	103	248		CO ₂ 1.5
205	609.0	1.1	.1	.178	4.45	60.7	15.21	27.4	1.38	3.2	80	117	2.1	103	246		CO ₂ 1.5
210	608.9	1.0	.1	.167	4.18	62.0	15.54	27.4	1.39	3.0	80	116	2.2	103	243		CO ₂ 1.5
215	608.8	.9	.1	.157	3.93	62.9	15.76	28.1	1.42	2.8	79	115	2.1	103	241		CO ₂ 1.5
220	608.7	.8	.1	.154	3.85	63.1	15.82	28.1	1.42	2.6	79	115	2.1	102	239		CO ₂ 1.5
225	608.6	.7	.1	.151	3.90	63.0	15.79	29.5	1.49	2.6	79	114	2.1	102	236		CO ₂ 1.5
230	608.5	.6	.1	.152	3.80	63.2	15.84	30.8	1.55	2.5	79	114	2.1	102	234		CO ₂ 1.5
235	608.5	.6	0	.147	3.68	64.0	16.04	27.7	1.40	2.6	79	112	2.2	102	231		CO ₂ 1.5
240	608.5	.6	0												2930		CO ₂ 1.5

BURN RATE AND FLUE GAS DATA
 WOC JVE DATA SHEET #12
 WST2-Form 14 Rev 1/88
 ENO WT. 607.9 lbs

Unit: HIGH VALLEY X-TEC Date: 3/23/99
 Run: EPA #4 Technician(s): A.T.I., J. Ren, PLS,
 Page: 3 of 3

Minute Time	Scale Wt	lbs left	Burn Rate	CO ₂		O ₂		3 T/C(1) T/C(2)				4 T/C(3)				Static Press.	Comments
				v.	%CO ₂	v.	%O ₂	Tel	CO v.	%CO	Bal	Wet Bulb	Dry Bulb	% H ₂ O	Calc W/B		
240	608.4	.5	.1	.139	3.48	64.8	16.24										
245	608.3	.4	.1	.134	3.36	65.3	16.37										
250	608.2	.3	.1	.132	3.31	65.8	16.49										
255	608.2	.3	0	.129	3.23	66.2	16.59										
260	608.1	.2	.1	.123	3.08	67.2	16.84										
265	608.1	.2	0	.121	3.03	67.5	16.92										
270	608.0	.1	.1	.108	2.71	68.9	17.27										
275	608.0	.1	0	.104	2.61	69.3	17.37										
280	608.0	.1	0	.101	2.54	69.8	17.50										
285	607.9	0	.1	.098	2.46	70.1	17.57										
290																	
295																	
300																	
305																	
310																	
315																	
320																	
325																	
330																	
335																	
340																	
345																	
350																	
355																	

T/C#	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
Minute / Time	Stove Top	Left Side	Back	Right Side	Bottom	Firebox	2nd Burn Gas	Room Temp	Tunnel	C. Gas Box	Impinger Out	5G-1 Filter	5G-1 Condenser	Con- dar	
0	400	4100	420	525	500	570	921	70	109	250	42	84	47	257	
5	425	449	449	571	498	545	1211	71	149	250	42	86	39	257	
10	509	439	389	496	499	525	1300	72	132	257	42	87	39	257	
15	547	431	371	487	495	508	1291	70	127	257	42	87	39	257	
20	568	426	366	480	488	498	1328	70	127	257	42	88	39	250	
25	593	425	367	479	481	492	1311	70	128	250	42	88	39	250	
30	630	427	374	483	474	493	1347	69	130	250	42	88	39	250	
35	640	440	374	497	468	507	1375	70	128	250	42	88	38	250	
40	639	452	378	510	463	519	1376	70	127	257	42	88	38	250	
45	628	463	387	522	458	532	1399	71	125	250	43	88	39	257	
50	620	472	397	533	455	544	1423	71	124	250	43	88	39	257	
55	609	482	408	544	453	558	1420	71	123	250	43	88	39	257	
60	598	493	422	553	452	571	1396	71	123	250	43	88	39	257	
65	586	502	435	560	452	584	1324	72	121	257	43	88	39	257	
70	569	506	450	561	454	592	1311	71	119	257	44	88	39	257	
75	550	509	468	561	456	600	1240	72	117	257	43	88	39	257	
80	524	507	486	558	458	605	1176	72	115	257	44	88	39	250	
85	501	502	498	555	459	606	1141	72	113	250	44	88	39	250	
90	479	495	494	550	461	606	1104	71	111	250	44	87	39	250	
95	460	490	486	545	463	605	1111	70	110	250	44	87	39	250	
100	446	486	479	539	464	606	1092	71	109	250	44	86	39	250	
105	431	483	472	531	466	606	1026	70	107	250	44	86	39	250	
110	416	480	458	522	469	606	970	70	106	250	44	86	39	249	
116	402	474	449	514	471	599	950	70	104	250	44	85	39	250	
120	396	472	452	514	471	599	950	70	104	250	44	85	39	250	

13,770 11,993 10,247 13,616 11,257 13,497 29,543 1697

PRE AND POST TEST ZERO/SPAN CHECK
WOODSTOVE DATA SHEET #15-1

Site: Myren Consulting, Woodinville, WA Date: 3/23/99 Analyte: CO₂

Source: HIGH VALLEY X-TEC Run #: EPA #4

Zero Cyl #: 36919 Conc. 00.0 % CO₂ Cyl Press: 230 psi

Certified by: CASCADE AIRGAS Date: 4/24/96

Span Cyl #: 250-1060 Conc. 6.0 % CO₂ Cyl Press: 1470 psi

Certified by: OXARC Date: 8/22/97

Analyzer: Make: Horiba Model: PIR-2000 SN: 607024

Range: 0 - 25.0% CO₂ Analyzer Output: 0 - 1.0 v.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter:

EPA Span Value = 25.0% CO₂

EPA Control Limits = + 2.5% of 25.0% CO₂ = + 0.625% CO₂

Pre Run Audit: By: ATH, RLS Time: 1135 Temp: 71 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	00.0	.000	0.2556	+0.2556	+0.10
Span	24.0	1.240	6.0	6.0	.239	5.966	-0.3415	-0.57

Comments:

Post Run Audit: By: ATH, RLS Time: 1743 Temp: 69 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	00.0	.000	0.2556	+0.2556	+0.10
Span	24.0	1.240	6.0	5.8	.238	5.9410	-0.05900	-0.98

Comments:

+ Conc. Difference = Act % - Exp (Std) %

Zero % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$

Span % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

PRE AND POST TEST ZERO/SPAN CHECK
WOODSTOVE DATA SHEET #15-2

Site: Myren Consulting, Woodinville, WA Date: 3/23/99 Analyte: O₂

Source: HIGH VALLEY X-TEC Run #: EPA # 4

Zero Cyl #: 36919 Conc. 00.0 % O₂ Cyl Press: 230 psi

Certified by: CASCADE AIRGAS Date: 4/24/96

Span Cyl #: 250-1060 Conc. 6.0 % O₂ Cyl Press: 1470 psi

Certified by: OXARC Date: 8/22/97

Analyzer: Make: Taylor Model: OA 137 SN: 137/4772

Range: 0 - 25.0% O₂ Analyzer Output: 0 - 100 mv.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter: _____

EPA Span Value = 25.0% O₂

EPA Control Limits = + 2.5% of 25.0% O₂ = + 0.625% O₂

Pre Run Audit: By: ATM, RLS Time: 1135 Temp: 71 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ%
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	00.0	00.0	-0.01547	-0.01547	-0.06
Span	6.0	24.0	6.0	6.0	23.9	5.981	-0.01946	-0.32

Comments:

Post Run Audit: By: ATM, RLS Time: 1743 Temp.: 69 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ%
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	00.0	00.0	-0.01547	-0.01547	-0.06
Span	6.0	24.0	6.0	6.0	23.9	5.981	-0.01946	-0.32

Comments:

+ Conc. Difference = Act % - Exp (Std) %
 Zero % Differenece = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$
 Span % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

PRE AND POST TEST ZERO/SPAN CHECK
WOODSTOVE DATA SHEET #15-3

Site: Myren Consulting, Woodinville, WA Date: 3/23/99 Analyte: CO

Source: HIGH VALLEY X-TEC Run #: EPA #4

Zero Cyl #: 36919 Conc. 00.0 % CO Cyl Press: 230 psi

Certified by: CASCADE AIRGAS Date: 4/24/96

Span Cyl #: 250-1060 Conc. 1.26 % CO Cyl Press: 1470 psi

Certified by: OXARC Date: 8/22/97

Analyzer: Make: Infra Red Model: 702 D SN: 113

Range: 0 - 10.0% CO Analyzer Output: 0 - 100 mv.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter:

EPA Span Value = 5.0% CO

EPA Control Limits = +2.5% of 5.0% CO = + 0.125% CO

Pre Run Audit: By: ATM, RLS Time: 1135 Temp: 71 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.00	00.0	0.0091	-0.0091	-0.18
Span	1.26	25.2	1.26	1.26	25.0	1.2467	-0.0133	-1.05

Comments:

Post Run Audit: By: ATM, RLS Time: 1743 Temp.: 69 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.00	00.0	0.0091	-0.0091	-0.18
Span	1.26	25.2	1.26	1.24	24.7	1.2316	-0.0283	-2.25

Comments:

+ Conc. Difference = Act % - Exp (Std) %

Zero % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$

Span % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

Run: EPA #4
 Date: 3/23/99
 Technicians: ATH, PLS.
 WST6-Form3-Rev11/89

QUALITY CHECKS
 WOODSTOVE DATA SHEET #16

Ambient = Tr: 66 °F T/C#30: _____ °F
 Thermocouple Check (at ambient): T/C#1: 66 °F; T/C#2: 65 °F;
 T/C #3: 120 °F; T/C #4: 134 °F; T/C #5: 198 °F;
 T/C #6: 171 °F; T/C #7: 189 °F; T/C #8: 245 °F;
 T/C #9: 259 °F; T/C #10: 150 °F; T/C #11: 66 °F;
 T/C #12: 65 °F; T/C #13: 63 °F; T/C #14: 62 °F;
 T/C #15: 64 °F; T/C #16: 65 °F; T/C #17: 65 °F;
 T/C #18: _____ °F; T/C #19: _____ °F; T/C #20: _____ °F;
 T/C #21: _____ °F; T/C #22: _____ °F; T/C #23: _____ °F;
 T/C #24: _____ °F; T/C #25: _____ °F; T/C #26: _____ °F;

Comments: STOVE STILL WARM FROM OVER NIGHT BURN.

Thermocouple Readout: Pretest Zero/Span Check and Calibration:
 Zero (0°F) : 000 °F Adj to: 000 °F Post Test Check Zero (0°F): 600 °F % Difference 0
 Span (2000°F): 1999 °F Adj to: 2000 °F Span (2000°F): 2000 °F 0
 (Allowable % Difference = 1.5%. Use formulas on Woodstove Data Sheet #15 to calculate % Difference)

Thermocouple Readout Pretest Linearity Check
 0°F = 000 °F; 200°F = 201 °F; 400°F = 399 °F;
 600°F = 600 °F; 800°F = 799 °F; 1000°F = 1000 °F;
 1200°F = 1200 °F; 1400°F = 1400 °F; 1600°F = 1599 °F
 1800°F = 1800 °F; 2000°F = 2000 °F

Combustion Gas (CO₂, O₂, CO) Train Leak Check: Pre Post
 Draft (Static) Gauge Zero Check: Pre Post

Scale Check Pre (Wt, #'s): 606.3 - 611.3 5.0 lbs. OK (PLS)
 Post (Wt, #'s): 607.9 - 612.9 5.0 lbs. OK (PLS)

Stack cleaned prior to the run: Yes _____ No
 Tunnel cleaned prior to the run: Yes _____ No

Becherini Scale Center, Inc.
 317 E. Sprague
 Spokane, WA 99202

SCALE CALIBRATION RECORD

Customer: Myron Consulting Date: 9/9/98
 Work Order Number: _____ PO Number: _____

Equipment Mfg.	Serial Number	Specifications	Weight used	Initial Readings	Final Readings
1. <u>Panther</u>	<u>4466459</u>	<u>1000X .1lb</u>	<u>Ø</u>	<u>Ø</u>	<u>Ø</u>
	<u>Pass</u> Fail		<u>100.0</u>	<u>100.0</u>	<u>100.0</u>
Notes:			<u>200.0</u>	<u>199.9</u>	<u>200.0</u>
			<u>500.0</u>	<u>499.8</u>	<u>500.0</u>
			<u>Ø</u>	<u>Ø</u>	<u>Ø</u>

Equipment Mfg.	Serial Number	Specifications	Weight used	Initial Readings	Final Readings
2.					
	Pass...Fail				
Notes:					

Equipment Mfg.	Serial Number	Specifications	Weight used	Initial Readings	Final Readings
3.					
	Pass...Fail				
Notes:					

Equipment Mfg.	Serial Number	Specifications	Weight used	Initial Readings	Final Readings
4.					
	Pass...Fail				
Notes:					

Additional Comments: _____

Last Checked: 3-98 Next Check Due: 3-99
 Weights Certified: _____ Technician: Paul Fisher

DENSITY STANDARD USED FOR TROEMNER PRECISION WEIGHTS

Troemner Inc. adjusts all new weights and all weights received for recalibration on the basis of apparent mass versus material of density 8.0g/cm³ at 20°C. This action is in accordance with the recommendations of the American Society for Testing and Materials specification ANSI/ASTM E 617 and the International Organization of Legal Metrology (OIML) International Recommendation No. 20.

Previously, all weights had usually been adjusted on the basis of apparent mass versus "brass," a hypothetical material of defined density 8.4g/cm³ at 0°C and 8.3909g/cm³ at 20°C. This practice originated in the early 1800's and was adopted in all of the English speaking countries as well as a number of other countries. Now most mass standards and test weights are made from stainless steel (density ranges from 7.77g/cm³ to 8.0g/cm³). A number of countries have adopted the recommendations of OIML and the foremost balance manufacturers are adjusting the built-in weights in their balances on the basis of apparent mass versus 8.0g/cm³. In order to smooth the transition in this country, the Reports of Calibration of the National Bureau of Standards are reporting the corrections to calibrated mass standards on both bases.

In terms of normal weighting procedures the change is very small. For a given weight, the mass value assigned on the basis of apparent mass versus density 8.0g/cm³ material will be 7 parts per million higher than the value assigned on the basis of apparent mass versus "density 8.4g/cm³" material. In many cases the allowed weight adjustment tolerances are so

large that this change is immaterial although closely adjusted weights often have a smaller tolerance than the correction change. For example at the 1 kilogram level the change is 7 mg. For comparison the ANSI/ASTM E 617 Class 6 tolerance for 1 kilogram is 100 mg while the Class 1 tolerance is 2.5 mg. A detailed discussion of mass and mass values is given in Reference 3.

Precision Weights manufactured by Troemner Inc. to ASTM Class 1, 1.1, 2, 3, 4, 5, and 6 tolerances and the equivalent OIML and NBS tolerances are of the following materials:

Designation	Base Material	Density	Weight Range
Stainless Steel	18-8	7.84g/cm ³ at 20°C	1 g & larger
Stainless Steel	18-8	8.0g/cm ³ at 20°C	50 mg to 500 mg
Aluminum	1100	2.7g/cm ³ at 20°C	30 mg & smaller

References:

- ANSI/ASTM E 617
Available from: Troemner Inc. 6825 Greenway Ave., Phila., Pa. 19142
215-724-0800 or American Society for Testing and Materials, 1916 Race Street, Phila., Pa. 19103
- OIML INTERNATIONAL RECOMMENDATION No. 20
Available from: Organisation Internationale De Metrologie Legale
11 Rue Trudon - 75009 Paris, France
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QUALITY CONTROL SERVICES

LABORATORY AND METROLOGY EQUIPMENT: SALES AND SERVICE

Date: 04/13/1999

Customer: Myren Consulting
512 Williams Lake Road
Colville, WA 99114
Attn: Ben Myren

CERTIFICATE OF CALIBRATION

THE INSTRUMENTS LISTED BELOW HAVE BEEN SERVICED AND CALIBRATED BY QUALITY CONTROL SERVICES ON THE DATE INDICATED. SERVICE CONSISTS OF ACCURACY TESTS, ADJUSTING TO MANUFACTURER OR CUSTOMER SPECIFICATIONS AND COMPLETE CALIBRATION WITH STANDARDS TRACEABLE TO THE NATIONAL INSTITUTE OF STANDARDS AND TECHNOLOGY (N.I.S.T.).

Item:	Make:	Model:	Serial Number:	Location:	Contact:	Cal. Date:	Cal. Due:
Balance	Mettler	AE100	K04827	Lab	Ben Myren	04/06/1999	09/1999

STANDARDS USED FOR THIS CALIBRATION:

Item:	Make:	Model:	Serial Number:	NIST ID:	Cal. Date:	Cal. Due:
Weight Set	Rice Lake	IMG-20KG	A45	822/251337	07/07/1998	07/1999

Technician: D.Deleasa

Signature

D. Deleasa

QUALITY CONTROL SERVICES

LABORATORY AND METROLOGY EQUIPMENT: SALES AND SERVICE

Date: 10/29/1998

Customer: Myren Consulting
512 Williams Lake Road
Colville, WA 99114
Attn: Ben Myren

CERTIFICATE OF CALIBRATION

THE INSTRUMENTS LISTED BELOW HAVE BEEN SERVICED AND CALIBRATED BY QUALITY CONTROL SERVICES ON THE DATE INDICATED. SERVICE CONSISTS OF ACCURACY TESTS, ADJUSTING TO MANUFACTURER OR CUSTOMER SPECIFICATIONS AND COMPLETE CALIBRATION WITH STANDARDS TRACEABLE TO THE NATIONAL INSTITUTE OF STANDARDS AND TECHNOLOGY (N.I.S.T.).

Item:	Make:	Model:	Serial Number:	Location:	Contact:	Cal. Date:	Cal. Due:
Balance	Mettler	AE100	K04827	Lab	Ben Myren	10/20/1998	10/1999

STANDARDS USED FOR THIS CALIBRATION:

Item:	Make:	Model:	Serial Number:	NIST ID:	Cal. Date:	Cal. Due:
Weight Set	Rice Lake	IMG-20KG	A45	822/251337	07/07/1998	07/1999

Technician: D.Deleasa

Signature

D. Deleasa

WOODSTOVE DATA SHEET #33

Thermocouple Calibration Record

TC #	Location	Ice Water Bath (°F)	Boiling Water (°F)	TC #	Location	Ice Water Bath (°F)	Boiling Water (°F)
1	Wet Bulb	32.4	209.8	21			
2	Dry Bulb	32.3	209.8	22			
3	Stack	32.5	209.8	23			
4	Stove Top	32.4	209.7	24			
5	Left Side	32.3	209.9	25			
6	Back	32.4	209.8	26			
7	Right Side	32.4	209.7	27			
8	Bottom	32.5	209.7	28			
9	Firebox	32.6	209.9	29	Oven		
2nd Burn				30	N/A-Calibrator		
10	Catalytic	32.6	209.8	31			
11	Room	32.3	209.9	32			
12	Tube Furnace TNT TEND	32.5	209.7	33			
13	Sample Box C Gas Flap	32.6	209.7	34			
14	Impinger Out C Gas	32.6	209.8	35	Rear Top		
15	Gas Box Filter #1	32.5	209.7	36	Rear L Side		
16	Gas Out Filter #1 and	32.5	209.8	37	Rear R Side		
17	SO₂ Gas Out			38	Rear Firebox		
18	Extra			39	Rear 2nd/cat		
19	Extra			40			
20	Extra						

Thermocouples checked against

Reference Thermometer #: ERTCO CAT 1005-3FC CAT 517 SN 1697

Ice Water Bath 32.3 °F

Boiling Water 210.1 °F

Room Temp 68 °F

B.P. 29.61" Hg "Hg

Date: 2/2/98 Technician: A.T. Myron

ALTEK

CERTIFICATE OF CALIBRATION

This is to Certify that your Altek Unit has been calibrated using standards whose accuracies are traceable to the National Institute of Standards and Technology (formerly NBS) within the limits of the NIST Calibration Services. Actual records pertaining to these standards are on file and are available for examination.

Certified by: Altek Industries Corp.
Recommend Recalibration: Annually

In service date 4/11/96

Model K2100F Serial No. Serial # 177533

T. Kuech

Calibration Technician

31 AUG 95

Factory Calibration Date

ALTEK INDUSTRIES CORP
210 Commerce Drive, Rochester, NY 14623 U.S.A.
(716) 334-3720 FAX: (716) 334-6673
800-32-ALTEK
800-322-5835
Anywhere in USA

METER BOX 511 M, SN 900167

Date: 2/2/99

Thermocouple No.: JENCO Model 768-KF-02

Ambient Temperature: 68 °F

Barometric Pressure: 28.61 "Hg

Calibrator: A.T. Myer

Reference: Mercury-in-glass: ETCO SN 1697

Other: Altec

Ambient ETCO

Reference point No. ^a	Source ^b (specify)	Reference thermometer temperature, °F	Thermocouple potentiometer temperature, °F	Difference, % ^c
1	Altec	0	0	0
2		100	99	-0.17
3		200	201	+0.15
4		300	299	-0.13
5		400	397	-0.35
6		500	496	-0.42
7		600	597	-0.28
8		700	697	-0.25
9		800	801	+0.08
10		900	902	+0.15
11		1000	1007	+0.48
12		1100	1109	+0.58
13		1200	1212	+0.72
14		1400	1421	+1.13
15		1600	1615	+0.73
16		1800	1810	+0.44
17	✓	2000	1998	-0.08

^aEvery 30°C (50°F) for each reference point

^bType of Calibration system used

^c
$$\frac{(\text{Ref. temp. } ^\circ\text{C} + 273) - (\text{Test therm. temp. } ^\circ\text{C} + 273)}{\text{Ref. Temp. } ^\circ\text{C} + 273} \times 100 \leq 1.5\%$$

RANGE 0-1999°F

Date: 2/2/99
 Ambient Temperature: 68 °F
 Calibrator: A.T. Myron

Thermocouple No.: Extech Model 4020 KF
 Barometric Pressure: 28.61 "Hg
 Reference: Mercury-in-glass: ERTCO SN 1697
 Other: Altec

Amb ERTCO

Reference point No. ^a	Source ^b (specify)	Reference thermometer temperature, °F	Thermocouple potentiometer temperature, °F	Difference, ^c %	
1	Altec	0	1	+0.22	
2		100	99	-0.18	
3		200	201	+0.15	
4		300	299	-0.13	
5		400	400	0	
6		500	499	-0.10	
7		600	600	0	
8		700	698	-0.17	
9		800	800	0	
10		900	899	-0.07	
11		1000	1002	0.14	
12		1100	1101	+0.06	
13		1200	1201	+0.06	
14		1400	1401	+0.05	
15		1600	1600	0	
16		1800	1799	-0.04	
17		↓	1900	1900	0

^a Every 30°C (50°F) for each reference point
^b Type of Calibration system used
^c $\frac{(\text{Ref. temp: } ^\circ\text{C} + 273) - (\text{Test therm. temp. } ^\circ\text{C} + 273)}{\text{Ref. Temp. } ^\circ\text{C} + 273} \times 100 \leq 1.5\%$

Thermometer Calibration

2/2/99 A.T.M.G.

Mfr	ERTCO	ERTCO	VWR	Fisher	Taylor	Taylor	Premium	Weston
Cat #	1005-3FC	517	1016-0150B	ASTM-59F	1330NA	1330NA		
SN	1697	K85-163	---	A04544	WB	DB	AI	
Range	-1 to 101°C	0-260°C	-30 to 50°C	0-180°F	20-120°F	20-120°F	0-220°F	-40-160°F
Graduation	0.1°C	1.0°C	1.0°C	1.0°F	1.0°F	1.0°F	1°F	2°F
Type	Tube	Tube	Tube	Tube	Tube	Tube	Dial	Dial
Temp Pt 1	20.5	21.0	21.0	71	71	70.5	71	70
2	25.0	25.5	25.0	80	80	80.5	80	80
3	12.0	12.0	12.25	51	52	52	52	52
4	1.0	1.0	1.0	33	33	33	34	34
5	98.5	99	---	---	---	---	209	---

$$^{\circ}\text{F} = (^{\circ}\text{C} \times \frac{9}{5}) + 32$$

$$^{\circ}\text{C} = (^{\circ}\text{F} - 32) \frac{5}{9}$$

NOTE: Taylor 1330NA WB & DB = thermometers in the sling psychrometer

R E P O R T O F C A L I B R A T I O N

LIQUID-IN-GLASS-THERMOMETER

CALIBRATED BY EVER READY THERMOMETER CO.

MARKED: ERTCO CAT 1005-3FC S/N-1697
RANGE: -1 TO +101 DEGREES C IN 0.1 DEGREE GRADUATIONS.

THERMOMETER READING	CORRECTION (ITS-90)**
0.00 C	0.00 C
10.00	0.00
20.00	0.00
30.00	0.00
37.00	0.00
40.00	0.00
50.00	0.00
56.00	0.00
60.00	0.02
70.00	0.00
80.00	0.00
90.00	0.00
100.00	0.00

** ALL TEMPERATURES IN THIS REPORT ARE BASED ON THE INTERNATIONAL TEMPERATURE SCALE OF 1990 (ITS-90) PUBLISHED IN THE METROLOGIA 27, NO. 1, 3/10/90.

THIS THERMOMETER WAS CALIBRATED AGAINST A STANDARD CALIBRATED AT THE NATIONAL INSTITUTE OF STANDARDS AND TECHNOLOGY (NIST) FORMERLY THE NATIONAL BUREAU OF STANDARDS (NBS) IN ACCORDANCE WITH ASTM METHOD E 77, AND NBS MONOGRAPH 174.

FOR A DISCUSSION OF ACCURACIES ATTAINABLE WITH SUCH THERMOMETERS SEE NBS MONOGRAPH 250-23.

IF NO SIGN IS GIVEN ON THE CORRECTION, THE TRUE TEMPERATURE IS HIGHER THAN THE INDICATED TEMPERATURE; IF THE SIGN GIVEN IS NEGATIVE, THE TRUE TEMPERATURE IS LOWER THAN THE INDICATED TEMPERATURE. TO USE THE CORRECTIONS PROPERLY, REFERENCE SHOULD BE MADE TO THE NOTES GIVEN BELOW.

CONTINUED

TEST NUMBER: 152439
DATE: 07/16/96
STANDARD SERIAL NO. 128239
NIST IDENTIFICATION NO. 88024

R E P O R T O F C A L I B R A T I O N
LIQUID-IN-GLASS-THERMOMETER

THE THERMOMETER WAS TESTED IN A LARGE, CLOSED-TOP, ELECTRICALLY HEATED, LIQUID BATH, BEING "IMMERSED" 76MM. THE TEMPERATURE OF THE ROOM WAS ABOUT 25 DEGREES C (77 DEGREES F). IF THE THERMOMETER IS USED UNDER CONDITIONS WHICH WOULD CAUSE THE AVERAGE TEMPERATURE OF THE EMERGENT LIQUID COLUMN TO DIFFER MARKEDLY FROM THAT PREVAILING IN THE TEST, APPRECIABLE DIFFERENCES IN THE INDICATIONS OF THE THERMOMETER WOULD RESULT.

THE TABULATED CORRECTIONS APPLY PROVIDED THE ICE-POINT READING, TAKEN AFTER EXPOSURE FOR NOT LESS THAN 3 DAYS TO A TEMPERATURE OF ABOUT 20 DEGREES C (70 DEGREES F) IS 0.00 DEGREES C. IF THE ICE-POINT READING IS FOUND TO BE HIGHER (OR LOWER) THAN STATED, ALL OTHER READINGS WILL BE HIGHER (OR LOWER) TO THE SAME EXTENT. IF THE THERMOMETER IS USED AT A GIVEN TEMPERATURE SHORTLY AFTER BEING HEATED TO A HIGHER TEMPERATURE. AN ERROR OF 0.01 DEGREES OR LESS, FOR EACH 10 DEGREE DIFFERENCE BETWEEN THE TWO TEMPERATURES, MAY BE INTRODUCED. THE TABULATED CORRECTIONS APPLY IF THE THERMOMETER IS USED IN THE UPRIGHT POSITION; IF USED IN A HORIZONTAL POSITION, THE INDICATIONS MAY BE A FEW HUNDREDTHS OF A DEGREE HIGHER.

TEST NUMBER: 152439
DATE: 07/16/96
STANDARD SERIAL NO. 128239
NIST IDENTIFICATION NO. 88024



Charles Tang-Nian
QUALITY CONTROL MANAGER

X INSTRUMENTS
PA METHOD 5
Pre-Test Calibration

English Meter Box and English Calibration Meter Units

Filename: C:\My Documents\511cal1399.wk1

Model Number: AEEK 511-N Date: → March 13, 99
 Serial Number: ~~20344~~ 20344 Barometric Pressure: → 29.64 (in. Hg)
 Calibration Meter Factor Yc: → 1.0149 (number)

dH (in H2O)	Elapsed Time (min)	DRY GAS METER READING			GAS			CALIBRATION METER READINGS			CALIBRATION METER	
		Volume Initial (cu ft)	Volume Final (cu ft)	Volume Total (cu ft)	Temperature Inlet (deg F)	Temperature Outlet (deg F)	Volume Initial (cu ft)	Volume Final (cu ft)	Volume Total (cu ft)	Temperature Inlet (deg F)	Temperature Outlet (deg F)	
0.50	15.78	747.400	753.900	6.500	Initial→ Final→→	67.0 72.0	500.345	506.507	6.462	69.0	63.0	
0.75	10.85	754.300	759.800	5.500	Initial→ Final→→	71.0 71.0	507.202	512.643	5.443	68.0	63.0	
1.00	8.92	760.300	765.504	5.204	Initial→ Final→→	72.0 73.0	513.125	519.272	5.147	68.0	68.0	
1.25	7.37	765.978	771.405	5.427	Initial→ Final→→	73.0 73.0	516.743	524.068	5.322	68.0	67.0	
1.50	6.93	772.600	777.903	5.303	Initial→ Final→→	73.0 72.0	525.250	530.463	5.213	67.0	67.0	

DRY GAS METER
METER CALIBRATION FACTOR

Value (number)	Variation (number)
1.006	0.002
1.005	0.002
1.006	0.003
0.999	-0.005
1.001	-0.002
Average 1.003	

DRY GAS METER
ORIFICE CALIBRATION FACTOR

Value (in H2O)	Variation (in H2O)
1.704	0.076
1.693	0.065
1.701	0.074
1.545	-0.082
1.494	-0.133
Average 1.627	

Note: For Calibration Factor Y, the ratio of the reading of the calibration meter to the dry gas meter, acceptable tolerance of individual values from the average is +0.02.

For Orifice Calibration Factor dh0, the orifice differential pressure in inches of H2O that equates to 0.75 cfm of air at 68 F and 29.92 inches of Hg, acceptable tolerance of individual values from the average is +0.2.

I certify that the above Dry Gas Meter was calibrated in accordance with E.P.A. Method 5, paragraph 7.1; CFR 40 Part 60, using the Precision Wet Test Meter # 11A56, which in turn was calibrated using the American Ball Prover # 3785, certificate # F107, which is traceable to the National Bureau of Standards (N.I.S.T.).

Signature A.T. Myron

Date 3/13/99

METER BOX CALIBRATION AUDIT

		Test Data									
Run #		1	2	3	4	5	6	7	8	9	10
Avg. ΔH		.900	.900	.900	.900	.900	.898				
Max Vac		0	0	0	0	0	0				

Avg. Test Series ΔH : 0.89967 in H₂O. Test Series Max Vac: 0 ✓ in Hg

Audit Dry Gas Meter: 300392 Correction (Y) Factor: 1.0149
 Test Dry Gas Meter: 511-M Correction (Y) Factor: 1.003

Audit Data

		Audit #1	Audit #2	Audit #3
BP:		<u>28.48" Hg</u>	<u>23.47" Hg</u>	<u>28.47" Hg</u>
Vac:		<u>0</u>	<u>0</u>	<u>0</u>
Audit Meter:	Final Vol	<u>553.122</u>	<u>558.572</u>	<u>564.475</u>
	Initial Vol	<u>547.855</u>	<u>553.329</u>	<u>558.963</u>
	Vol (V _w , ft ³)	<u>5.267</u> ✓	<u>5.243</u> ✓	<u>5.512</u> ✓
Audit Meter:	Initial	<u>67</u>	<u>66</u>	<u>66</u>
Temp (°F)(T _w)	Mid	<u>66</u>	<u>66</u>	<u>66</u>
	Final	<u>65</u> ✓	<u>66</u> ✓	<u>66</u> ✓
	Avg (°F/°A)	<u>(66) 526</u>	<u>(66) 526</u>	<u>(66) 526</u> ✓
ΔH (in H ₂ O)	Initial	<u>.90</u>	<u>.90</u>	<u>.90</u>
	Mid	<u>.90</u>	<u>.90</u>	<u>.90</u>
	Final	<u>.90</u>	<u>.90</u>	<u>.90</u>
	Avg	<u>.90</u> ✓	<u>.90</u> ✓	<u>.90</u> ✓
Dry Gas Meter:	Final Vol	<u>750.600</u>	<u>756.004</u>	<u>761.955</u>
	Initial Vol	<u>745.400</u>	<u>750.700</u>	<u>756.400</u>
	Vol (V _d , ft ³)	<u>5.200</u> ✓	<u>5.304</u> ✓	<u>5.555</u> ✓
Dry Gas Meter	Initial	<u>63</u>	<u>67</u>	<u>68</u>
Temp (°F):Inlet	Mid	<u>64</u>	<u>69</u>	<u>67</u>
	Final	<u>66</u> ✓	<u>70</u> ✓	<u>69</u> ✓
	Avg (°F/°A)	<u>(64.3) 524.3</u>	<u>(68.7) 528.7</u>	<u>(68) 528</u> ✓
Dry Gas Meter	Initial	<u>63</u>	<u>65</u>	<u>68</u>
Temp (°F):Outlet	Mid	<u>64</u>	<u>65</u>	<u>68</u>
	Final	<u>64</u> ✓	<u>65</u> ✓	<u>68</u> ✓
	Avg (°F/°A)	<u>(63.7) 523.7</u>	<u>(65) 525</u>	<u>(68) 528</u> ✓
Avg Dry Gas		<u>(64) 524</u> ✓	<u>526.85</u> ✓	<u>(68) 528</u> ✓
Meter Temp (T _m -°F/°A)		<u>9:25:30</u>	<u>9:29:37</u>	<u>10:03:06</u>
Time (minutes)				

$$Y = \frac{(V_w)(MCF)(BP)(T_m)}{(V_d)(BP + \frac{\Delta H}{13.6})(T_w)}$$

$$Y \text{ Factor } \% \text{ Difference} = \frac{\text{Act} - \text{Exp}}{\text{Exp}} \times 100$$

NOTE: MCF = Meter Correction (Y) Factor for Dry Gas Meter used as a Transfer Standard

Run 1

$$Y = \frac{(5.267)(1.0149)(28.43)(524)}{(5.200)(28.43 + \frac{.90}{13.6})(526)} = \frac{79,773.352}{78,079.502} = 1.0217$$

$$\Delta\% = \frac{(1.0217 - 1.0056)}{1.0056} \times 100 = +1.601\%$$

Run 2

$$Y = \frac{(5.243)(1.0149)(28.47)(526.85)}{(5.304)(28.47 + \frac{.90}{13.6})(526)} = \frac{79,413.722}{79,613.173} = 1.0025$$

$$\Delta\% = \frac{(1.0025 - 1.0056)}{1.0056} \times 100 = -0.308\%$$

Run 3

$$Y = \frac{(5.512)(1.0149)(28.47)(528)}{(5.555)(28.47 + \frac{.90}{13.6})(526)} = \frac{84,091.839}{83,380.710} = 1.0085$$

$$\Delta\% = \frac{(1.0085 - 1.0056)}{1.0056} \times 100 = +0.288\%$$

$\bar{X} = +0.53\%$

NOTE: The Y Factor % Difference must be < +5.0% to be acceptable

Determination of Interpolated Y Factor for Average Certification Test Series Delta H from Dry Gas Meter Calibration Data:

$$\frac{0.75}{(A)} \text{ inch H}_2\text{O Delta H} = \frac{1.005}{(C)} \text{ Calculated Calibration Y Factor (from Calibrations)}$$

$$\frac{1.00}{(B)} \text{ inch H}_2\text{O Delta H} = \frac{1.006}{(D)} \text{ Calculated Calibration Y Factor (from Calibrations)}$$

$$\frac{1.00}{(B)} - \frac{.75}{(A)} = \frac{.25}{(A)} \times 100 = \frac{25}{(E)}$$

$$\frac{1.006}{(D)} - \frac{1.005}{(C)} = \frac{.001}{(C)} \div \frac{25}{(E)} = \frac{0.00004}{(F)}$$

$$\frac{.8997}{\text{Avg Delta H}} - \frac{.75}{(A)} = \frac{.1497}{(A)} \times 100 = \frac{14.97}{(G)}$$

$$\left[\frac{0.00004}{F} \times \frac{14.97}{G} \right] + \frac{1.005}{C} = \frac{1.0056}{\text{Interpolated Y Factor For Avg. Test Series Delta H}}$$

at -10" Hg 549/551

Volume Metering System Leak Check: .002 CF³ inch H₂O in one minute

REFERENCE METER CALIBRATION
 TWO POINT VERIFICATION CHECK
 ENGLISH REFERENCE METER UNITS
 DGM Serial # 300392
 Date 7/26/98

Barometric Pressure 29.71
 Meter Yw 1.00000
 K (deg R/inches Hg) 17.64

Filename: F:\DATAFILE\CALIBRAT\CAL_MENU.DSK\DGM_2VER\300392-
 Revised: 1/5/98

Time (min)	Pressure (in. H2O)	Dry Gas Meter (DGM)		Temperature		Meter Readings		Wet Test Meter (WTM)		Temp (deg F)	DGM Coefficient Yds	Flow Rate (CFM)	DGM Coefficient Yds	PREVIOUS DATA
		Initial	Final	Initial	Final	Initial	Final	Volume (cubic feet)	Volume (cubic feet)					
10.00	-5.000	417.848	427.852	10.004	80.0	578.155	588.070	9.915	80.0	80.0	1.004	0.962	1.009	0.4509415 %
20.00	-1.800	427.852	436.302	8.450	81.0	588.070	596.510	8.440	80.0	80.0	1.006	0.410	1.013	0.6838462 %

%CHANGE MUST BE +/- 1.5%, ELSE PERFORM 15PT CAL

I certify that the above Dry Gas Meter was calibrated in accordance with E.P.A. Method 5, paragraph 7.1; CFR 40 Part 60, using the Precision Wet Test Meter # 11AE6, which in turn was calibrated using the American Bell Prover # 3785, certificate # F107, which is traceable to the National Bureau of Standards (N.I.S.T.).

Signature *[Signature]* Date 7-26-98

REFERENCE METER CALIBRATION
ENGLISH REFERENCE METER UNITS

DGM Serial # 300392
Date 4/17/97
Filename: F:\DATAFILE\CALIBRAT\CAL_MENU.DSK\DGM_REF.
Revised: 06/08/95

Barometric Pressure 29.55
Meter Yw 1.00000
K (deg R/inches Hg) 17.64

Time (min)	Pressure (in. H2O)		Dry Gas Meter (DGM)		Temperature (deg F)		Wet Test Meter (WTM)		DGM Coefficient Yds	Coefficient Variation Yds-(Avg.Yds)	Flow Rate (CFM)
	Initial	Final	Volume (cubic feet)	Initial	Final	Initial	Final	Volume (cubic feet)			
43.50	-6.800	975.414	1027.032	51.618	74.0	75.0	570.631	621.609	70.0	1.013	1.153
5.00	-6.800	27.032	33.092	6.060	75.0	76.0	621.609	627.579	70.0	0.000	1.174
5.50	-6.800	33.092	39.759	6.667	76.0	76.0	627.579	634.140	70.0	0.000	1.173
Max Yds - Min Yds =0.000757781 Must be no greater than 0.030 Average Yds =1.012668100 Must be between 0.95 to 1.05											
21.00	-4.600	39.759	59.519	19.760	76.0	76.0	634.140	653.669	70.0	1.011	0.915
8.00	-4.600	59.519	67.033	7.514	76.0	76.0	653.669	661.070	70.0	1.008	0.910
6.50	-4.600	67.033	73.137	6.104	76.0	77.0	661.070	667.091	70.0	1.010	0.911
Max Yds - Min Yds =0.003425424 Must be no greater than 0.030 Average Yds =1.009592597 Must be between 0.95 to 1.05											
35.00	-3.000	73.137	99.630	26.493	77.0	76.0	667.091	693.309	70.0	1.009	0.737
11.50	-3.000	99.630	108.357	8.727	70.0	72.0	693.309	702.130	74.0	1.013	0.749
17.50	-3.000	108.357	121.465	13.108	72.0	72.0	702.130	715.389	74.0	1.015	0.740
Max Yds - Min Yds =0.006019406 Must be no greater than 0.030 Average Yds =1.012417828 Must be between 0.95 to 1.05											
11.50	-2.000	121.465	127.641	6.176	72.0	73.0	715.389	721.703	74.0	1.025	0.536
28.00	-2.000	127.641	142.554	14.913	73.0	75.0	721.703	736.961	74.0	1.028	0.532
10.00	-2.000	142.554	147.894	5.340	75.0	76.0	736.961	742.395	74.0	1.026	0.530
Max Yds - Min Yds =0.003679685 Must be no greater than 0.030 Average Yds =1.026129451 Must be between 0.95 to 1.05											
27.50	-1.400	147.894	159.237	11.343	76.0	77.0	742.395	753.825	74.0	1.016	0.406
22.50	-1.400	159.237	167.914	8.677	77.0	79.0	753.825	762.519	74.0	1.013	0.377
16.00	-1.400	167.914	174.098	6.184	79.0	80.0	762.519	768.690	74.0	1.012	0.376
Max Yds - Min Yds =0.004226433 Must be no greater than 0.030 Average Yds =1.013540053 Must be between 0.95 to 1.05											

Overall Average Yds =1.014869606

I certify that the above Dry Gas Meter was calibrated in accordance with E.P.A. Method 5, paragraph 7.1; CFR 40 Part 60, using the Precision Wet Test Meter # 11AE6, which in turn was calibrated using the American Bell Prover # 3785, certificate # F107, which is traceable to the National Bureau of Standards (N.I.S.T.).

Signature *[Signature]* Date 4-17-97

VANEOMETER CALIBRATION

Myren Consulting uses a Dwyer Model #480 Vaneometer to measure test chamber air velocity. The manufacturer's specifications for accuracy are $\pm 5.0\%$ to 100 FPM and $\pm 10\%$ from 100 FPM to top of scale. Myren Consulting insures that the instrument is level and clean prior to taking each reading. According to EPA personnel (Westlin, RTP) no further calibration of the instrument is necessary.

DRAFT GAUGE CALIBRATION

Myren Consulting uses a Dwyer Model 115-AV 0 - 0.25" inclined water manometer (readability resolution ± 0.001 " of water) to measure the static pressure in the stack. Once leveled and zeroed as per the manufacturer's written operating instructions, the Dwyer 0 - 0.25" manometer is a primary standard and needs no additional calibration.

The manometer is leveled and zeroed at the start of each test run, checked as necessary during the run to verify that the settings have not changed and again at the end of each test run. The results of each check are recorded on Woodstove Data Sheet #16 in each individual test run.

BAROMETER CALIBRATION

Myren Consulting uses a Weems and Plath aneroid barometer to measure barometric pressure (BP) in the Woodinville, WA lab. The barometer is calibrated daily by obtaining the barometric pressure (station pressure) from the National Weather Service (NWS) adjusting that pressure for altitude and then calibrating the lab barometer as necessary to that pressure.

MOISTURE METER CALIBRATION

The Delmhorst Model RC-1E, SN 1509 Moisture Meter is calibrated each time the meter is turned on using the two (2) calibration settings (Zero and Span). The potentiometers for each calibration point (X = Zero, Y = Span) are adjusted until the meter is correctly calibrated. Then the operation of the meter is checked in the normal operating range used during testing (11 - 25%) with a Delmhorst Model MCS-1 Moisture Content Standard at 12.5% and 22%.

Myren Consulting has a second moisture meter - Delmhorst Model RDX-1 SN 1359 - to use as a backup and as means of checking the readings on the Model RC-1E.

The readings obtained from the moisture meter are corrected as per the manufacturer's written instructions. See the following page for the correction table used to correct the readings.

10.0 - 10.6
 10.5 - 11.2
 11.0 - 11.7
 11.5 - 12.3
 12.0 - 12.8
 12.5 - 13.3
 13.0 - 13.9
 13.5 - 14.4
 14.0 - 14.9
 14.5 - 15.4
 15.0 - 15.9
 15.5 - 16.5
 16.0 - 17.0
 16.5 - 17.5
 17.0 - 18.1
 17.5 - 18.6
 LEGAL ↑ 18.0 - 19.2
 RANGE 18.5 - 19.8
 19.0 - 20.3
 19.5 - 20.9
 20.0 - 21.4
 20.5 - 22.0
 21.0 - 22.6
 21.5 - 23.1
 22.0 - 23.7
 22.5 - 24.3
 ↓ 23.0 - 24.9

24.0 - 26.0
 24.5 - 26.6
 25.0 - 27.2

26-ED ELECTRODE

OPERATING INSTRUCTIONS

The 26-E and 18-E Electrodes, fitted with insulated pins and used with any Delmhorst Moisture Detectors for Wood, are available in detecting moisture gradient in lumber or in testing dry stock that is wet on the surface.

These Electrodes, as long as they have good insulation on their shanks, measure moisture content at the tip of the pins only, that is in a layer about 3/16" thick.

Shell and core, moisture content is easily measured by driving the pins to the proper depths.

When using the Electrode, place the pins on the wood so that the current will flow parallel to the grain and drive the pins into the wood by means of the sliding hammer. Note the pins' penetration, and read the meter.

The Moisture Meter is calibrated for use with a 4-pin Electrode. When using a 2-pin Electrode, a small correction should be applied, as noted below, where line "A" shows meter readings, and line "B" the correct readings for the 2-pin Electrode.

A= 7	8	10	12	14	16	18	20	22
B= 7.3	8.4	10.6	12.8	14.9	17.0	19.2	21.4	23.7

When the insulation on the contact pins wears off, the above correction should be disregarded, and the electrode should not be used on lumber which may have a wet surface. Always use the L-319 insulating washer especially if surface moisture on the wood is expected. If washers are not available, do not allow the retainers to touch the surface of the wood.



WOODSTOVE DATA SHEET #26-A
 CEM GAS TRAIN RESPONSE TIME
 PRE CERTIFICATION TEST SERIES CHECK

Date	2/2/99	2/2/99	2/2/99	2/2/99	2/2/99	2/2/99	2/2/99	2/2/99
Technicians	ATM	ATM	ATM	ATM	ATM	ATM	ATM	ATM
Elapsed Time	CO2 Conc.(V)	CO2 Conc.(V)	CO2 Conc.(V)	CO Conc.(V)	CO Conc.(V)	CO Conc.(V)	O2 Conc.(V)	O2 Conc.(V)
0 Seconds	.334	.329	.76	.79	.83	.83	50.1	50.9
15	.333	.329	.76	.78	.82	.82	50.1	60.0
30	.049	.047	.06	.07	.08	.08	81.4	81.6
45	.023	.021	.05	.05	.07	.07	82.6	82.8
60	.012	.011	.03	.04	.05	.05	84.3	84.5
75	.008	.009	.03	.03	.03	.03	84.5	84.5
90	.006	.005	.02	.02	.03	.03	84.5	84.6
105	.004	.003	.02	.01	.02	.02	84.6	84.6
120	.002	.002	.01	.01	.01	.01	84.7	84.7
135	.002	.002	.01	.01	.01	.01	84.7	84.7
150	.001	.001	0	0	0	0	84.7	84.7
165	.001	.001	0	0	0	0	84.7	84.7
180	.001	.001	0	0	0	0	84.7	84.7
Initial Response Time (Seconds)	N15	N15	N15	N15	N15	N15	N17	N18
95% Response Time (Seconds)	>45<60	>45<60	>45<60	>45<60	>45<60	>45<60	760<75	760<75
Analyzer Flow Rate	1.5SCFH	1.5SCFH	1.5SCFH	1.5SCFH	1.5SCFH	1.5SCFH	1500 cc/min	→

Comments

InterMountain Ambient

P.O. Box 5106 □ Missoula, MT 59806 □ (406) 543-6174

Pre High Valley

QA WS 1/85

CO₂ ANALYZER MULTIPOINT CALIBRATION REPORT FORM

Site: Colville, WA Date: 3/20/99
 Analyzer: Make: HORIBA Model: PIR 2000 SN: 607204
 Calibration by: A.T. Myron
 Cal Gas Flow: 1.5 SCFH Measured by: Rotameter: Mass Flowmeter:
 BP: 28.59" Hg Instrument ID: WELMS
 Temp: 71 °F Instrument ID: EXTCH
 Analyzer last calibrated: 3/13/99 By: A.T. Myron

Cylinders:

1. # 36919 Concentration: 00.0 % CO₂ Cyl. Press.: 230 psi.
 Certified by: Cascade Angus Date: 4/24/96
2. # 250-1146 Concentration: 12.0 % CO₂ Cyl. Press.: 550 psi.
 Certified by: Oxarc Date: 8/22/97
3. # 250-1175 Concentration: 21.0 % CO₂ Cyl. Press.: 1390 psi.
 Certified by: Oxarc Date: 8/22/97
4. # 250-1060 Concentration: 6.0 % CO₂ Cyl. Press.: 1300 psi.
 Certified by: Oxarc Date: 8/22/97

Analyzer: Calibrated Range. 0-25.0 % Output: 0-1.0 v.
 Flow: 1.5 SCFH Measured by: Rotameter: Mass Flowmeter:

Calibration Results

Point #	Cyl. #	% CO ₂	Expected		Actual		Adj.		% Dif.	Potentiometer	
			Meter	DVM	Meter	DVM	Meter	DVM		Unadi.	Adj.
1	1	0.0	00.0	.000	00.0	.000	—	—	—	6.46	—
2	2	12.0	48.0	.480	48.0	.481	47.5	.480	—	2.53	2.52
3	3	21.0	84.0	.840	84.0	.844	—	—	+0.11	—	—
4	4	6.0	24.0	.240	24.0	.240	—	—	-0.12	—	—
5	1	0.0	00.0	.000	00.0	.000	—	—	0	—	—

Comments: 0.50 = 12.4623256

Linear Regression Results:

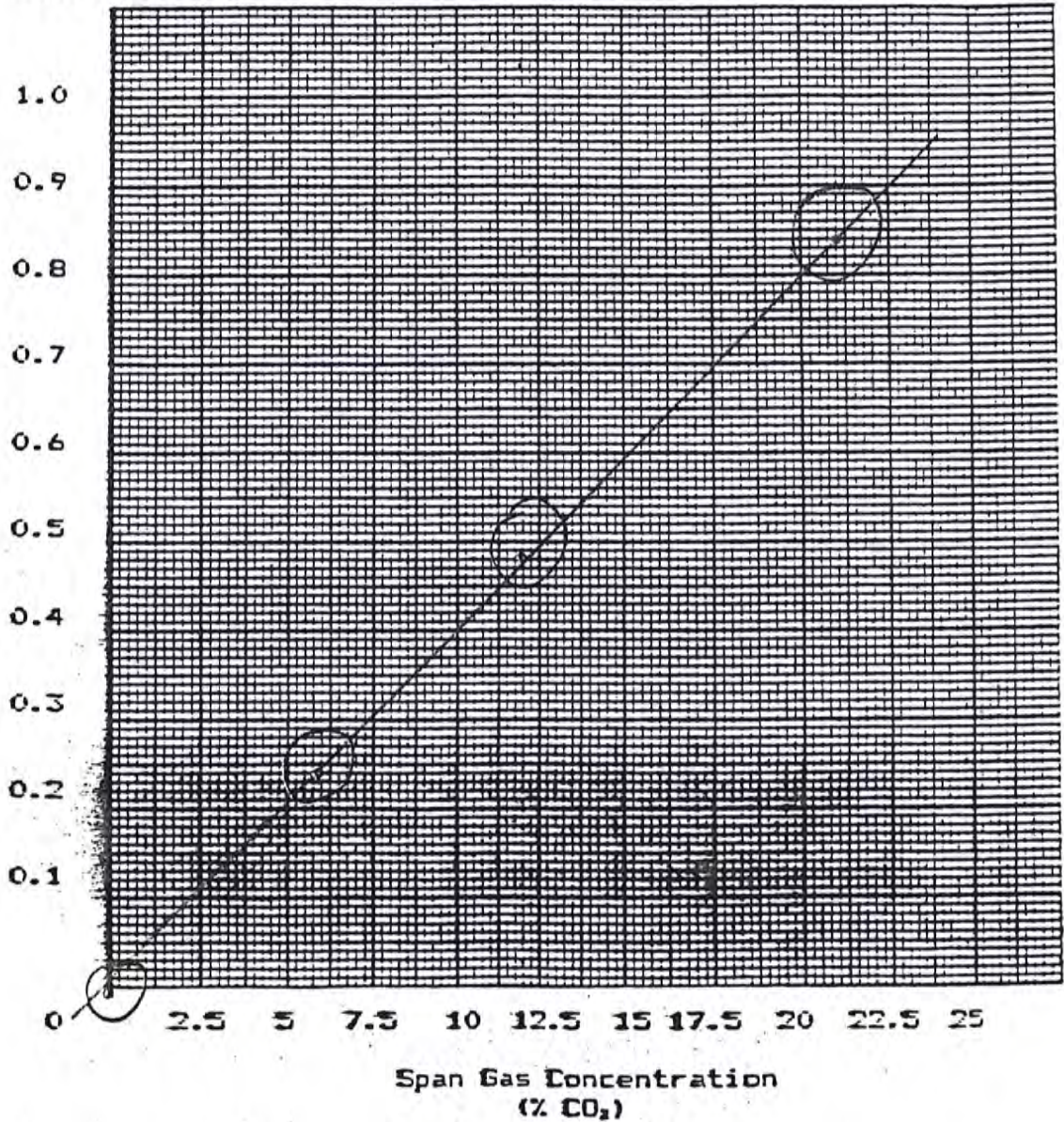
$Y = MX + B$

Slope (M) = $\frac{24.98349}{}$

Y Intercept (B) = $\frac{.0205549}{}$

Correlation Coefficient (r) = $\frac{0.9999954}{}$

Analyzer
Output
(volts)



Comments

InterMountain Ambient

P.O. Box 5108 □ Missoula, MT 59806 □ (406) 543-6174

Pre High Valley

QA WS 1/85

O₂ ANALYZER MULTIPOINT CALIBRATION REPORT FORM

Site: Colville WA Date: 3/20/99
 Analyzer: Make: Taylor Model: OA 137 SN: 137/4772
 Calibration by: A.T. Myner
 Cal Gas Flow: 1500 cc/min Measured by: Rotameter Mass Flowmeter:
 BP: 23.59" Hg Instrument ID: Weems
 Temp: 71.0 F Instrument ID: EXTCH
 Analyzer last calibrated: 3/13/99 By: A.T. Myner

Cylinders:

1. # 36919 Concentration: 00.0 % O₂ Cyl. Press.: 250 psi.
 Certified by: Cascade Airgas Date: 4/24/96
2. # 250-1146 Concentration: 12.0 % O₂ Cyl. Press.: 540 psi.
 Certified by: Oxarc Date: 8/22/97
3. # 250-1175 Concentration: 21.0 % O₂ Cyl. Press.: 1380 psi.
 Certified by: Oxarc Date: 8/22/97
4. # 250-1060 Concentration: 6.0 % O₂ Cyl. Press.: 1320 psi.
 Certified by: Oxarc Date: 8/22/97

Analyzer: Calibrated Range: 0-25.0 % Output: 0-100 m.v.
 Flow: 1500 cc/min Measured by: Rotameter Mass Flowmeter:

Calibration Results

Point #	Cyl. #	% O ₂	Expected		Actual		Adj.		% Dif.	Potentiometer	
			Meter	DVM	Meter	DVM	Meter	DVM		Unadj.	Adj.
1	1	0	00.0	00.0	00.0	00.0	—	—	—	—	—
2	2	12.0	12.0	48.0	12.05	48.1	12.05	48.0	—	—	✓
3	3	21.0	21.0	84.0	21.0	83.7	—	—	-0.08	—	—
4	4	6.0	6.0	24.0	6.0	24.0	—	—	+0.09	—	—
5	1	0	00.0	00.0	00.0	00.0	—	—	0	—	—

Comments: 50.0 = 12.5284877

Linear Regression Results:

$Y = MX + B$

Slope (M) = 1.25088

Y Intercept (B) = -0.01542

Correlation Coefficient (r) = 0.999997

Analyzer

Output

mV (volts)

$\times 10^2$

1.0

0.9

0.8

0.7

0.6

0.5

0.4

0.3

0.2

0.1

0

2.5

5

7.5

10

12.5

15

17.5

20

22.5

25

Span Gas Concentration
(% D_2)

Comments

Pre High Valley

QA WS 1/85

CO ANALYZER
MULTIPOINT CALIBRATION REPORT FORM

Site: Colville, WA Date: 3/20/99
Analyzer: Make: Infra Red Model: 702 D SN: 113
Calibration by: A.T. Myrum
Cal Gas Flow: 1.5 SCFH Measured by: Rotameter: X Mass Flowmeter:
RF: 28.59" Hg Instrument ID: Weems
Temp: 71°F Instrument ID: Exteca
Analyzer last calibrated: 3/13/99 By: A.T. Myrum

Cylinders:

1. # 36919 Concentration: 00.0 % CO Cyl. Press.: 230 psi.
Certified by: Cascade Airgas Date: 4/24/96
2. # 250-1146 Concentration: 2.51 % CO Cyl. Press.: 590 psi.
Certified by: Oxarc Date: 8/22/97
3. # 250-1175 Concentration: 4.03 % CO Cyl. Press.: 1390 psi.
Certified by: Oxarc Date: 8/22/97
4. # 250-1060 Concentration: 1.26 % CO Cyl. Press.: 1320 psi.
Certified by: Oxarc Date: 8/22/97

Analyzer: Calibrated Range: 0-5.0 % Output: 0 - 100 mv.
Flow: 1.5 SCFH Measured by: Rotameter: X Mass Flowmeter:

Calibration Results

Point #	Cyl. #	% CO	Expected		Actual		Adj.		% Dif.	Potentiometer	
			Meter	DVM	Meter	DVM	Meter	DVM		Unadi.	Adi.
1	1	0.00	0.00	00.0	0.00	00.0	-	-	0	-	-
2	2	2.51	2.51	50.2	2.50	50.0	2.51	50.2	-	-	✓
3	3	4.03	4.03	80.6	4.02	80.3	-	-	-0.12	-	-
4	4	1.26	1.26	25.2	1.29	25.4	-	-	+0.66	-	-
5	1	0.00	0.00	00.0	0.00	00.0	-	-	0	-	-

Comments:

50.0 = 2, 50 36 150

Linear Regression Results:

$Y = MX + B$

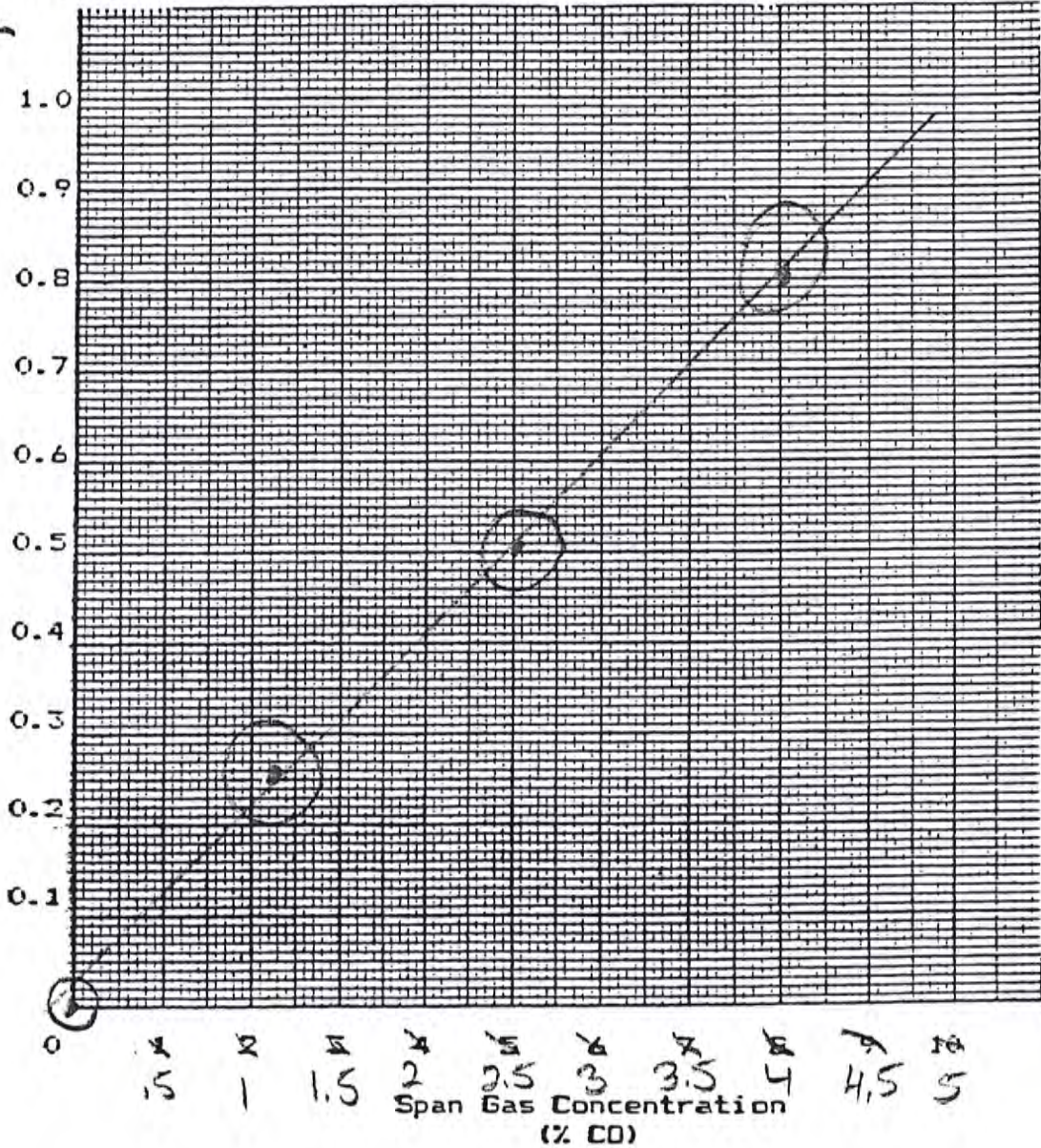
Slope (M) = $0,0502136$

Y Intercept (B) = $-0,0070762$

Correlation Coefficient (r) = $0,9999912$

Analyzer
Output
M (volts)

$\times 10^2$

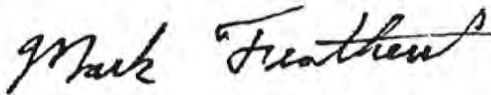


Comments

MALLINCKRODT**CERTIFICATE OF ANALYSIS**A Division of Mallinckrodt Baker, Inc.
222 Red School Lane • Phillipsburg, NJ 08865
Telephone: (908) 859-2151 • Fax: (908) 859-9318ITEM: ACETONE AR (ACS)
CODE: 2440
LOT : KTDC

TESTS	LIMITS	RESULTS
TITRATABLE ACID	0.0003 meq/g Max.	0.0002 meq/g
ALDEHYDE	0.002% Max.	0.002%
TITRATABLE BASE	0.0006 meq/g Max.	0.0004 meq/g
ISOPROPYL ALCOHOL	0.05% Max.	0.005%
METHANOL	0.05% Max.	0.005%
RESIDUE AFTER EVAPORATION	0.001% Max.	0.0002%
SOLUBILITY IN WATER	To Pass Test	Passes Test
SUBSTANCES REDUCING PERMANGANATE	To Pass Test	Passes Test
WATER	0.5% Max.	0.3%
COLOR	APHA 10 Max.	APHA 5
ASSAY	99.5% Min.	99.9%

It is hereby certified that the above is a true copy of the actual analysis of the lot indicated.



Mark Featherston
Manager, QA/QC
Mallinckrodt Baker, Inc
03/07/96 wwr

Acetone Purchased 7/10/96
1st blank done 8/8/96
2nd blank done 9/10/97
3rd blank done 9/10/97
4th blank done 3/13/97

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FAX (509) 662-1229

YAKIMA, WA 98903
1004 EAST MEAD
(509) 248-0827
FAX (509) 452-8704

Primary Standard Certificate of Analysis

Method of Analysis Micro GC / Gravimetric

Customer: Myren Consulting Reference # PM7234-3

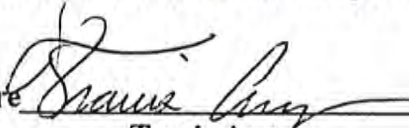
P.O.# Cylinder # 250-1146

Results of Investigation

<u>Component</u>	<u>Requested</u>	<u>Concentration</u>
Air -----	N/A -----	N/A -----
Argon -----	N/A -----	N/A -----
Carbon Dioxide -----	12.0% -----	12.0% -----
Carbon Monoxide -----	2.50% -----	2.51% -----
Helium -----	N/A -----	N/A -----
Hydrogen -----	N/A -----	N/A -----
Methane -----	N/A -----	N/A -----
Nitrogen -----	Balance -----	Balance -----
Oxygen -----	12.0% -----	12.0% -----

Hazard Class UN 1956
DOT Shipping Name Compressed Gas NOS
Shipping Volume (scf approximate) 160 scf @ ntp
Cylinder Pressure 1500 psig
CGA Valve Connection 350

Oxarc Primary Standard mixtures are prepared with gravimetric techniques using weights traceable to NIST. Mixture blended to +/- 1% relative to minor component and certified to +/- 1% analytical accuracy.

Authorized Signature  Date 8/25/97
Travis Auger

Comments:

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(509) 248-0827
FAX (509) 452-8704

Primary Standard Certificate of Analysis

Method of Analysis Micro GC / Gravimetric

Customer: Myren Consulting Reference # PM7234-2

P.O.# Cylinder # 250-1175

Results of Investigation

<u>Component</u>	<u>Requested</u>	<u>Concentration</u>
Air	N/A	N/A
Argon	N/A	N/A
Carbon Dioxide	21.0%	21.0%
Carbon Monoxide	4.00%	4.03%
Helium	N/A	N/A
Hydrogen	N/A	N/A
Methane	N/A	N/A
Nitrogen	Balance	Balance
Oxygen	21.0%	21.0%

Hazard Class UN 1956
DOT Shipping Name Compressed Gas NOS
Shipping Volume (scf approximate) 160 scf @ ntp
Cylinder Pressure 1500 psig
CGA Valve Connection 350

Oxarc Primary Standard mixtures are prepared with gravimetric techniques using weights traceable to NIST. Mixture blended to +/- 1% relative to minor component and certified to +/- 1% analytical accuracy.

Authorized Signature Travis Auger Date 8/25/97
Travis Auger

Comments:

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INDUSTRIAL GASES
MEDICAL GASES



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729 COMMERCIAL AVE.
(208) 734-9711
FAX (208) 734-7923

ATCHEE, WA 98801
ME GARDENS RD.
(509) 662-8417
FAX (509) 662-1229

YAKIMA, WA 98903
1004 EAST MEAD
(509) 248-0827
FAX (509) 452-8704

Primary Standard Certificate of Analysis

Method of Analysis Micro GC / Gravimetric

Customer: Myren Consulting Reference # PM7234-4

P.O.# Cylinder # 250-1060

Results of Investigation

<u>Component</u>	<u>Requested</u>	<u>Concentration</u>
Air	N/A	N/A
Argon	N/A	N/A
Carbon Dioxide	6.00%	6.00%
Carbon Monoxide	1.25%	1.26%
Helium	N/A	N/A
Hydrogen	N/A	N/A
Methane	N/A	N/A
Nitrogen	Balance	Balance
Oxygen	6.00%	6.00%

Hazard Class UN 1956
DOT Shipping Name Compressed Gas NOS
Shipping Volume (scf approximate) 160 scf @ ntp
Cylinder Pressure 1500 psig
CGA Valve Connection 350

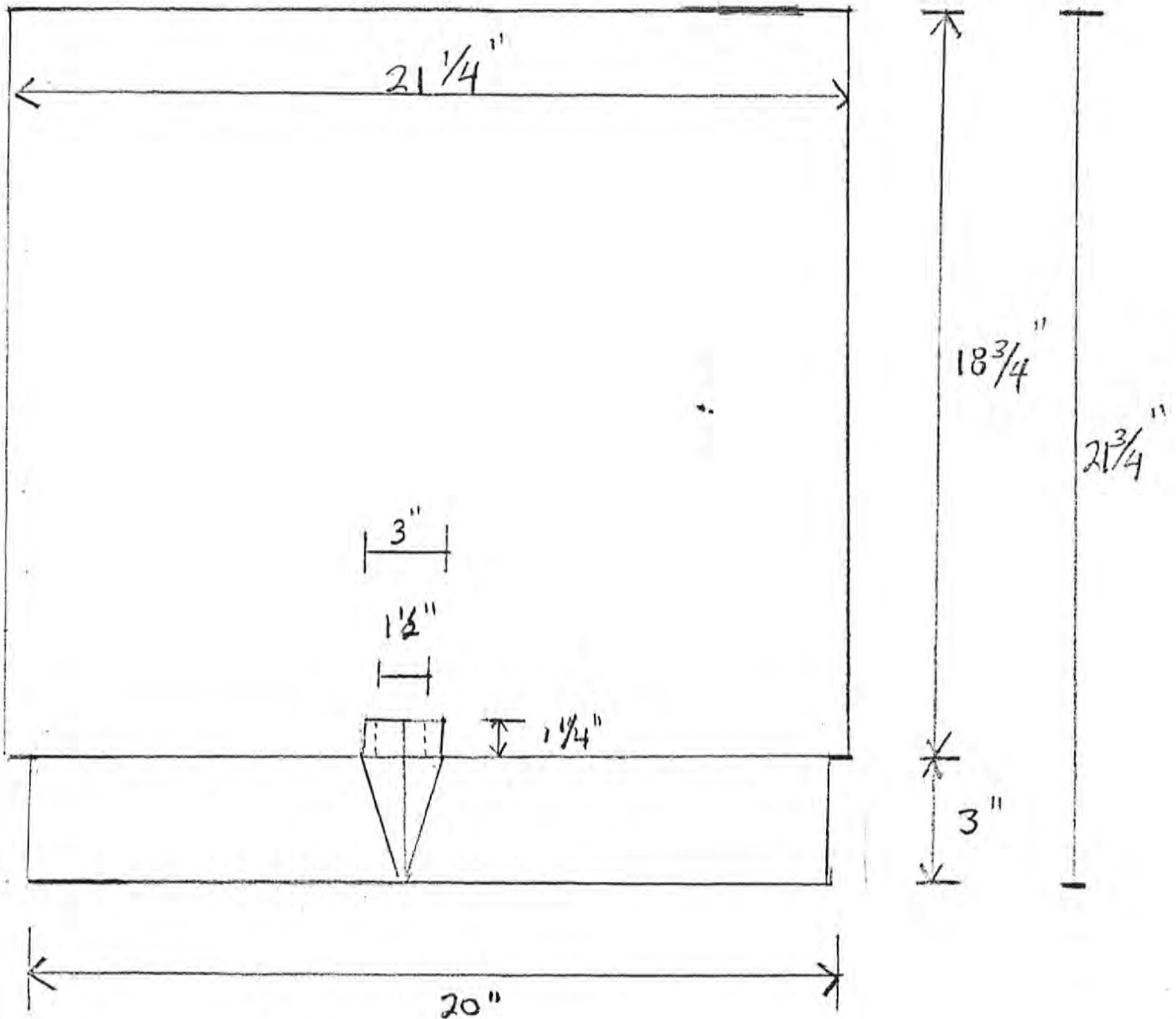
Oxarc Primary Standard mixtures are prepared with gravimetric techniques using weights traceable to NIST. Mixture blended to +/- 1% relative to minor component and certified to +/- 1% analytical accuracy.

Authorized Signature Travis Auger Date 8/25/97
Travis Auger

Comments:

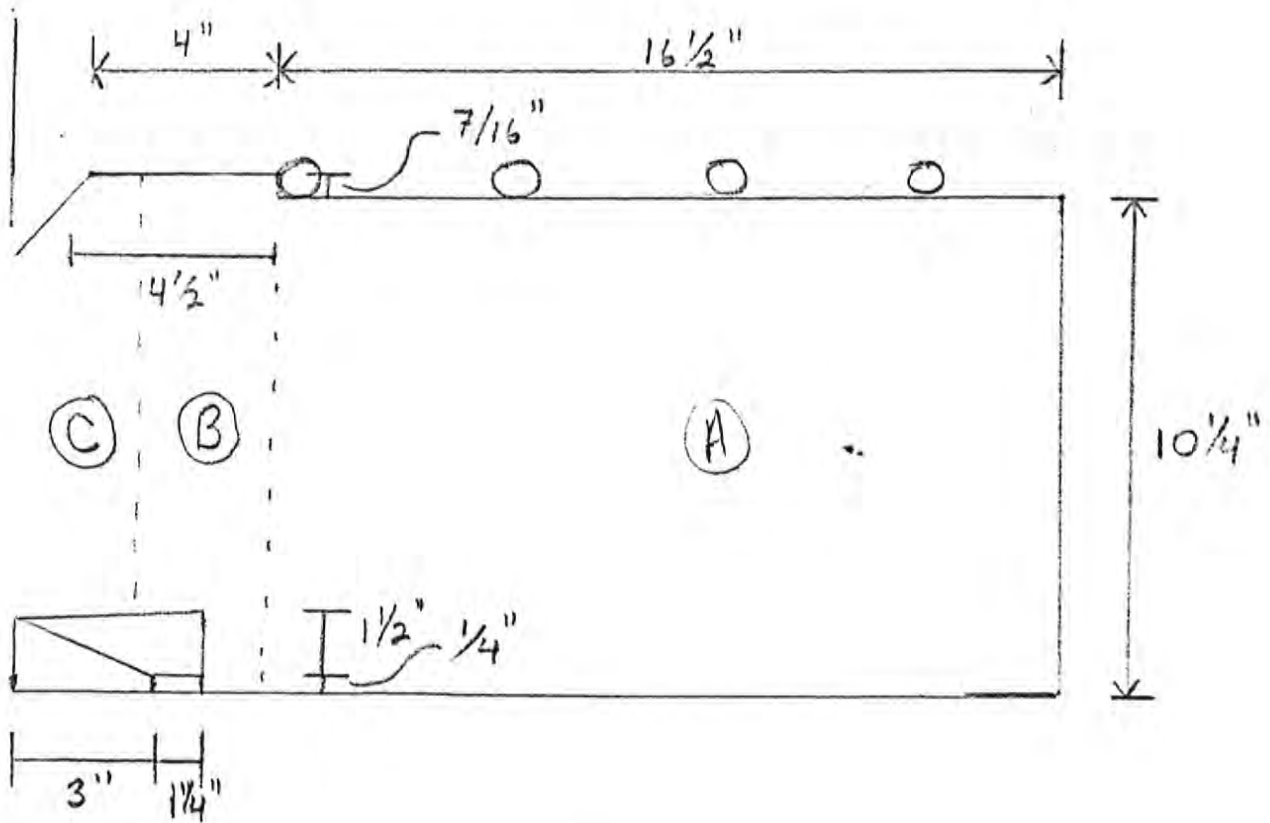
STOVE QC

The High Valley 1600 noncatalytic wood stove is a large sized (2.7 cubic foot) rectangularly shaped wood stove that is designed to normally be loaded in a north-south (front to back) manner. However, the unit will handle 20" cordwood loaded either way. The two most distinguishing features of the unit are (1.) its large size and (2.) its step top design. The secondary combustion system uses 4 stainless steel tubes to deliver the secondary air to the secondary combustion zone.



Top View

High Valley XTEC
 Page 1 of 4
 Not to Scale
 A.T. Myron



SIDE View

High Valley XTEC
 Page 2 of 4
 NOT to Scale
 A.T. Myren

USEABLE FIREBOX VOLUME Calculations:

$$A: 16.5 \times 21.25 \times 10.25 = 3593.906 \text{ in}^3$$

$$B: (18.75 - 16.5) \times 21.25 \times (10.25 + .4375) = 510.996$$

$$C: 3 \times 20 \times (10.25 + .4375) = \frac{641.250}{4746.152 \text{ in}^3}$$

Less:

$$D: \frac{.4375 \times .5}{2} \times 20 = 2.1875 \text{ in}^3$$

Airwash area

$$E: \frac{3 \times 1.25}{2} \times 20 = 37.500$$

$$F: 3 \times .25 \times 20 = 15.000$$

Bottom Primary Air Duct

$$G: \frac{3.25 \times 1.25}{2} \times \frac{3}{2} = 3.047$$

$$\frac{3 \times 1 \times 1.75}{2} = \frac{2.625}{60.360 \text{ in}^3}$$

LPAO

High Valley XTEC
Page 3 of 4
A. J. Myren

Firebox Volume AND Fuel load Size Calculations

$$4746.152 \text{ in}^3 - 60.360 \text{ in}^3 = 4685.792 \text{ in}^3$$

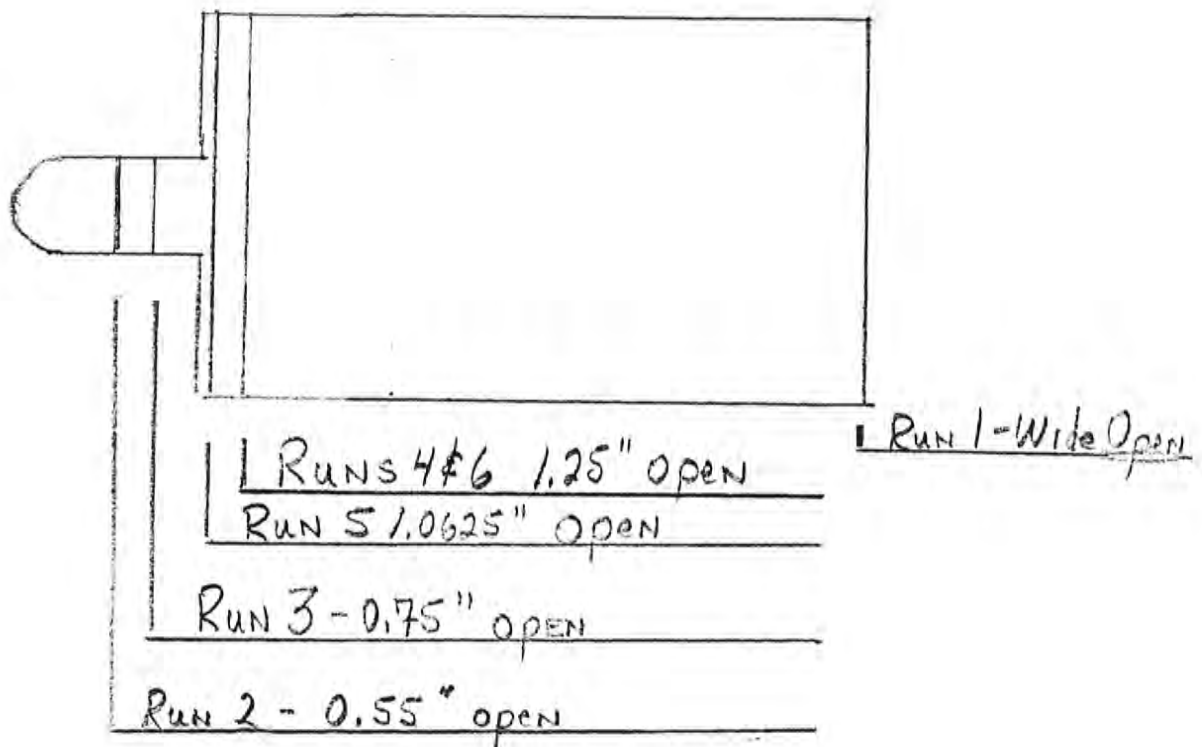
$$4685.792 \text{ in}^3 \div 1728 \text{ in}^3/\text{ft}^3 = 2.71169 \text{ ft}^3$$

$$2.71169 \text{ ft}^3 \times 7.0 \text{ lbs}/\text{ft}^3 = 18.982 \text{ lbs} - \text{ideal fuel load wt.}$$

$$18.982 \times (.1 \times 18.982) = 17.084 - 20.880$$

$$= 17.1 - 20.8 \text{ Fuel Load weight range}$$

High Valley 1600 Orifice Settings



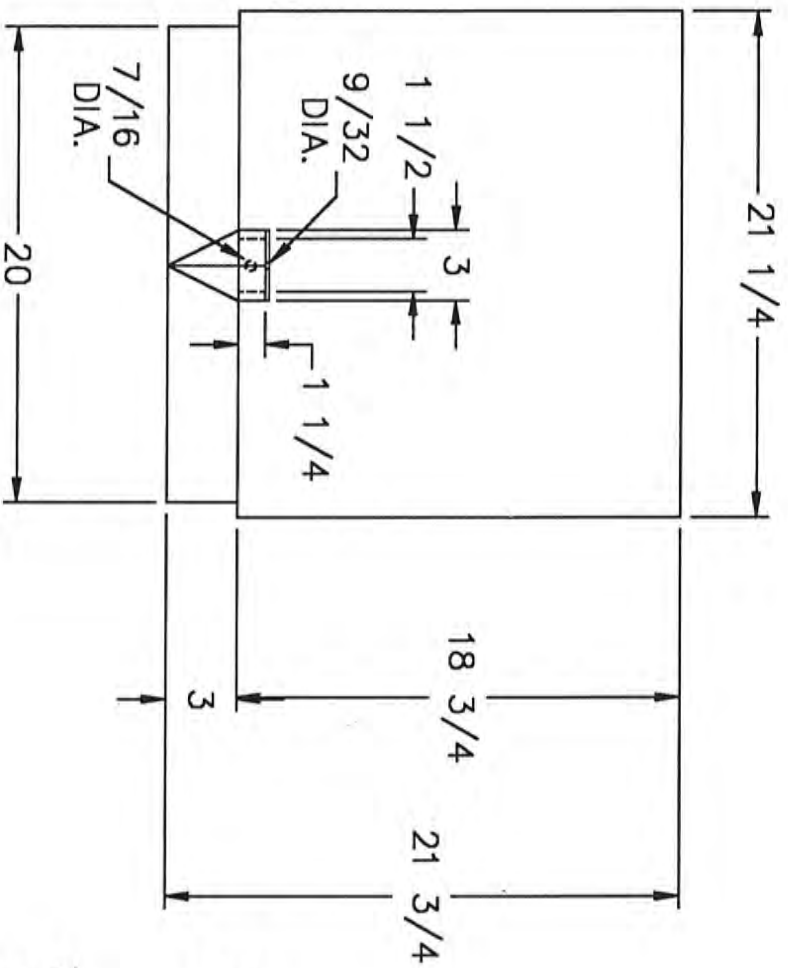
High Valley XTEC
P.

**High Valley Stoves
Index for Blueprints**

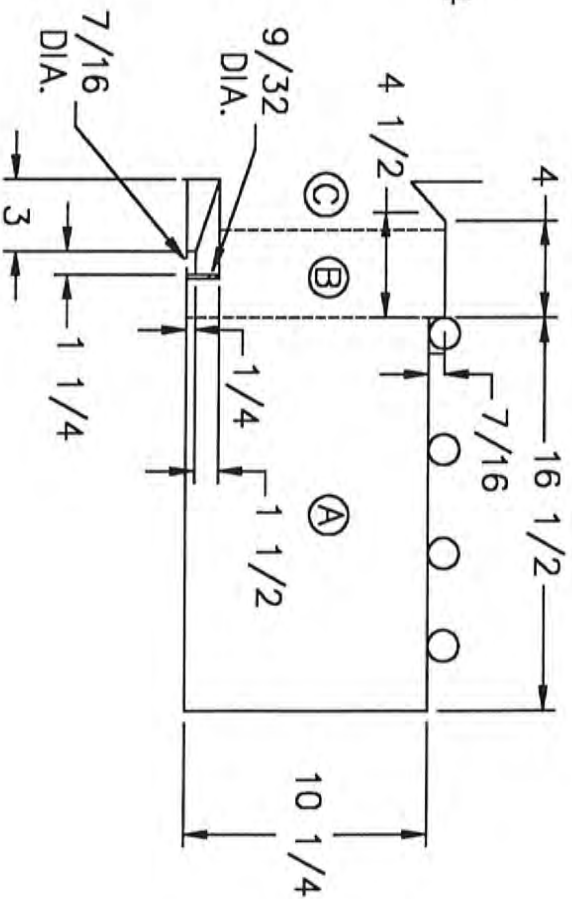
<u>Description</u>	<u>Page</u>
Air Flow	1
Convection Air	2
Firebox Volume	2A
Firebrick	3 and 4
Stainless Steel Air Tube	5
Firebrick Shelf in Top of Firebox	6
Air Wash Channels	7 and 8
Slide Draft Rod and Plate	9 and 10
Vertical Rear Air Tube	11
Air Wash Cap	12
Front	13
Air Tube Holder	14
Firebox	15
Outer Top	16
Air Wash Channels rear and side	17 and 18
Hearth and Bottom	19
Outer Bottom (Fresh Air Bottom)	20
Skin	21
Inner Rear Heat Shield	22
Door Handle	23
Door (front, back, cutaway)	24, 25, 26

FIREBOX VOLUME

TOP VIEW

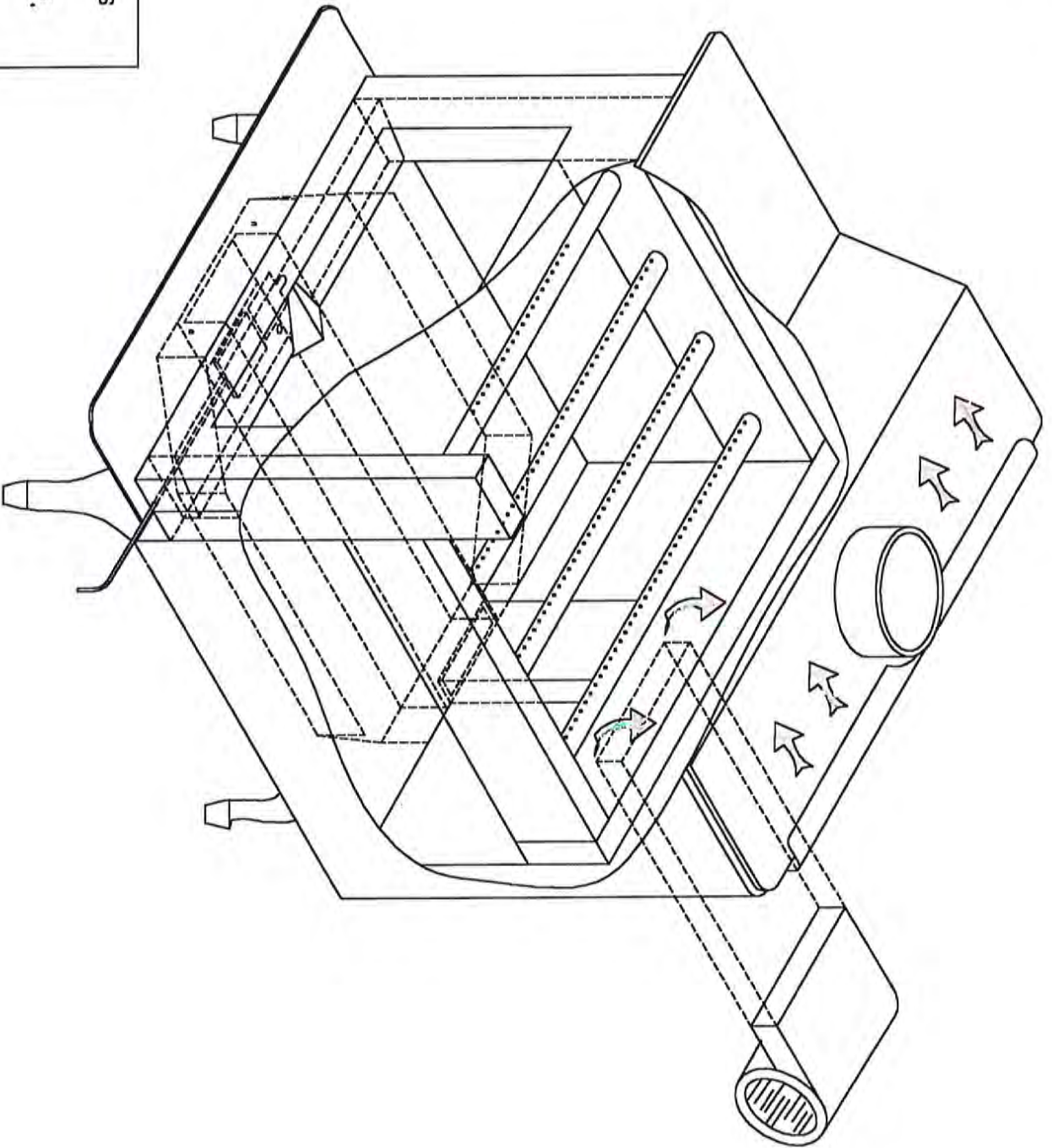


SIDE VIEW



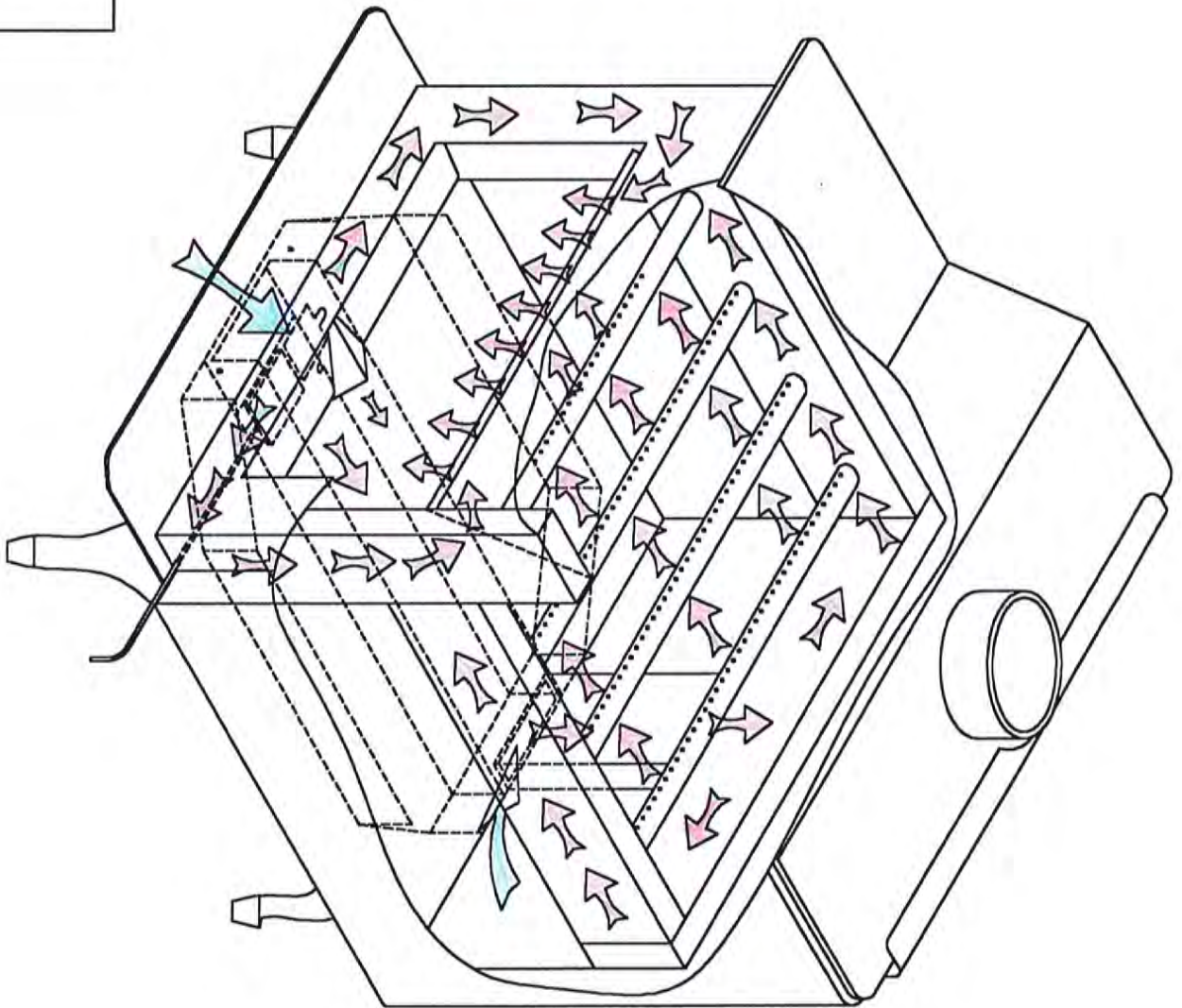
High Valley Stoves
Model 1600
Drawn by: Matt B.
Date: 4/15/99
2A of 26

Convection Air



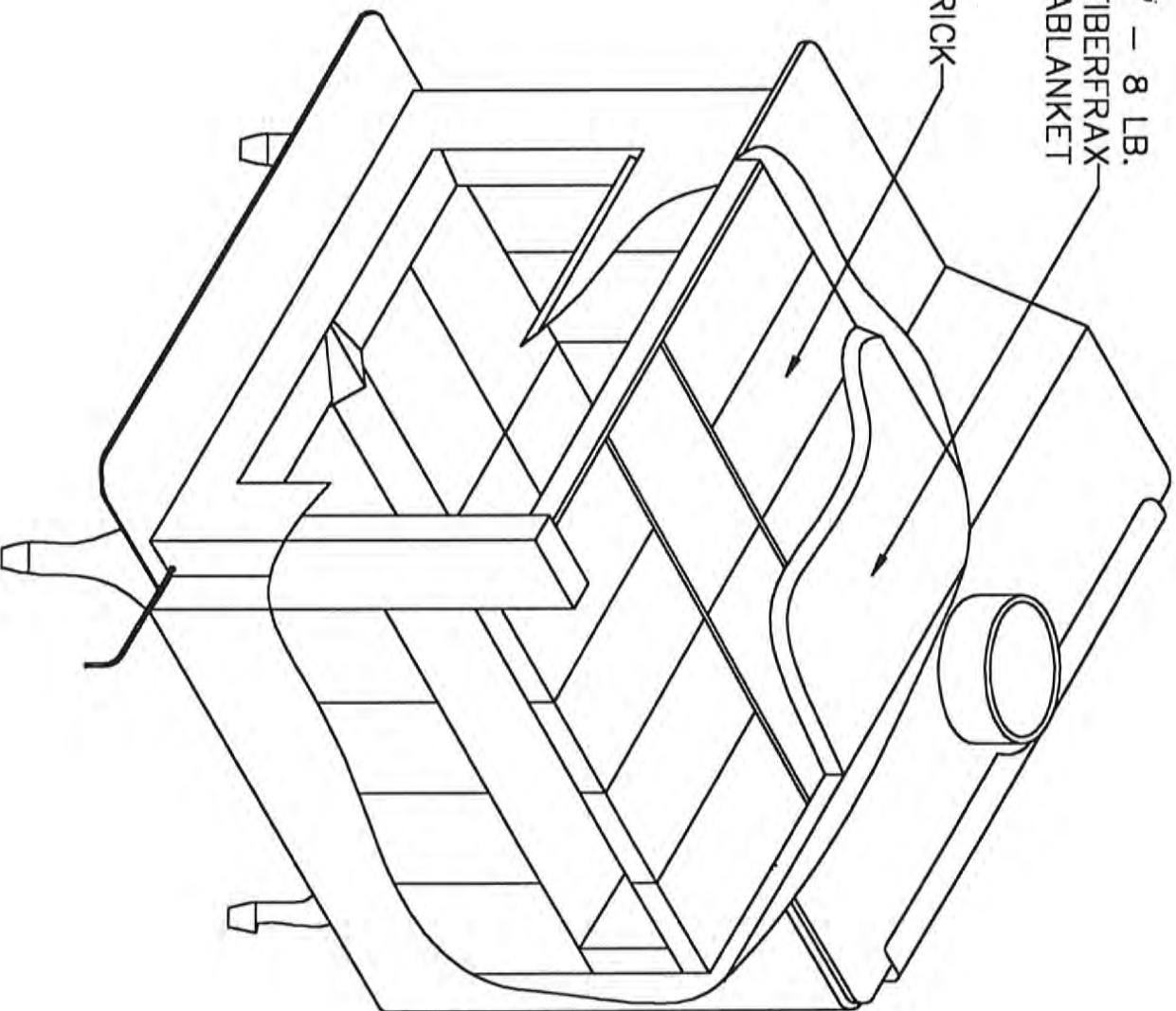
High Valley Stoves
Model 1600
Drawn by: Matt B.
Date: 4/15/99
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High Valley Stoves
Model 1600
Drawn by: Matt B.
Date: 4/15/99
1 of 26



1" - 8 LB.
FIBERFRAX
DURABLANKET

FIREBRICK



High Valley Stoves
Model 1600
Drawn by: Matt B.
Date: 4/15/99
3 of 26

Upper shelf of Model 1600

26	28	29
25		30
24	27	31
23		32

	5	6	vertical air tube	7	8	
4	14	15	18	19	21	9
3						10
2	13	16	17	20	22	11
1						12

High Valley Stoves

Firebrick Layout

Model 1600

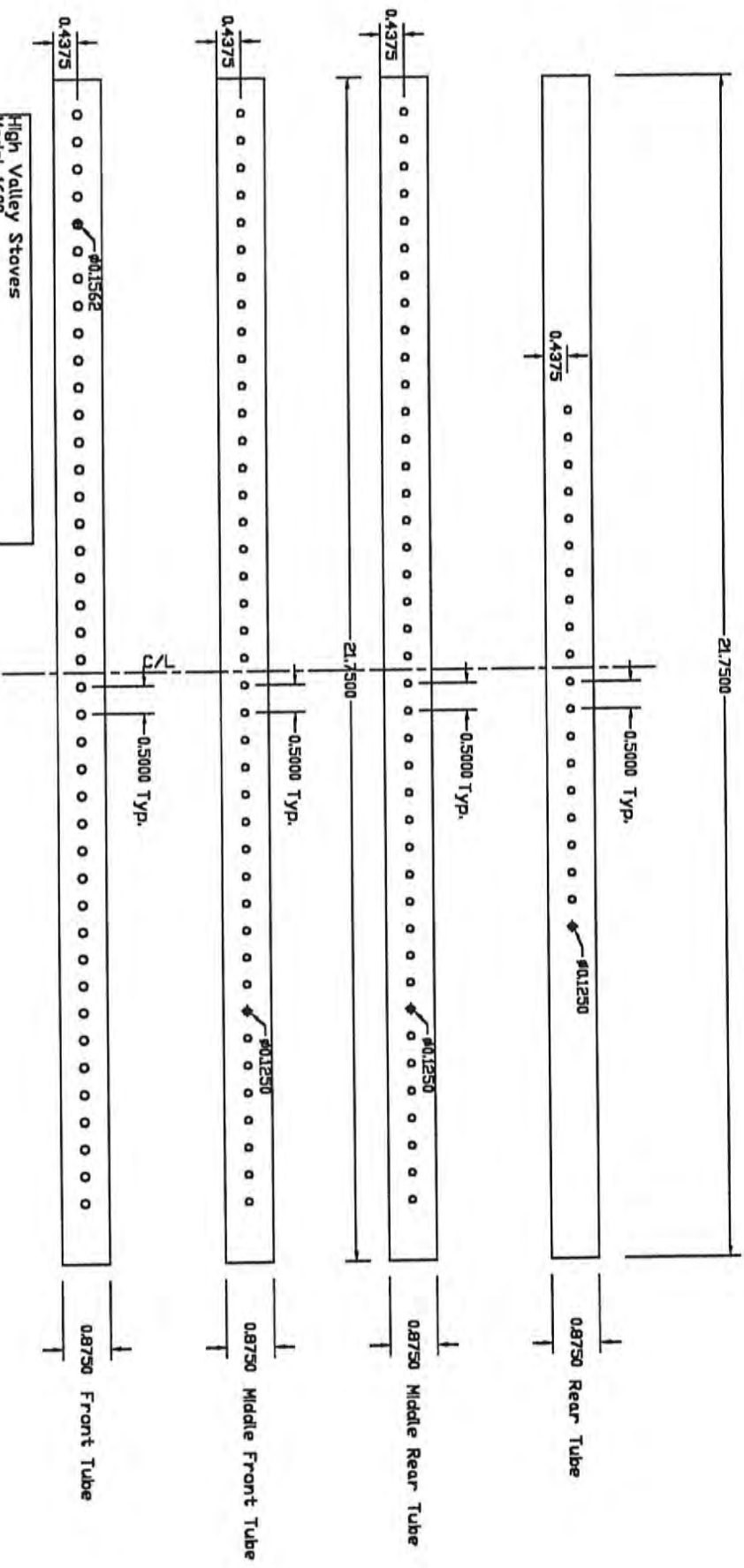
Brick 1-16 1" thick X 4 1/2" X 9"

Brick 17-18 1" thick X 2 1/4" X 9"

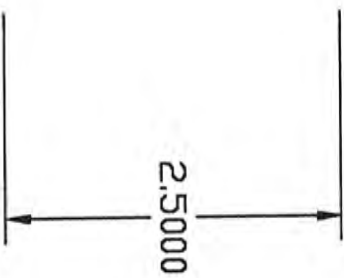
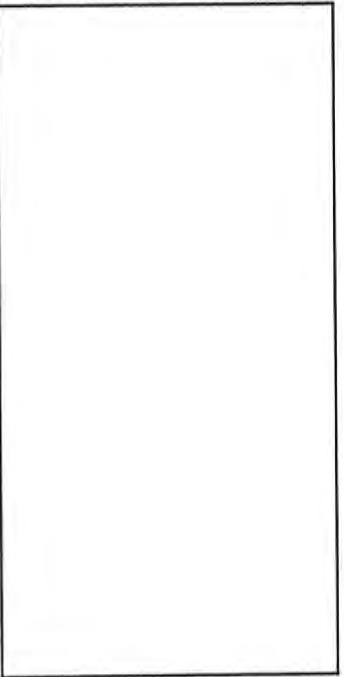
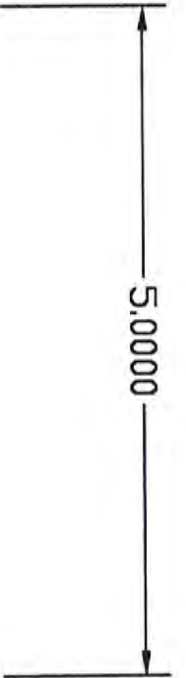
Brick 19-22 1" thick X 4 1/2" X 9"

Brick 23-32 1" thick X 4 1/2" X 9"

High Valley Stoves Model 1600 Firebrick Layout Drawn By: Matt B. Date: 4/15/99 Drawing 4 of 26

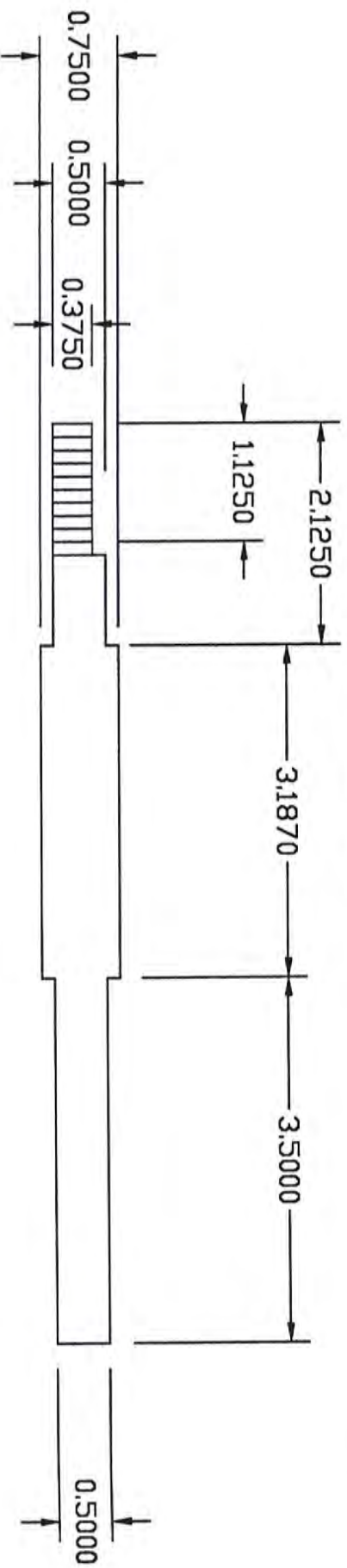


High Valley Stoves
 Model 1600
 Air Tubes
 Material Size: SS .875 OD X .750 ID X 21.750
 Drawn By: Matt B.
 Date: 4/7/99
 Drawing 5 of 26

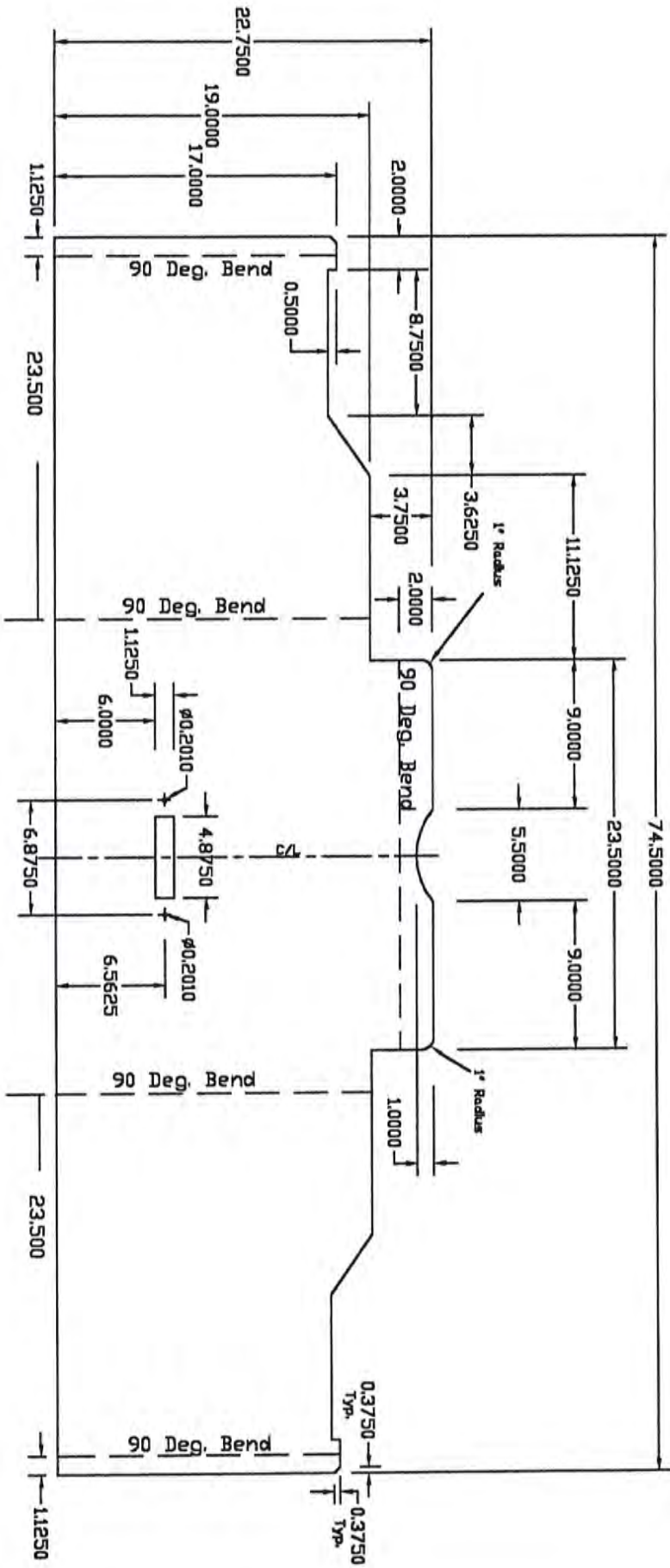


High Valley Stoves
Model 1600
Slide Draft Plate
Material Size: 3/8" X 5" X 2.5"
Drawn By: Matt B.
Date: 4/1/99
Drawing 10 of 26

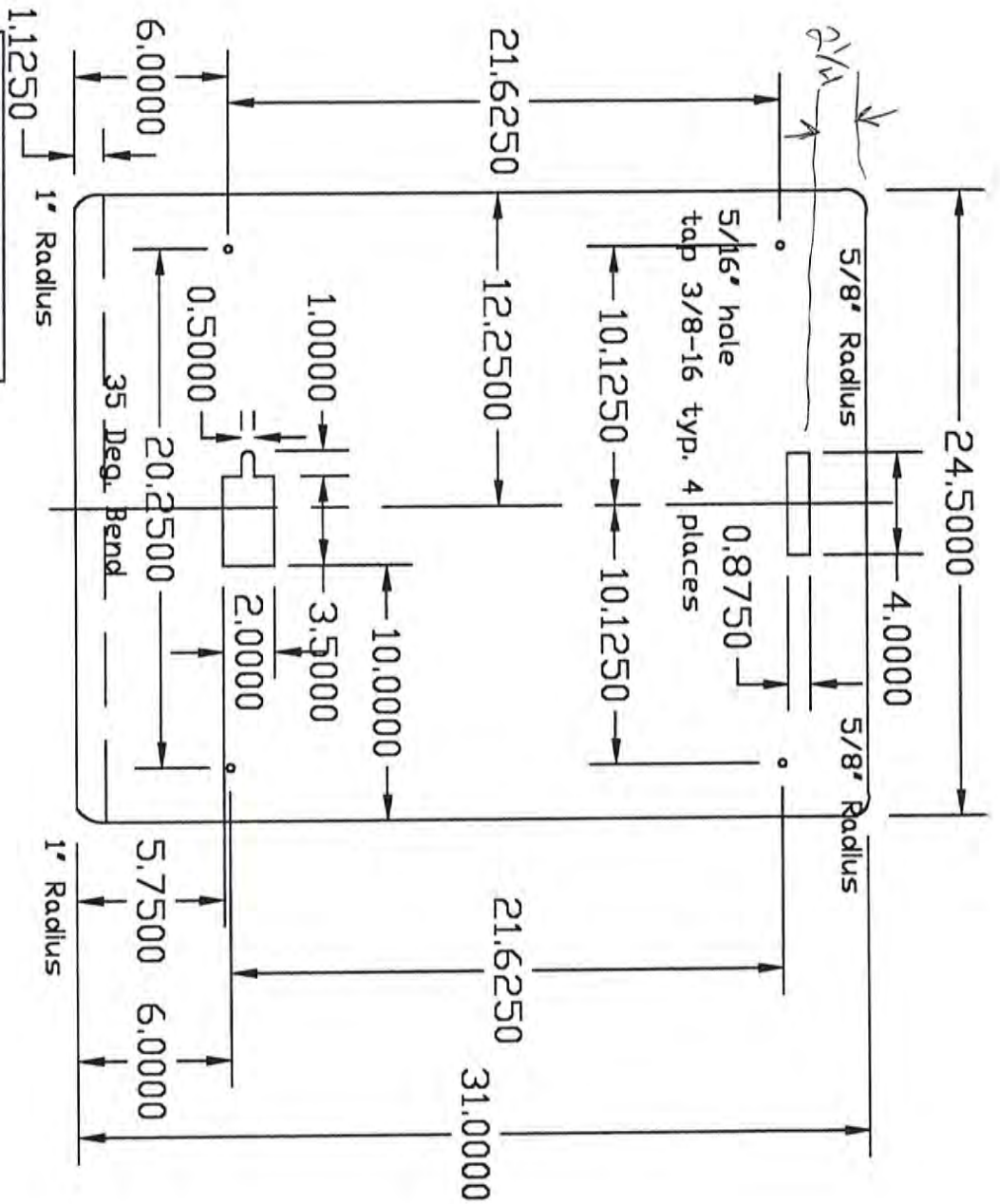
1/2" 13 Thread with a 1.25 flat that measures .375



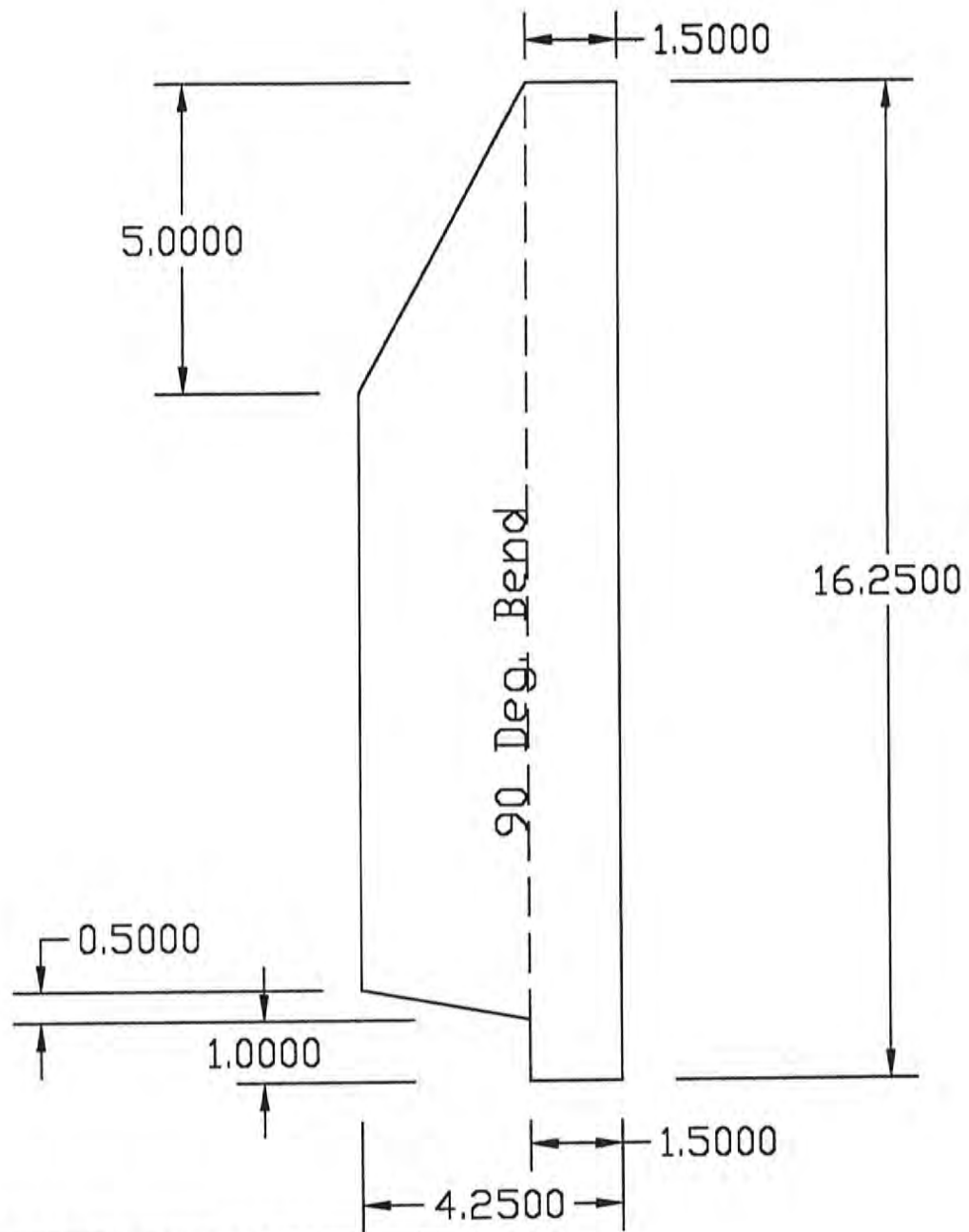
High Valley Stoves
Model 1600
Door Handle
Material Size: 3/4" CR rod X 9.75"
Drawn By: Matt B.
Date: 4/6/99
Drawing 23 of 26



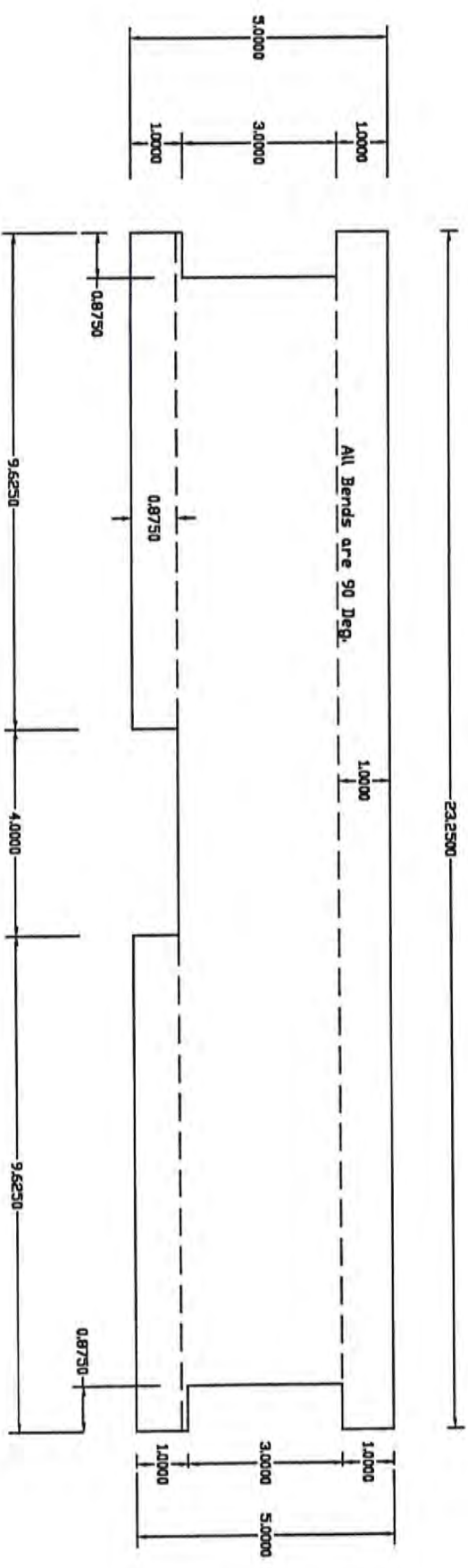
High Valley Stoves
Model 1600
Sketch
Material Size: 12ga X 22 3/4" X 74 1/2"
Drawn By: Hallett B.
Date: 4/12/99
Drawing E1 of 26



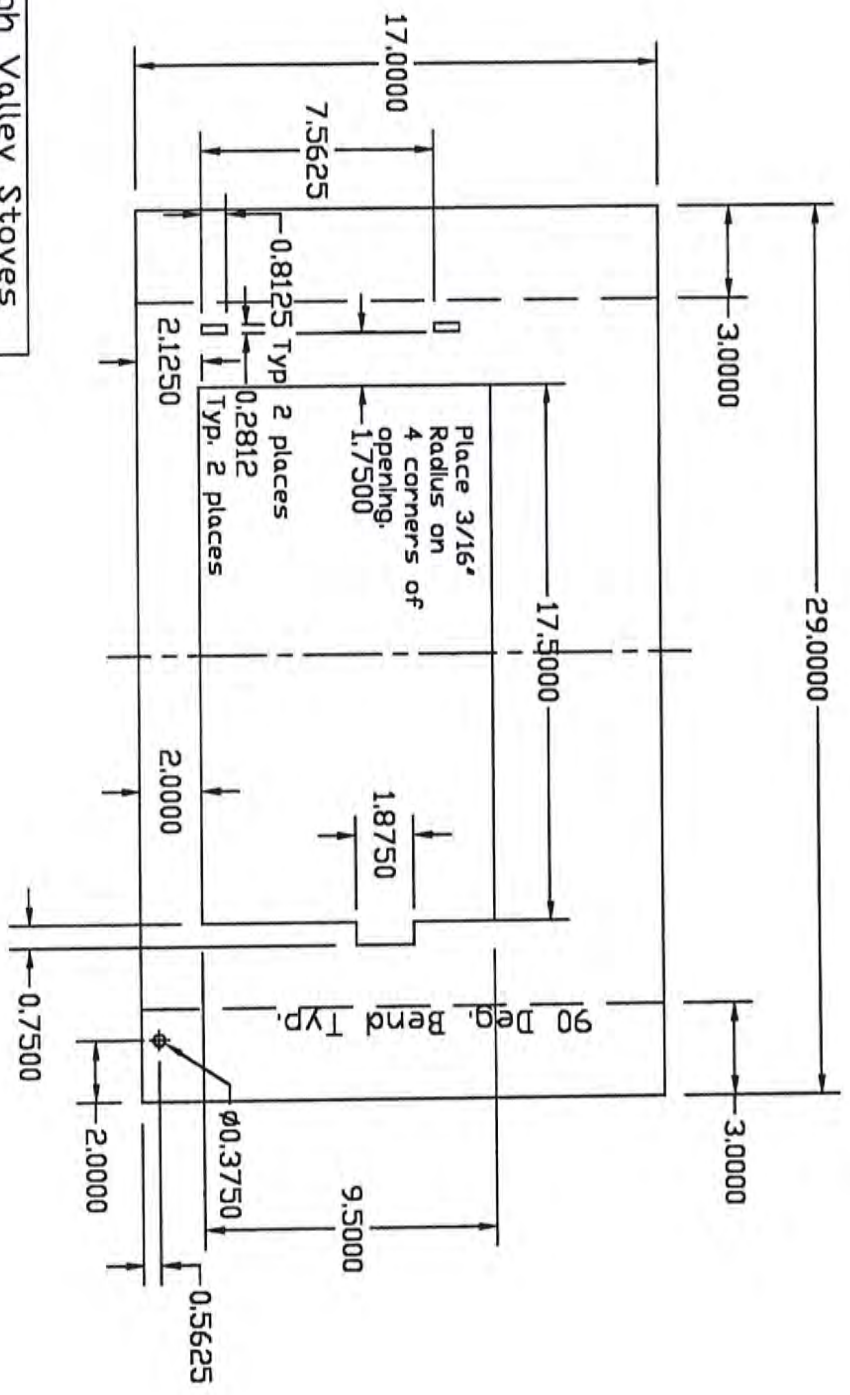
High Valley Stoves
 Step Top Stove
 Hearth and Bottom
 Material Size:
 3/16" X 31" X 24.5"
 Drawn By: Matt B.
 Date: 3/18/99
 Drawing 19 of 26



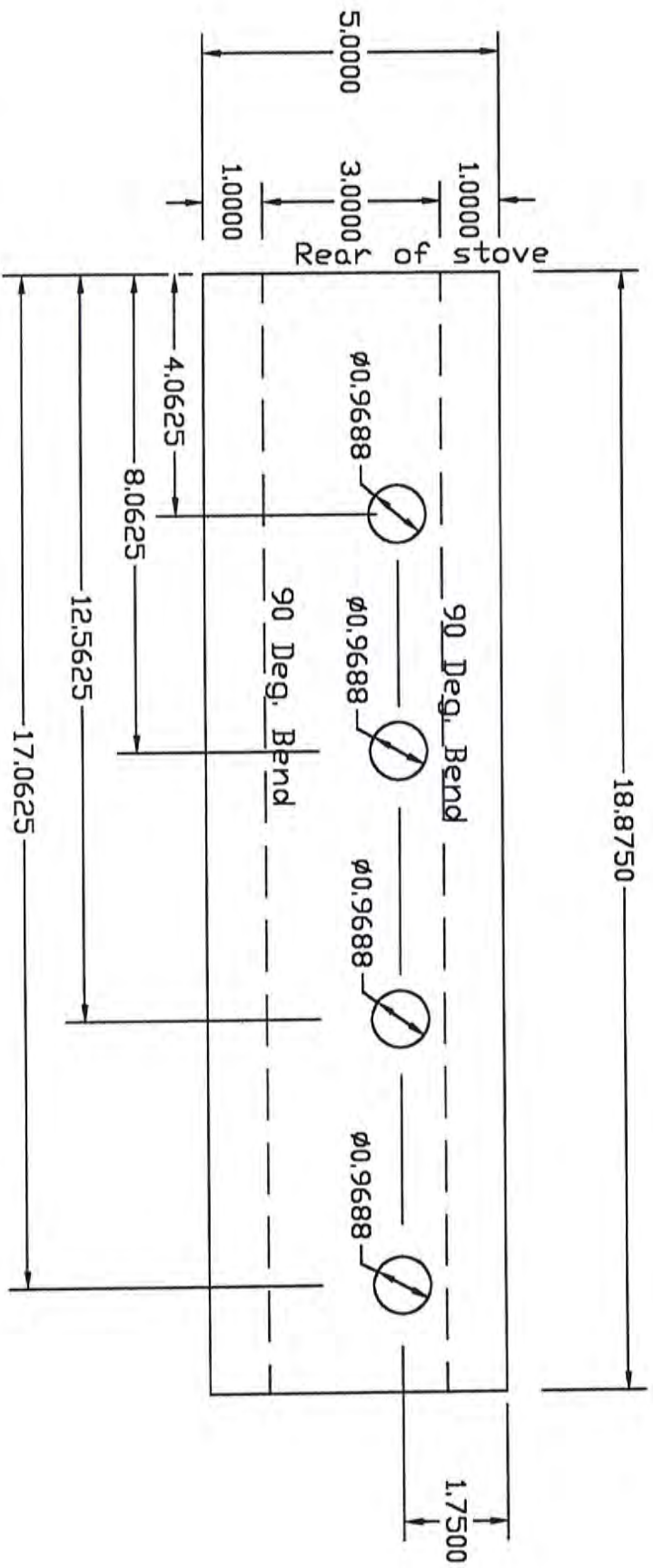
High Valley Stoves
 Step Top
 Side Air Wash Tube
 material Size:
 3/16" X 16.25" X 4.25"
 Drawn By: Matt B.
 Date 3/18/99
 2 required
 Drawing 18 of 26



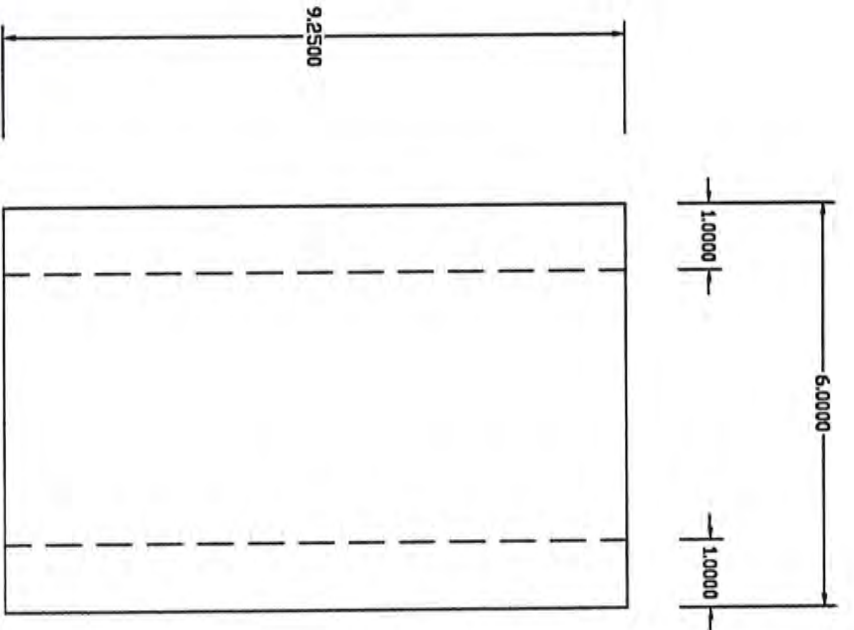
High Valley Stoves
 Model 1600
 Horizontal rear air tube
 Material Size: 3/16" X 23 1/4" X 5"
 Drawn By: Matt B.
 Date: 4/1/99
 Drawing 17 of 26



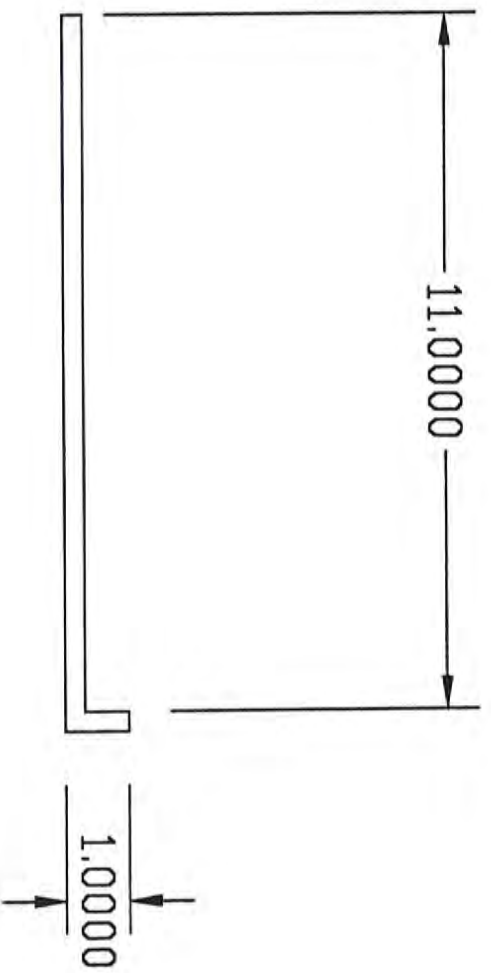
High Valley Stoves
 Step Top Stove
 Front
 Material Size:
 1/4" X 29" X 17"
 Drawn By: Matt B.
 Date: 4/14/99
 Drawing 13 of 26



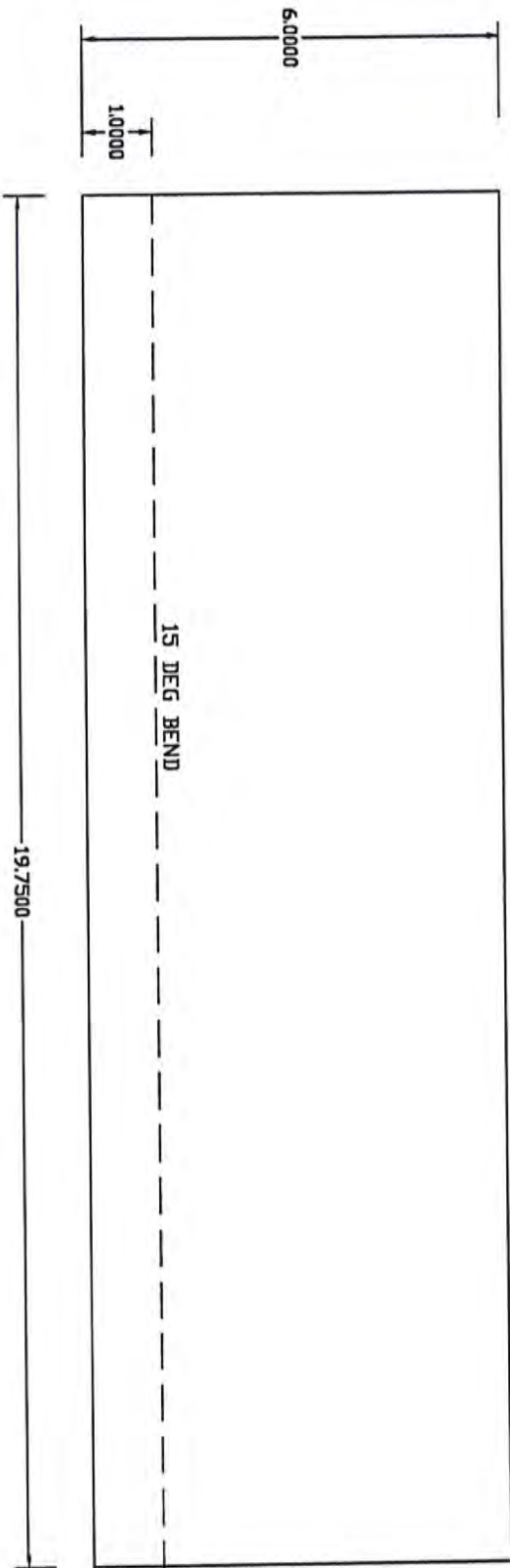
High Valle Stoves
 Model 1600
 Side Air Tube Holder
 Material Size: 3/16" X 5" X 18.875"
 Drawn By: Matt B.
 Date: 3/18/99
 Left and Right Required
 Drawing 14 of 26



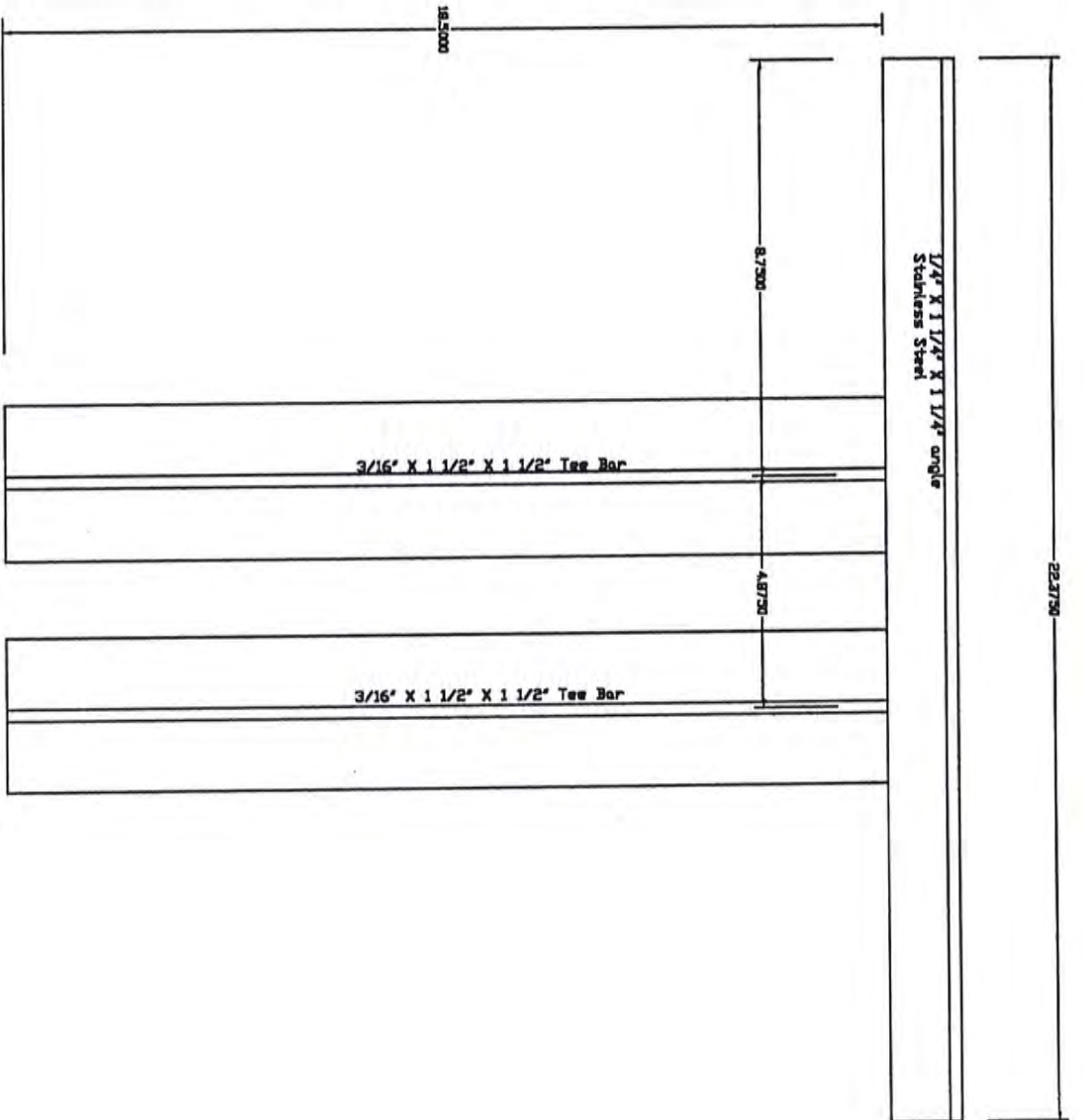
High Valley Stoves
Model 1600
Vertical Rear Air Tube
Material Size: 3/16" X 9.25 X 6"
Drawn By: Matt B.
Date: 4/1/99
Drawing 11 of 26



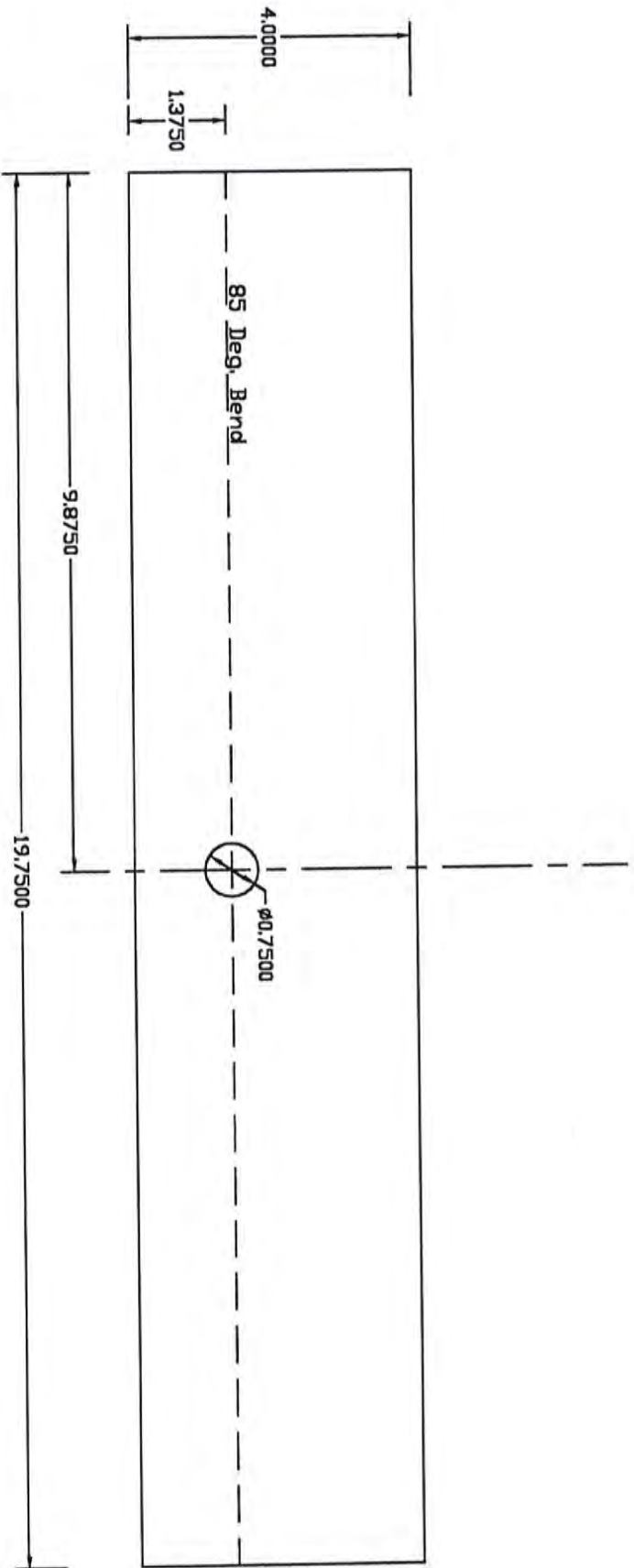
High Valley Stoves
Model 1600
Slide Draft Rod
Material Size: 5/16" X 12" Rod
Drawn By: Matt B.
Date 4/1/99
Drawing 9 of 26



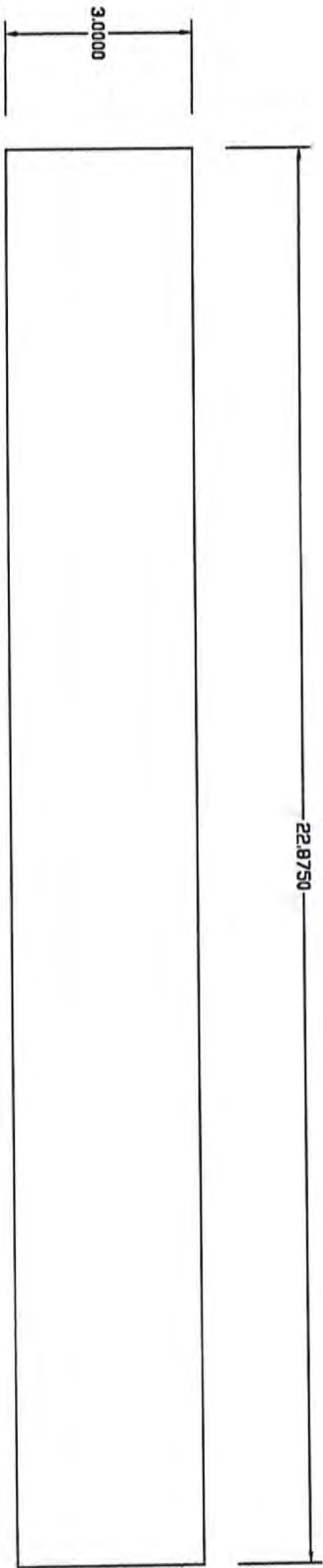
High Valley Stoves
Step Top
Top Air Wash
Material Size:
1/4" X 5.75" X 19.75"
Date: 3/18/99
Drawing 7 of 26



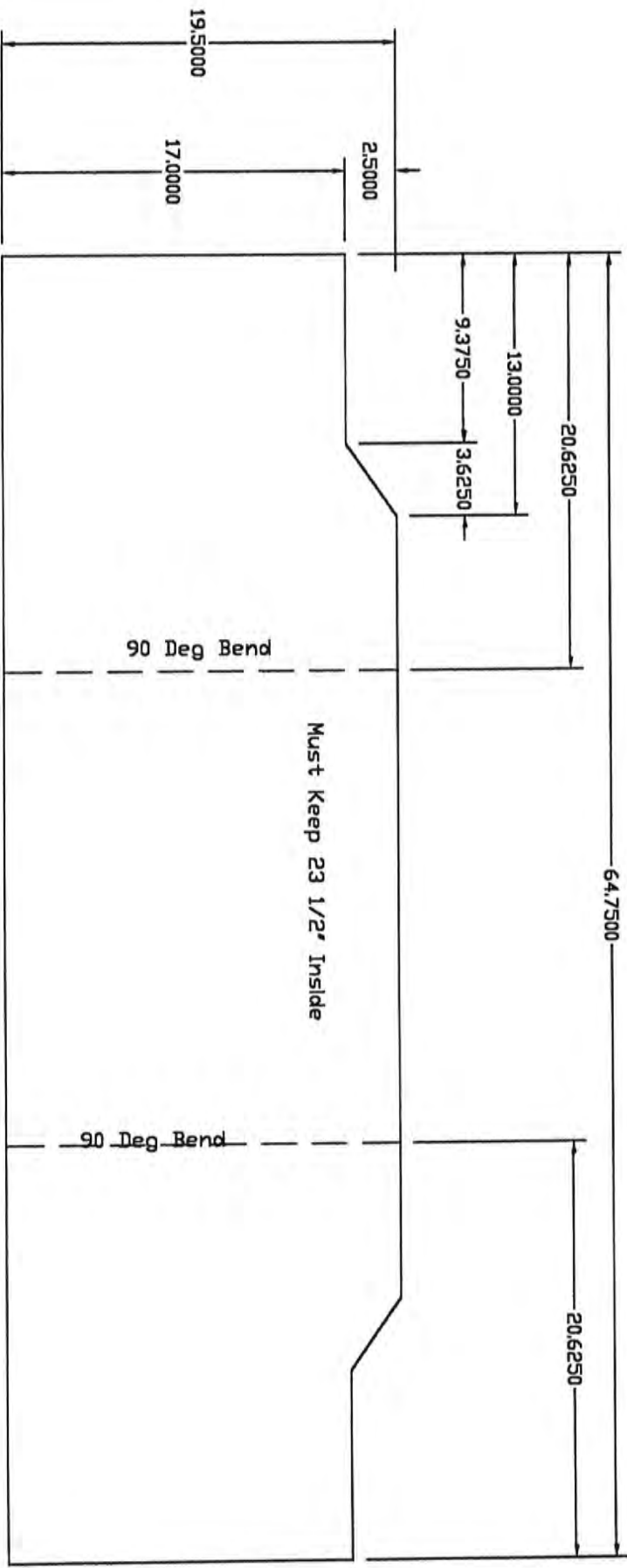
High Valley Stoves
 Model 1600
 Upper Firebrick Shelf
 Material Size
 2 pieces 3/16" X 1 1/2" X 1 1/2" Tee Bar
 1 piece stainless steel 1/4" X 1 1/4" X 1 1/4" angle
 Drawn By Matt B.
 Date 4/7/99
 Drawing 6 of 26



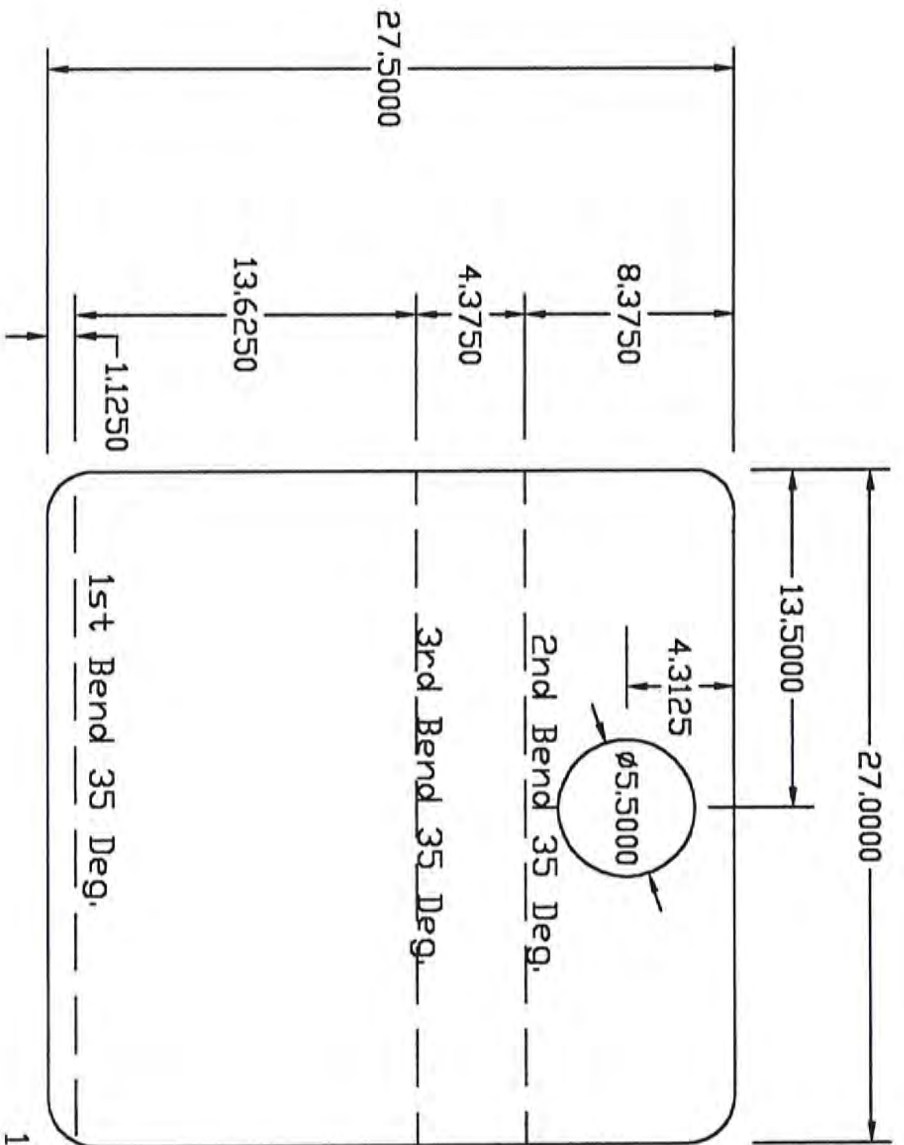
High Valley Stoves
Step Top
Bottom air wash
Material Size:
3/16 X 4.125 X 19.75
Date: 3/18/99
Drawing 8 of 26



High Valley Stoves
Step Top Stove
Top Air Wash Cap
Material Size: 3/16" X 3" X 22.875"
Date 3/18/99
Drawn By: Matt B.
Drawing 12 of 26

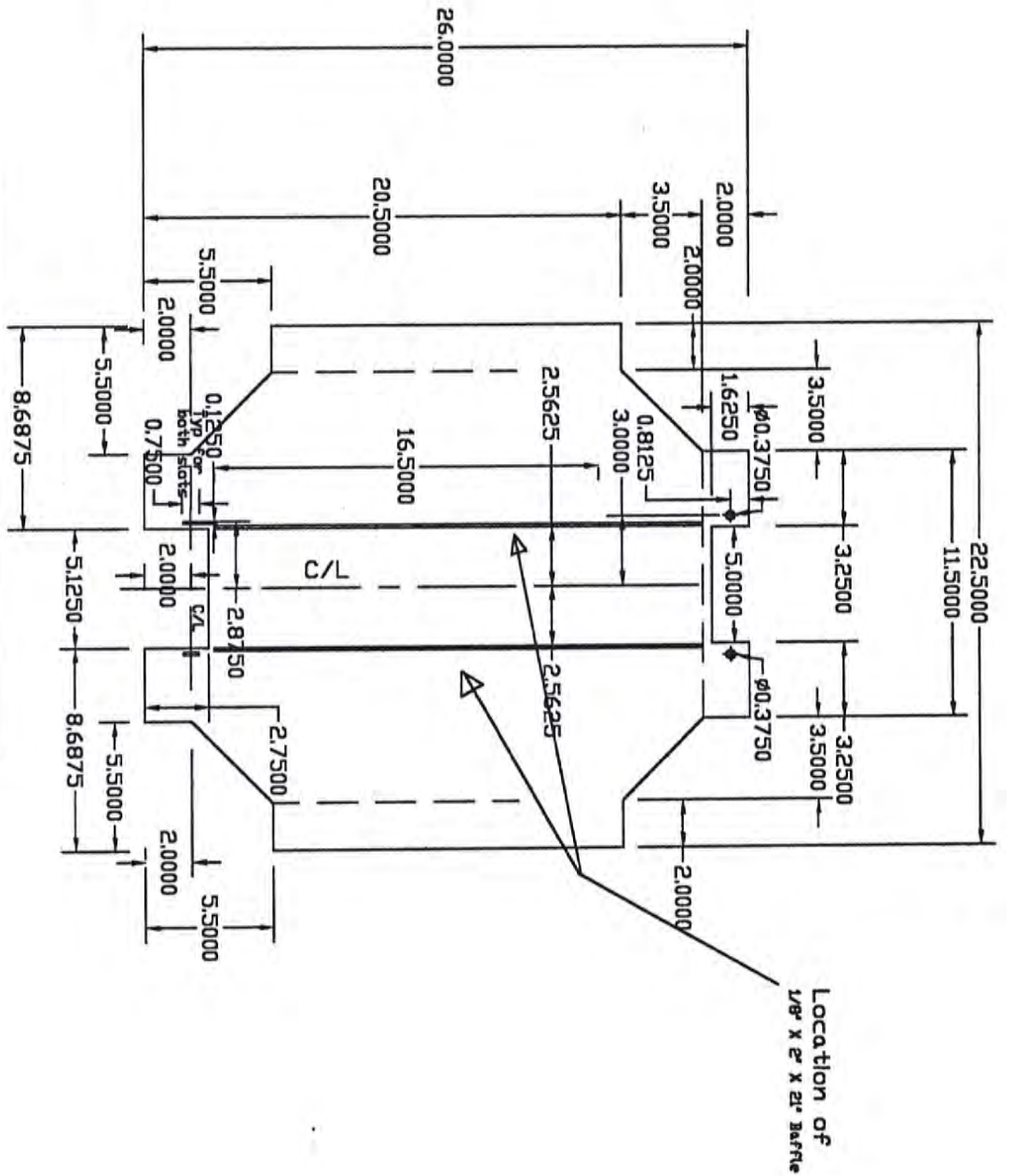


High Valley Stoves
 Step Top Stove
 Firebox
 Material Size: 1/4" X 19.5" X 64.75"
 Drawn By: Matt B.
 Date: 4/15/99
 Drawing 15 of 26

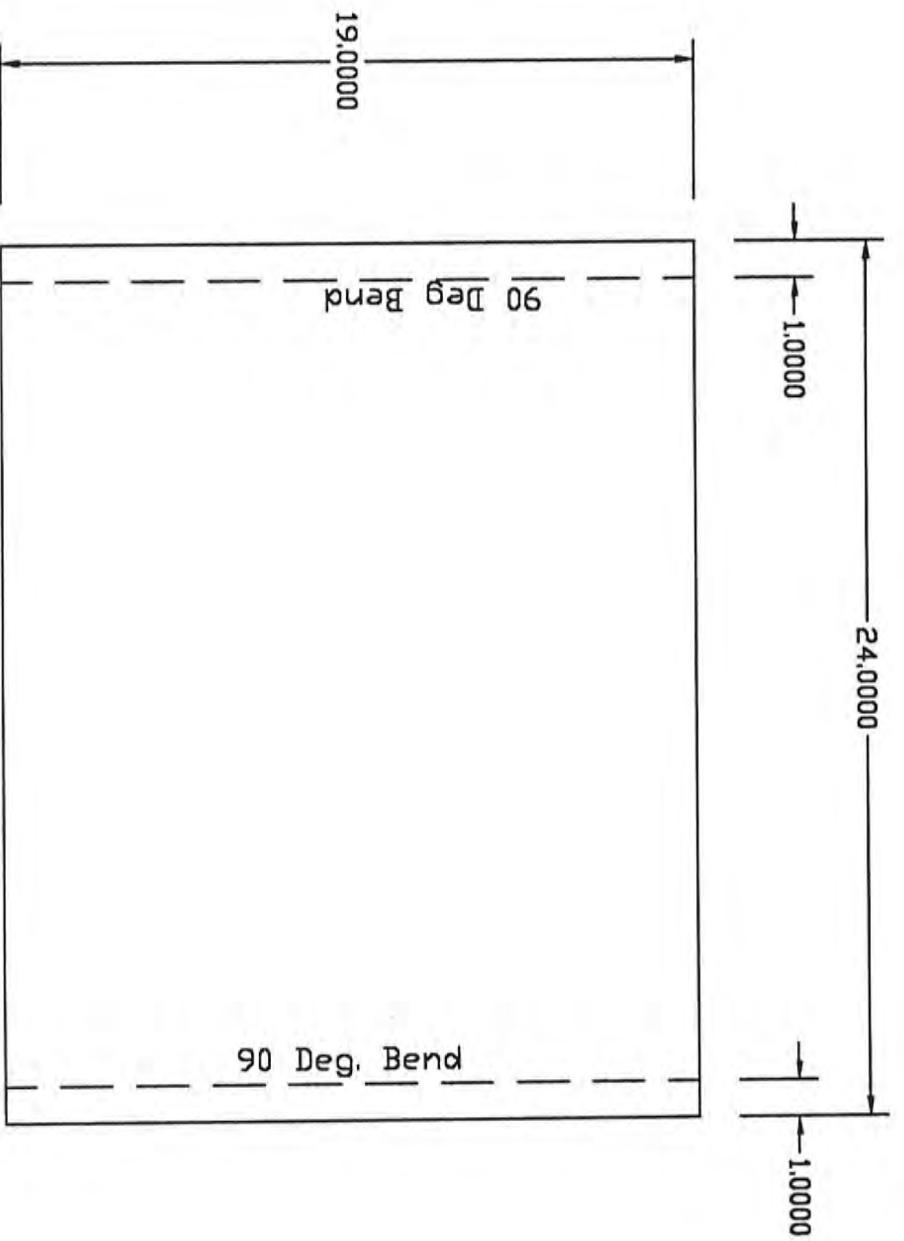


1" Radius on 4 Corners

High Valley Stoves
 Step Top Stove
 Outer Top
 Material Size: 3/8" X 27 1/2" X 27"
 Drawn By: Matt B.
 Date: 3/18/99
 Drawing 16 of 26

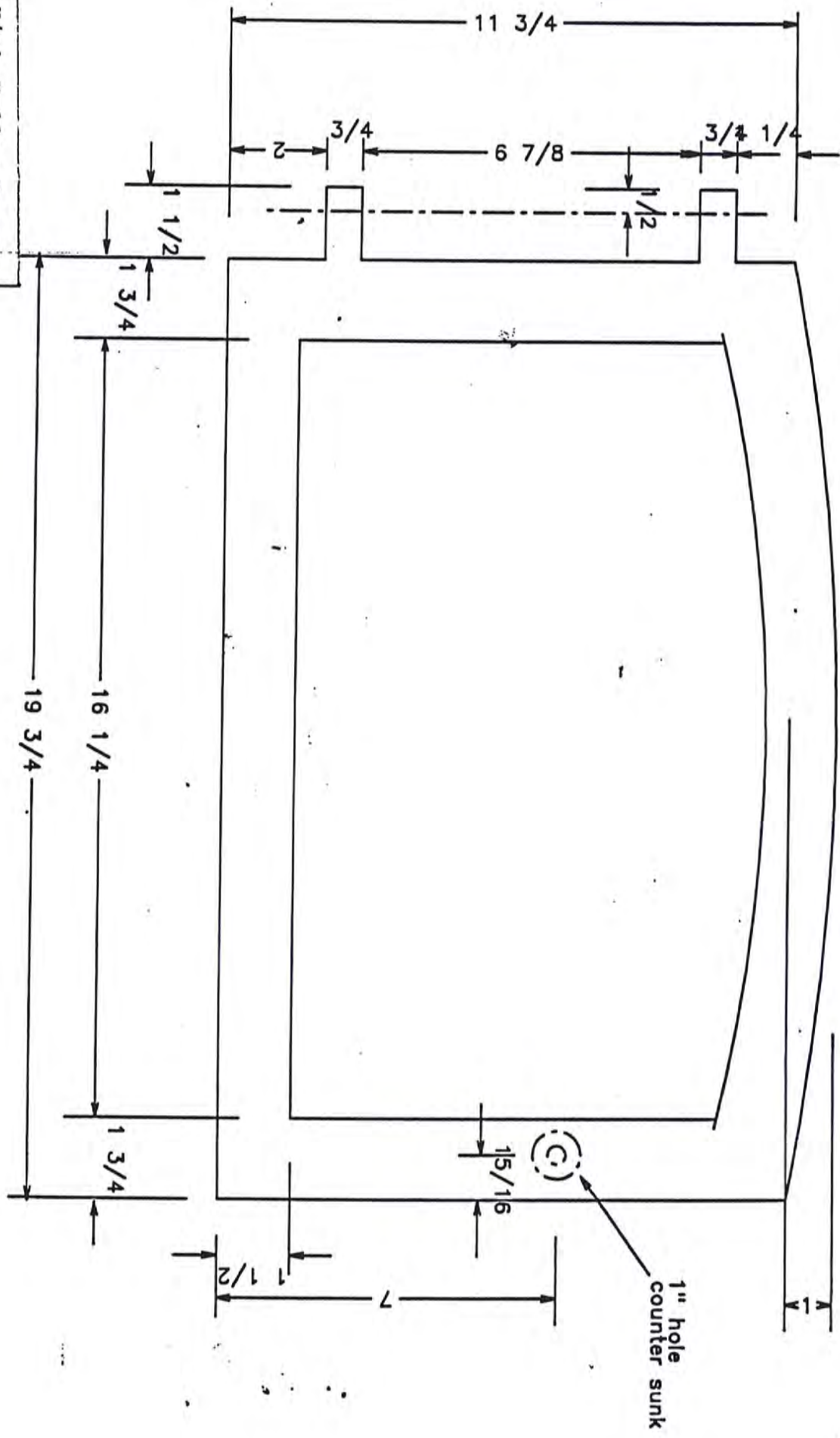


High Valley Stoves
 Model 1600
 Fresh Air Bottom
 Material Size 1/8" X 26" X 22 1/2"
 Date: 3/18/99
 Drawn By: Matt B.
 Drawing 20 of 26

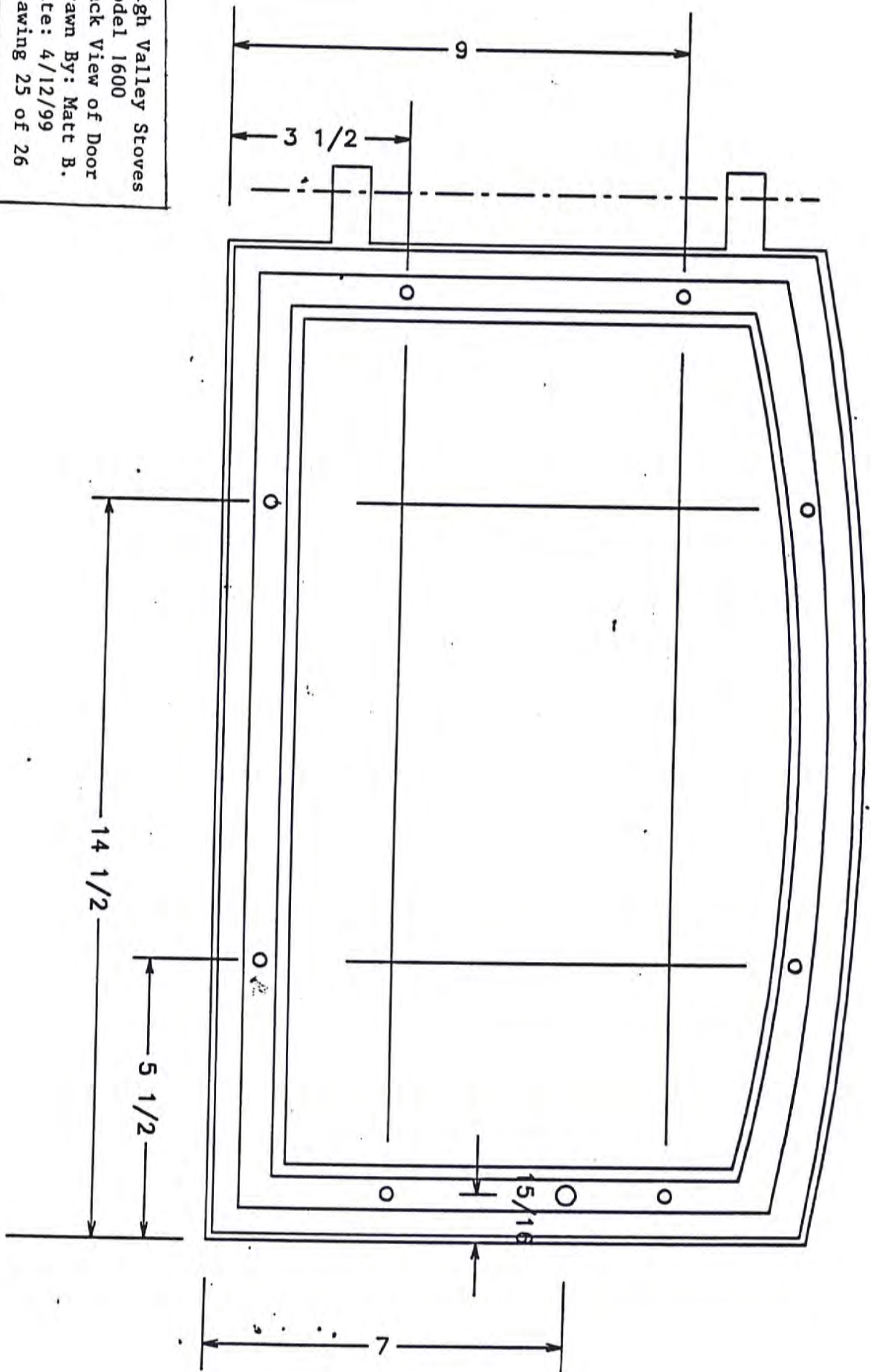


High Valley Stoves
Model 1600
Inner Heat Shield
Material Size: 16ga X 24" X 19"
Drawn By: Matt B.
Date: 4/1/99
Drawing 22 of 26

High Valley Stoves
 Model 1600
 Front View of Door
 Drawn By: Matt B.
 Date: 4/12/99
 Drawing 24 of 26



High Valley Stoves
Model 1600
Back View of Door
Drawn By: Matt B.
Date: 4/12/99
Drawing 25 of 26



High Valley Stoves
Model 1600
Cutaway View of Door
Drawn By: Matt B.
Date: 4/12/99
Drawing 26 of 26

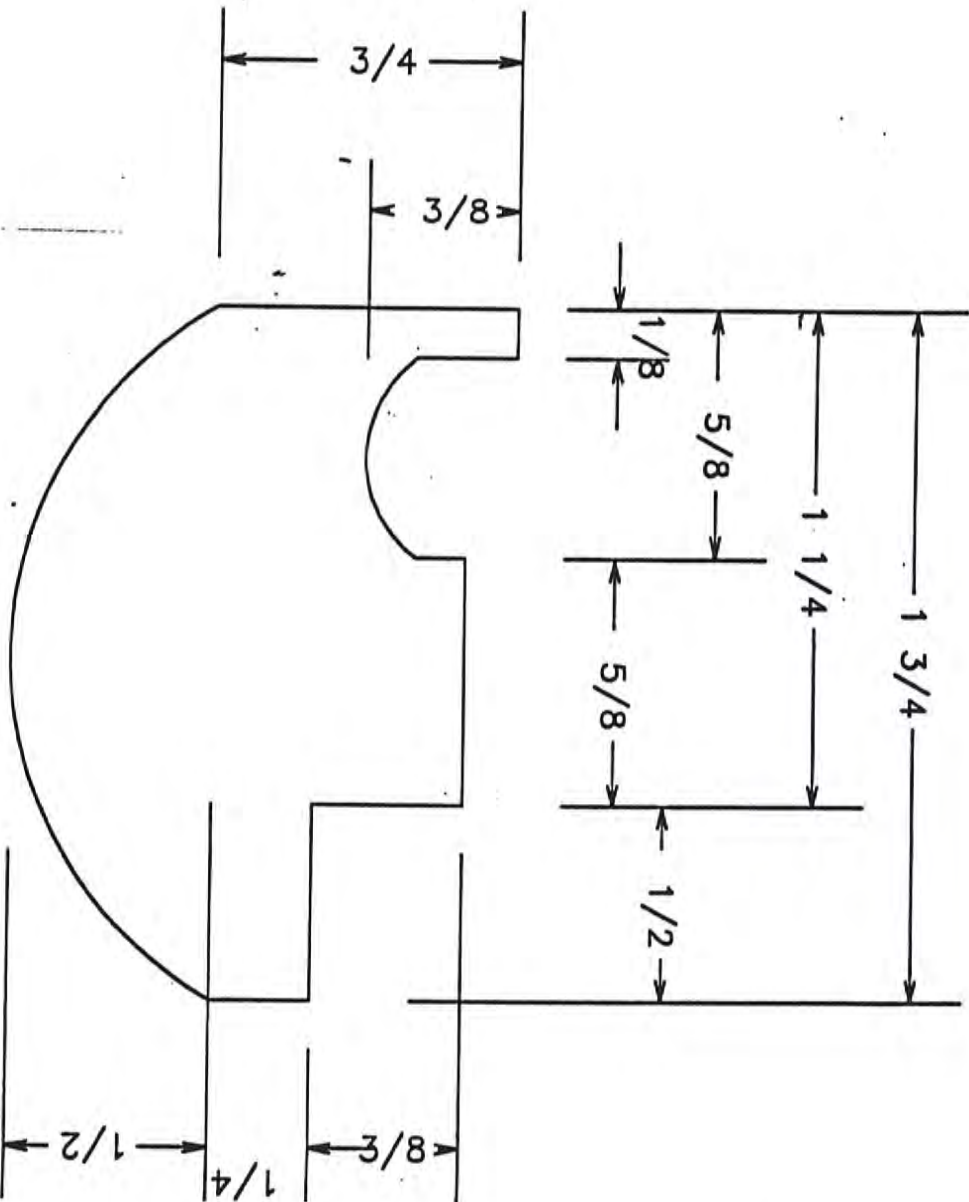


Table of Contents for
Material Safety Data Sheet Section

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Rheostat	Page 12-15
Fiberglass Door Rope	Page 16-17
Fiberglass Bolt Hole Rope (Glass Rope)	Page 18
Blower	Page 19
RTV Silicone (used to secure door rope)	Page 20-21
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Firebrick	Page 26-27
Charcoal Paint	Page 28-33



MATERIAL SAFETY DATA SHEET

1. CHEMICAL PRODUCT AND COMPANY IDENTIFICATION

Trade Name: FIBERFRAX® DURABLANKET® INSULATION PRODUCTS
 Chemical Name: VITREOUS ALUMINOSILICATE FIBERS
 Synonym(s): Ceramic fiber; refractory fiber; MMVF; refractory ceramic fiber; RCF
 synthetic vitreous fiber (SVF), man-made vitreous fiber (MMVF)
 Grade(s): Durablanket® HP; Durablanket® HP-S; Durablanket® S; Durablanket®
 Strip, Duraback®, Duraback® S, Tank Car Insulation, TCB, SMB, QSB600, QSB800.

Manufacturer/Supplier: Unifrax Corporation
 2351 Whirlpool St.
 Niagara Falls, NY 14305-2413

Product Stewardship Information Hotline
 1-800-322-2293 (Monday - Friday 8:00 a.m. - 4:30 p.m. EST)

CHEMTREC Assist: 1-800-424-9300

Effective Date: 03/16/98

Supersedes: 09/18/97

Print Date: 03/25/98

2. COMPOSITION / INFORMATION ON INGREDIENTS

<u>COMPONENTS</u>	<u>CAS NUMBER</u>	<u>% BY WEIGHT</u>
Aluminosilicate fiber (vitreous)	142844-00-6	100

(See Section 8 "Exposure Controls / Personal Protection" for exposure guidelines)

3. HAZARDS IDENTIFICATION

EMERGENCY OVERVIEW

WARNING! POSSIBLE CANCER HAZARD BY INHALATION. MAY CAUSE SKIN, EYE, AND RESPIRATORY TRACT IRRITATION. MAY BE HARMFUL IF INHALED. HAZARD DEPENDS ON DURATION AND LEVEL OF EXPOSURE. WHITE ODORLESS FIBROUS BLANKET.

HAZARD RATINGS

HAZARDOUS MATERIALS INFORMATION SYSTEM (HMIS) RATINGS:

Health: 1* Flammability: 0 Reactivity: 0 Personal Protection Index: X

POTENTIAL HEALTH EFFECTS

- TARGET ORGANS:** Skin, eyes, and lungs.
- INHALATION:** If inhaled in sufficient quantity, may cause respiratory tract irritation. Symptoms may include scratchiness of the nose or throat, cough or chest discomfort.
- EYE CONTACT:** Slightly to moderately irritating. Fibers may be abrasive; prolonged contact may cause damage to the outer surface of the eye.
- SKIN CONTACT:** Slightly to moderately irritating. Exposure may result in irritation, inflammation, rash or itching.
- INGESTION:** If ingested in sufficient quantity, may cause gastrointestinal disturbances. Symptoms may include nausea, vomiting, or abdominal pain.
- CHRONIC EFFECTS:** Studies to date, involving occupationally exposed workers, have not identified any increased incidence of respiratory disease. Long-term, high-dose exposure to specially-sized, rodent respirable fiber has resulted in the development of fibrosis, lung cancer and mesothelioma in rats & hamsters. See Sections 11 & 16 of this MSDS for more information.

MEDICAL CONDITIONS AGGRAVATED BY EXPOSURE:

Pre-existing medical conditions, including dermatitis, asthma or chronic lung disease may be aggravated by exposure; individuals who are atopic (with a history of allergies) may experience greater amounts of skin and respiratory irritation.

HAZARD CLASSIFICATION:

Although studies, involving occupationally exposed workers, have not identified any increased incidence of respiratory disease, results from animal testing have been used as the basis for hazard classification:

The **Seventh Annual Report on Carcinogens (1994)**, prepared by the **National Toxicology Program (NTP)**, classified respirable RCF and glasswool as substances reasonably anticipated to be carcinogens.

The **International Agency for Research on Cancer (IARC)** has classified ceramic fiber, fibrous glasswool and mineral wool (rockwool & slagwool) as possible human carcinogens (Group 2b) based on sufficient evidence of carcinogenicity in animals, but insufficient data in humans.

The **State of California**, pursuant to Proposition 65, The Safe Drinking Water and Toxic Enforcement Act of 1986, has listed "ceramic fibers (airborne fibers of respirable size)" as a material known to the State of California to cause cancer.

The **Commission of The European Communities (DG XI)** has classified RCF as substances which should be regarded as if they are carcinogenic to man.

IARC has also classified respirable crystalline silica, a possible byproduct of RCF devitrification following sustained, high-temperature (>1800°F) use, as a substance known to be carcinogenic to humans (Group 1).

4. FIRST AID MEASURES

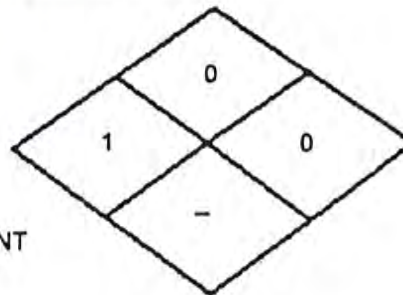
FIRST AID PROCEDURES

- INHALATION:** If respiratory tract irritation occurs, relocate individual to a dust free environment. Get medical attention if irritation persists. See Section 8 for additional measures to reduce or eliminate exposure.
- EYE CONTACT:** If eyes become irritated, flush immediately with large amounts of lukewarm water for at least 15 minutes. Eyelids should be held away from the eyeball to ensure thorough rinsing. Do not rub eyes. Get medical attention if irritation persists.
- SKIN CONTACT:** If skin becomes irritated, remove contaminated clothing. Do not rub or scratch exposed skin. Wash area of contact thoroughly with soap and water. Using a skin cream or lotion after washing may be helpful.
- INGESTION:** If gastrointestinal irritation occurs, relocate individual to a dust free environment. Seek medical attention if symptoms persist.
- NOTES TO PHYSICIANS:** Skin and respiratory effects are the result of mechanical irritation; fiber exposure does not result in allergic manifestations.

5. FIRE FIGHTING MEASURES



- 4 – EXTREME
- 3 – HIGH
- 2 – MODERATE
- 1 – SLIGHT
- 0 – INSIGNIFICANT



NFPA Unusual Hazards: None

Flammable Properties:
Flashpoint: None.
Method: N. App

Flammable Limits:
Lower Flammable Limit: N. App.
Upper Flammable Limit: N. App.

Autoignition Temperature: None.

Hazardous Decomposition Products: None.

Extinguishing Media: Use extinguishing media suitable for type of surrounding fire.

Fire Fighting Instructions: See "Extinguishing Media" above

Unusual Fire and Explosion Hazard: None.

6. ACCIDENTAL RELEASE MEASURES

SPILL PROCEDURES

Use vacuum suction with HEPA filters to clean up spilled material. Use wet sweeping or a dust suppressant where sweeping is necessary.

7. HANDLING AND STORAGE

HANDLING AND STORAGE

Handle ceramic fiber with caution. Minimize airborne dusts by avoiding the unnecessary disturbance of materials.

Prolonged exposure to high temperatures generally increases the relative friability of aluminosilicate fibers. Removal and clean up of after service product may result in exposure to a mixture of crystalline phase silica and vitreous aluminosilicate fiber (See Section 16 for more details). Depending on the product's use, other contaminants may also be present. During removal, the exposed material should be frequently misted with water to minimize airborne dust. A surfactant may be added to the water to improve the wetting process. Use only enough water to wet the insulation. Do not allow water to accumulate on floors.

Clean Up

Dust suppressing cleaning methods such as wet sweeping or vacuuming should be used to clean the work area. If vacuuming is used the vacuum must be equipped with a HEPA filter. Compressed air or dry sweeping should not be used for cleaning. Dust suppressing compounds may be used to clean up light dust.

For additional information regarding the use and handling of refractory ceramic fiber, contact the Unifrax Corporation Product Stewardship Information Line at 1-800-322-2293 (See Section 16).

EMPTY CONTAINERS: Product packaging may contain residue. Do not reuse.

8. EXPOSURE CONTROLS/PERSONAL PROTECTION

EXPOSURE GUIDELINES

<u>Components</u>	<u>OSHA (PEL)</u>	<u>ACGIH (TLV)</u>	<u>SUPPLIER</u>
Aluminosilicate fiber (vitreous)	None Established	None Established	0.5 fiber/cc 8-hr TWA (RCFC)*

* Pending the results of long-term health effects studies, airborne exposures should be controlled at or below the Refractory Ceramic Fiber Coalition (RCFC) Recommended Exposure Guidelines listed above.

ENGINEERING CONTROLS

Dust suppressing control technologies such as local exhaust ventilation, point of generation dust collection, down draft work stations, emission controlling tool designs, and materials handling equipment are effective means of minimizing airborne fiber emissions. For additional information, contact the Unifrax Corporation Product Stewardship Information Line at 1-800-322-2293 (See Section 16).

PERSONAL PROTECTION EQUIPMENT

Respiratory Protection:
Aluminosilicate Fiber

When engineering and/or administrative controls are insufficient, the use of appropriate respiratory protection, pursuant to the requirements of OSHA 1910.134 AND 29 CFR 1926.103, is recommended. The following information is provided as an example of appropriate respiratory protection for aluminosilicate fibers. The evaluation of workplace hazards and the identification of appropriate respiratory protection is best performed, on a case by case basis, by a qualified Industrial Hygienist.

OSHA HAS NOT ESTABLISHED A SPECIFIC PERMISSABLE EXPOSURE LIMIT (PEL) FOR RCF.

SUPPLIERS' RESPIRATORY PROTECTION RECOMMENDATIONS (WHEN HANDLING RCF PRODUCTS)	
<u>Respirable Airborne Fiber Concentration</u>	<u>Respirator Recommendation</u>
Less than 0.5 f/cc	No specific recommendation. User preference based upon conditions present
0.5 f/cc to 5.0 f/cc	Half-face, air purifying respirator equipped with a high-efficiency particulate air (HEPA) filter cartridge
5.0 f/cc to 25 f/cc	Full-facepiece, air purifying respirator equipped with a high-efficiency particulate air (HEPA) filter cartridge
More than 25 f/cc	Full-facepiece, positive pressure supplied air respirator

OTHER INFORMATION:

- (1) Concentrations based upon an eight hour time weighted average (TWA) as determined by air samples collected and analyzed pursuant to NIOSH method 7400 (B) for airborne fibers.
- (2) During furnace tear-out activities after service RCF removals, the manufacturer recommends, at a minimum, the use of full-facepiece air purifying respirator equipped with a high-efficiency particulate air (HEPA) filter cartridge to control fiber and potential crystalline silica exposure.
- (3) In the absence of other objective data or when concentrations are unknown, the manufacturer recommends the use of half-face, air purifying respirator equipped with a high-efficiency particulate air (HEPA) filter cartridge.
- (4) Situations involving a potential exposure to airborne contaminants should be evaluated by a qualified industrial hygienist for the selection of appropriate respiratory protection and air monitoring.
- (5) The American Conference of Governmental Industrial Hygienists (ACGIH) has not adopted a threshold limit value (TLV) recommendation for RCF.

SKIN PROTECTION:

Wear gloves, head coverings and full body clothing as necessary to prevent skin irritation. Washable or disposable clothing may be used. If possible, do not take unwashed clothing home. Work clothes should be washed separately from other clothing and the washing machine rinsed thoroughly following use. Inform the launderer of the proper procedures. Store work clothes and street clothes separately to prevent contamination.

EYE PROTECTION: Wear safety glasses or chemical goggles to prevent eye contact. Do not wear contact lenses unless chemical goggles are also worn. Do not touch eyes with contaminated body parts or materials. Have eye washing facilities readily available where eye contact can occur.

See Section 16 regarding handling considerations for after service aluminosilicate fiber.

9. PHYSICAL AND CHEMICAL PROPERTIES

Odor and Appearance:	White, odorless fibrous blanket.		
Chemical Family:	Vitreous aluminosilicate fibers		
Boiling Point:	N. App.	% Solubility in Water:	N. App.
Melting Point:	1760° C (3200° F)	Specific Gravity:	2.73
Vapor Pressure:	N. App.	pH:	N. App.
Vapor Density (Air = 1):	N. App.	% Volatile:	N. App.
Molecular Weight:	N. App.	Molecular Formula:	Al ₃ O ₃ · 1.6SiO ₂

10. STABILITY AND REACTIVITY

CHEMICAL STABILITY: Stable under conditions of normal use.

INCOMPATIBILITY: Soluble in hydrofluoric acid, phosphoric acid, and concentrated alkali.

CONDITIONS TO AVOID: None.

HAZARDOUS DECOMPOSITION PRODUCTS: None.

HAZARDOUS POLYMERIZATION: Not Applicable.

11. TOXICOLOGICAL INFORMATION

The existing toxicology and epidemiology data bases for RCF's are based on ongoing studies. The Unifrax Corporation supports ongoing investigations and will make all data available to interested parties upon request. Information will be updated as studies are completed and reviewed. The following is a summary of the results to date:

EPIDEMIOLOGY

An epidemiologic investigation, being conducted by the University of Cincinnati, of RCF production workers in the U.S. is ongoing. The evidence obtained from employees in U. S. RCF manufacturing facilities, is as follows:

- 1) There is no evidence of any fibrotic lung disease (interstitial fibrosis) on x-ray.
- 2) There is no evidence of an elevated incidence of lung disease among RCF manufacturing employees who were exposed to RCF.

3) In the exposed population, a statistical "trend", comparing initial test results (circa 1987) to predicted norms as based on breathing tests, was observed between the duration of exposure to RCF and a decrease in some measures of pulmonary function. The observations are considered to be statistically significant, but clinically insignificant. In other words, if these observations were made on an individual employee, the results would be interpreted as being within the normal (predicted) respiratory range. A more recent longitudinal study of employees with 5 or more pulmonary function tests found that there was no further effect on lung function associated with RCF production experience.

4) Initial data (circa 1987) indicated that the decrease in pulmonary function appears to be greater in employees who smoke. RCF exposure and smoking behavior seem to demonstrate an interactive effect; in other words, RCF-exposed smokers seemed to show a greater decrease in respiratory function than would be produced by combining the average decrease observed from RCF-exposure only and smoking behavior only. More recent data and analysis have found that the smoking/production interactive effect is no longer observable. Nonetheless, to promote good health practices, employees are still actively encouraged not to smoke.

5) Pleural plaques, which are discrete areas of pleural thickening usually on the parietal pleura or diaphragm, have been observed in a small number of RCF employees. There appears to be a dose-response relationship between the occurrence of pleural plaques on chest radiographs and the following variables: a) years since RCF production hire date; b) duration of RCF production employment; and c) cumulative RCF exposure. The best evidence to date indicates that pleural plaques are a marker of exposure only. There is virtually no evidence to suggest that pleural plaques are a precursor mechanism of respiratory conditions such as interstitial fibrosis, lung cancer, or mesothelioma. Under most circumstances, pleural plaques are not associated with pulmonary impairment. The pathogenesis of pleural plaques remains incompletely understood; however, the mechanism appears to be an inflammatory response caused by inhaled fibers transported via lymphatics to the subpleural area.

TOXICOLOGY

Man-made vitreous fiber (MMVF) based products, including RCF, contain fibers of different sizes, some of which are small enough to be respirable by humans. Scientists have been conducting research since the 1950's to determine the potential risks for adverse health effects which may result from fiber inhalation.

In 1987 the International Agency for Research on Cancer (IARC) classified man-made vitreous fibers including glasswool, rockwool, slagwool, and RCF as possible human carcinogens (2B). More recently, the U.S. Department of Health and Human Services classified the respirable fibers of glasswool and RCF as "substances which may reasonably be anticipated to be carcinogens" (National Toxicology Program, 7th Annual Report on Carcinogens, 1994).

To date, a number of toxicological studies have been conducted which utilize non-physiological exposure methods such as intrapleural, intraperitoneal and intratracheal implantation or injection. Some of these studies concluded that RCF is a potential carcinogen. Some experts, however, suggest that these tests have limited relevance because they bypass many of the biological mechanisms which prevent fiber deposition or facilitate fiber clearance.

Other toxicological studies utilizing a physiological exposure method, inhalation, have produced findings of respiratory disease in rodents. The most recent RCF-inhalation studies were conducted at the Research and Consulting Company, Geneva, Switzerland. Rats and hamsters were exposed, using a nose-only inhalation system, to the "maximum tolerated dose" of 30 mg/m³ (about 200 fibers/cc) of specially-prepared RCF for 6 hours/day, 5 days/week, for up to 24 months. In another research effort, other rats were exposed, in a multi-dose study with a similar protocol, to doses of 3 mg/m³, 9 mg/m³, and 16 mg/m³, which corresponds to about 25, 75, and 115 fibers/cc.

No acute respiratory effects were seen in the rats in the 3 mg/m³ exposure group. Some cases of mild parenchymal fibrosis and one mesothelioma were observed in the 9 mg/m³ group. Some cases of pleural and parenchymal fibrosis were seen in the 16 mg/m³ and in the 30 mg/m³ exposure group. In addition to a statistically significant increase in lung tumors, two mesotheliomas were also observed in the 30 mg/m³ group. Hamsters, exposed to only the highest dose, did not develop lung tumors. However, a moderate amount of interstitial fibrosis was seen, as well as a 42% incidence rate of mesothelial tumors.

These studies have found RCF to be a rodent carcinogen, under the conditions of lifetime exposure at high doses. These studies suggest that there may be a dose/response threshold, below which irreversible respiratory impacts do not occur.

To obtain more epidemiology or toxicology information, please call the toll free telephone number for the Unifrax Corporation Product Stewardship Program found in Section 16 - Other Information.

12. ECOLOGICAL INFORMATION

Ecotoxicological Information:	No data available.
Distribution:	No data available.
Chemical Fate Information:	No data available.

13. DISPOSAL CONSIDERATIONS

DISPOSAL: Aluminosilicate fiber is not classified as a hazardous waste according to Federal regulations (40 CFR 261). Check local, regional, state or provincial regulations for applicable requirements for disposal. Any processing, use, alteration or chemical additions to the product, as purchased, may alter the disposal requirements. Under Federal regulations, it is the waste generator's responsibility to properly characterize a waste material, to determine if it is a "hazardous" waste.

EMPTY CONTAINERS: Product packaging may contain product residue. Do not reuse.

14. TRANSPORT INFORMATION

U.S. DEPARTMENT OF TRANSPORTATION (DOT)

BILL OF LADING DESCRIPTION (49 CFR 172.202): FIBERFRAX® DURABLANKET® INSULATION PRODUCTS (NON-REGULATED)

UNITED NATIONS (UN) NUMBER: NOT APPLICABLE

NORTH AMERICA (NA) NUMBER: NOT APPLICABLE

15. REGULATORY INFORMATION

Key statutory and regulatory classifications or listings for the product, as manufactured, which may impact product storage, use, handling or disposal:

U.S. FEDERAL REGULATIONS

Comprehensive Environmental Response Compensation and Liability Act of 1980 (CERCLA):

Constituents regulated as hazardous substances under the Comprehensive Environmental Response Compensation and Liability Act (CERCLA 40 CFR 302):

<u>Constituent</u>	<u>RQ in Pounds</u>
NONE	

Most RCF products, including this product, are composed of RCF with an average diameter greater than 1 micron, and therefore are not considered CERCLA hazardous substances. See 60 FR 30934 (June 12, 1995).

Clean Air Act (CAA):

Substances regulated as hazardous air pollutants under Section 112 of the Clean Air Act Amendments of 1990:

Chemical Name
NONE

Most RCF products, including this product, are composed of RCF with an average diameter greater than 1 micron, and therefore are not considered hazardous air pollutants. See 60 FR 30934 (June 12, 1995).

Toxic Substances Control Act (TSCA):

All substances in this product are listed, as required, on the TSCA inventory. Refractory ceramic fiber has been assigned a CAS number; however, it is a simple mixture and therefore not required to be listed on the TSCA inventory. The components of RCF are listed on the inventory.

This product contains refractory ceramic fiber and is subject to an EPA TSCA Section 5(e) Consent Order and may be subject to TSCA Section 12(b) Export Notification requirements. Monitoring of airborne workplace fiber concentrations is being conducted under the consent order. For more information on this program, contact the Unifrax Corporation Product Stewardship Information Line at 1-800-322-2293 (See Section 16).

Superfund Amendments and Reauthorization Act (SARA) Title III Information:

SARA Hazard Category:

Listed below are the hazard categories for the Superfund Amendments and Reauthorization Act (SARA) Section 311/312 (40 CFR 370):

Immediate Hazard: — Fire Hazard: — Reactivity Hazard: —
Delayed Hazard: X Pressure Hazard: —

SARA 313 Information:

Toxic chemical(s) subject to the annual reporting requirements of the Superfund Amendments and Reauthorization Act (SARA) Section 313 (40 CFR 372):

Chemical Name CAS Number Concentration
NONE

EPA has proposed to place man-made mineral fibers, including RCF, on the list of substances subject to the annual TRI reporting requirements, but a final listing decision has been deferred indefinitely. See 59 FR 61439 (November 30, 1994).

SARA 302/311/312 Information:

Extremely hazardous substances subject to the notification and inventory reporting requirements of the Superfund Amendments and Reauthorization Act (SARA) Section 302 (40 CFR 355) and Section 311/312 (40 CFR 370) respectively:

Chemical Name CAS Number Concentration
NONE

STATE REGULATIONS

California:

Substance(s) listed by the State of California on Proposition 65, the Safe Drinking Water and Toxic Enforcement Act of 1986:

Chemical Name CAS Number
Ceramic fibers (airborne particles of respirable size) 142844-00-6

New Jersey:

Chemical(s) which are listed as a special health hazard substance as defined in New Jersey Worker and Community Right to Know Act, New Jersey Administrative Code, Title 8, Department of Health, Chapter 59, Subchapter 10:

<u>Chemical Name</u>	<u>CAS Number</u>
NONE	

Pennsylvania:

Chemical(s) which are listed as a special health hazard substance as defined in Pennsylvania Right-to-Know Law, Section 3800:

<u>Chemical Name</u>	<u>CAS Number</u>
NONE	

INTERNATIONAL REGULATIONS

Canadian Workplace Hazardous Materials Information System (WHMIS):

The following Canadian Workplace Hazardous Materials Information System (WHMIS) categories apply to this product:

Compressed Gas: – Flammable/Combustible: – Oxidizer: – Acutely Toxic: –
Other Toxic Effects: X Biohazardous: – Corrosive: – Dangerously Reactive: –

Canadian Environmental Protection Act (CEPA):

All substances in this product are listed, as required, on the Domestic Substances List (DSL).

Chemical(s) which are listed on the Non-Domestic Substances List:

<u>Chemical Name</u>	<u>CAS Number</u>
NONE	

16. OTHER INFORMATION

After Service RCF: Removal

As manufactured, RCF products are vitreous aluminosilicates which do not contain respirable crystalline silica. However, following sustained, high temperature (>1800°F) use, it is possible for portions of the exposed RCF to devitrify into mullite or crystalline phase silica (cristobalite or quartz). Chronic exposure to respirable crystalline silica may lead to lung disease. IARC has concluded that: "Crystalline silica inhaled in the form of quartz or cristobalite from occupational sources is carcinogenic to humans (Group 1)." [IARC Monograph 68, June 1997, p. 210-211]. The Occupational Safety and Health Administration (OSHA) has adopted a permissible exposure limit (PEL) for respirable cristobalite at 0.05 mg/m³. When needed, the use of proper exposure controls and respiratory protection is recommended to reduce potential health risks and to ensure compliance with OSHA requirements. The evaluation of workplace hazards and the identification of appropriate respiratory protection is best performed, on a case by case basis, by a qualified Industrial Hygienist. For more detailed information regarding respirable crystalline silica, call the Product Stewardship Information Hotline (see below).

Product Stewardship Program

The Unifrax Corporation has established a program to provide customers with up-to-date information regarding the proper use and handling of refractory ceramic fiber. In addition, Unifrax Corporation has also established a program to monitor airborne fiber concentrations at customer facilities. If you would like more information about this program, please call the Unifrax Corporation Product Stewardship Information Hotline at 1-800-322-2293.

Definitions:

ACGIH:	American Conference of Governmental Industrial Hygienists
CAS:	Chemical Abstracts Service
EPA:	Environmental Protection Agency
f/cc:	Fibers per cubic centimeter
HEPA:	High Efficiency Particulate Air
HMIS:	Hazardous Materials Information System
mg/m³:	Milligrams per cubic meter of air
NFPA:	National Fire Protection Association
NIOSH:	National Institute for Occupational Safety and Health
OSHA:	Occupational Safety and Health Administration
	29 CFR 1910.134 & 1926.103: OSHA Respiratory Protection Standard
	29 CFR 1910.1200 & 1926.59: OSHA Hazard Communication Standard
PEL:	Permissible Exposure Limit
RCRA:	Resource Conservation and Recovery Act
SARA:	Superfund Amendments and Reauthorization Act
Title III:	Emergency Planning and Community Right to Know Act
Section 302:	Extremely Hazardous Substances
Section 304:	Emergency Release
Section 311:	MSDS/List of Chemicals and Hazardous Inventory
Section 312:	Emergency and Hazardous Inventory
Section 313:	Toxic Chemicals and Release Reporting
SVF:	Synthetic Vitreous Fiber
TLV:	Threshold Limit Value (ACGIH)
TSCA:	Toxic Substances Control Act

Revision Summary: Section 2: Added reference to Section 8. Section 3: Moved NFPA ratings to Section 5, added diamond, added "Hazard Classification" subsection. Section 8: Revised REG, Revised PPE table. Section 11: Replaced reference to MMVF with SVF. Section 13: added "listed or characteristic". Section 14: Added UN and NA information. Section 16: added "crystalline phase silica (cristobalite or quartz)". Added definitions.

MSDS Prepared By: UNIFRAX HSEQ DEPARTMENT

DISCLAIMER

The information presented herein is based on data considered to be accurate as of the date of preparation of this Material Safety Data Sheet. However, no warranty or representation, express or implied, is made as to the accuracy or completeness of the foregoing data and safety information. In addition, no responsibility can be assumed by vendor for any damage or injury resulting from abnormal use, from any failure to adhere to recommended practices, or from any hazards inherent in the nature of the product.



"The Right Control
for Your Application"

KB ELECTRONICS, INC., 73 Wortman Avenue, Brooklyn, New York 11207 (718) 257-3300

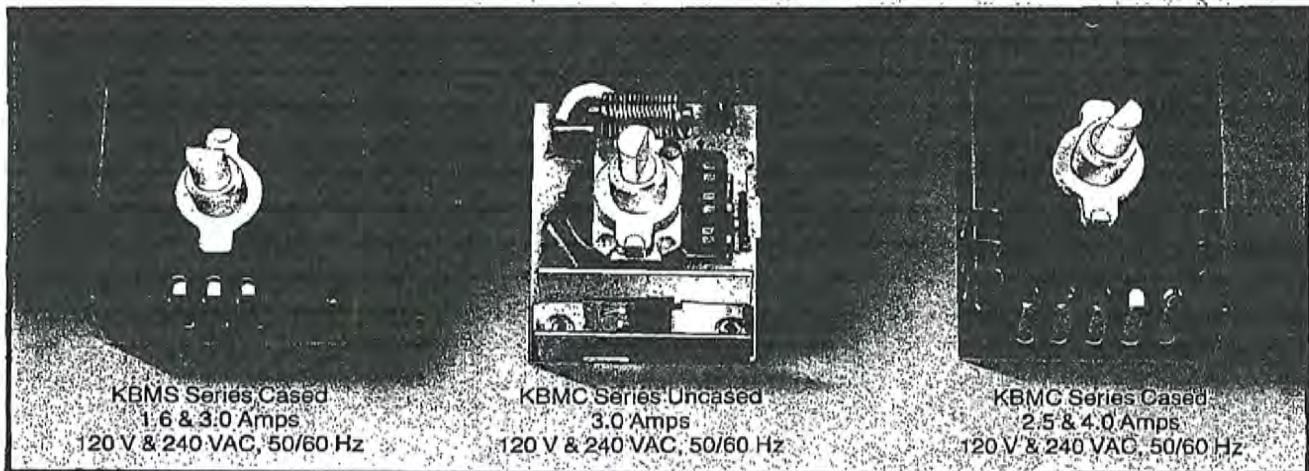
TWX (710) 584-2308

FAX (718) 257-4740

Post-it® Fax Note	7671	Date	4/8	# of pages	4
To	matt Buchanan		From	JOSEFINA	
Co./Dept.			Co.	KB Electronics	
Phone #			Phone #	954-346-4900	
Fax #	828-765-6850		Fax #		

DATA SHEET D-157

KBMC and KBMS Variable Speed Solid State AC Motor Controls



KBMS Series Cased
1.6 & 3.0 Amps
120 V & 240 VAC, 50/60 Hz

KBMC Series Uncased
3.0 Amps
120 V & 240 VAC, 50/60 Hz

KBMC Series Cased
2.5 & 4.0 Amps
120 V & 240 VAC, 50/60 Hz

—NEW EXPANDED LINE—

Designed for Speed Control
of Shaded Pole, AC/DC and Permanent Split
Capacitor (PSC) Motors

AVAILABLE FEATURES

- Flame Retardant ABS Enclosure
- High-Gain Radio Noise Filter
- Minimum Speed Trimpot
- On/Off Rotary Line Switch
- Kit for Wall Box Mounting
- Lever-Trol™ Option

TYPICAL APPLICATIONS

- Ceiling Fans • Range Hoods • Whole-House Attic Fans
- Vibrators • Humidifiers • Air Conditioners
- Fireplace Blowers • Window Fans •

UL Recognized* — CSA Certified*

DESCRIPTION

The KBMC and KBMS solid state controls provide infinitely variable speed control of Shaded Pole, PSC, and AC/DC motors. The consumer is allowed selection of air volume, noise level, and energy consumption to individual preference. Solid state variable speed controls are designed to replace obsolete tapped windings, chokes, rheostats, and other methods which are currently being used to obtain speed variation. All models utilize full-wave phase control circuitry which minimizes power loss and heat dissipation. A standard self-threading Zytel mounting bushing and potentiometer shaft is used for added electrical isolation. In addition, customized metal bushings and shafts may be obtained on special order. The controls are available with an internal on/off line switch and are also available with an optional third lead which can be used to control auxiliary circuits such as relays and indicator lamps. A high-gain radio noise suppression filter and a minimum speed trimpot are also available on all models. Specifically designed for OEM applications, the KBMC and KBMS Series offer a large selection of mounting arrangements, ratings, and options. A wall mounting kit is available which includes dial plate, knob, mounting strap, hardware and instructions. Units are normally supplied with a flame retardant ABS case; however, the KBMC Series is available uncased. Controls are UL Recognized and CSA Certified. *Special lead lengths and colors are available upon request. A mounting nut is supplied as standard with all controls.

*Most models — consult factory.

TECHNICAL DATA D-157

ELECTRICAL RATINGS

MODEL	VOLTAGE (VAC 50/60 Hz)	CURRENT (RMS AMPS)
KBMC-13BV	120	2.5*
KBMC-14BV	120	4.0
KBMC-23BV	240	2.5*
KBMS-11BV	120	1.6
KBMS-13BV	120	3.0
KBMS-23BV	240	3.0

*KBMC-13B and KBMC-23B without enclosure ("B") has an increased rating of 3.0 amps.

GENERAL INFORMATION

Controls as indicated are supplied as standard with the following:

- ABS enclosure
- "On/Off rotary line switch"
- High-gain RFI filter
- Minimum speed trimpot

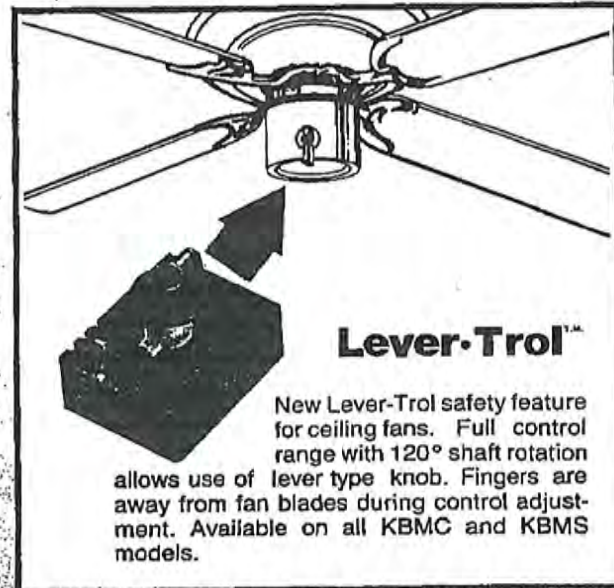
To eliminate ABS enclosure delete "B" suffix from model No. (KBMC-13)

To eliminate RFI filter add "I" suffix to model No. (KBMC-13I)

To eliminate "On/Off" switch add "NS" suffix to model No. (KBMC-13NS)

To eliminate minimum speed trimpot delete "V" from model No.

POTENTIOMETER ROTATION: on controls with built-in On/Off switch, control output is from "OFF" to "HIGH" to "LOW" with clockwise potentiometer shaft rotation. To reverse control output to "OFF" to "LOW" to "HIGH" add



"R" suffix to model No. (KBMC-13R). On controls without built-in ON/OFF switch (NS suffix), control output is from "Low" to "High" with clockwise potentiometer shaft rotation. To reverse control output to "High" to "Low" add "R" suffix to model No. (KBMC-13NSR).

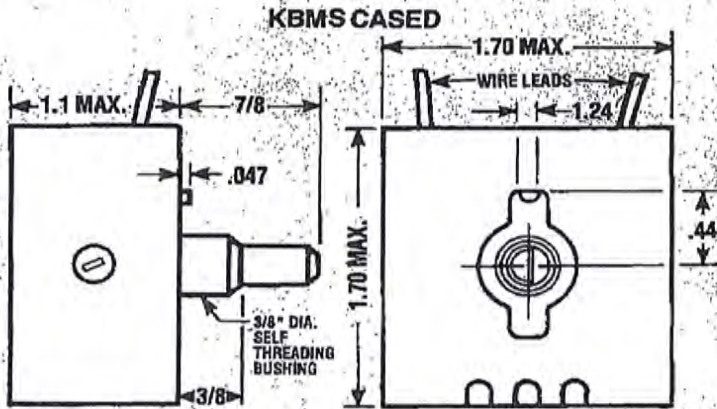
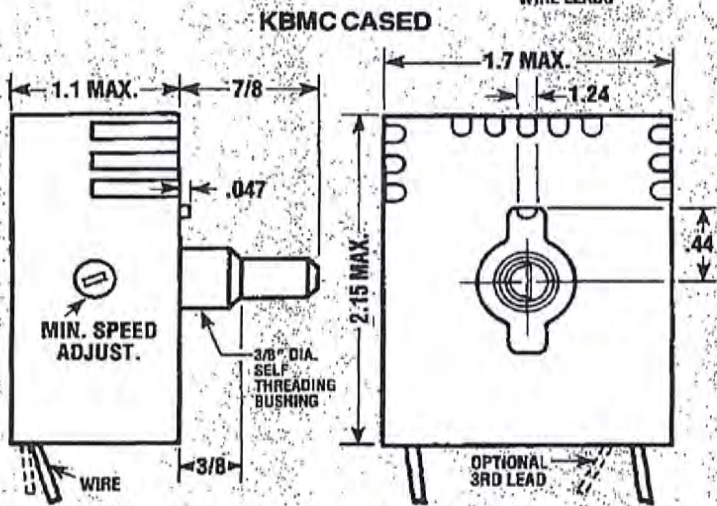
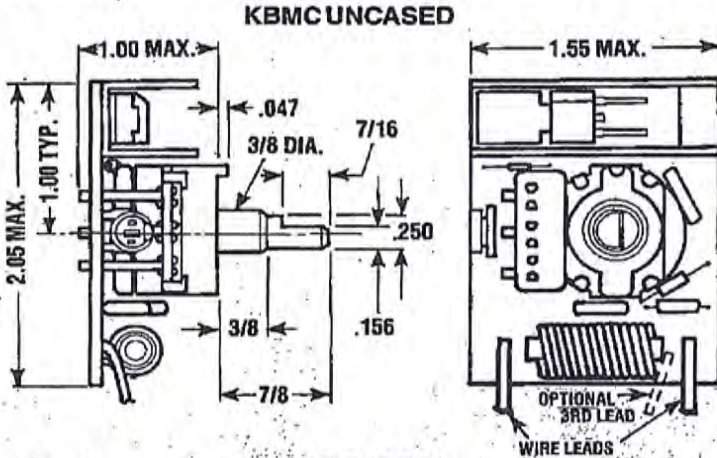
LEADS: standard leads are No. 18 AWG and are approximately 6" long and stripped 1/2". Other lead lengths are available upon request. Quick-disconnect terminals on leads also available.

SUFFIX ADDERS WITH DESCRIPTIONS

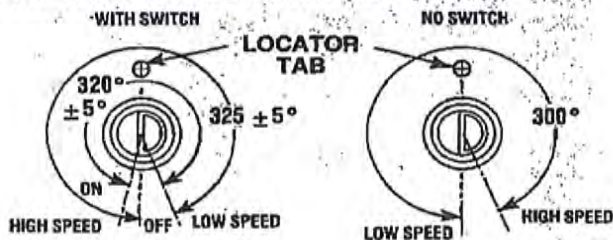
Suffix Identification	Description	Notes
B	Adds Enclosure, Flame Retardant ABS	All KBMS models and model KBMC-14B are always supplied with ABS enclosures
V	Adds Minimum Speed Trimpot	A fixed resistor is used on all models that do not contain the minimum speed trimpot
K	Adds Kit for Wall Box Mounting	Mounting Kit contains Dial Plate, Mounting Strap, Knob, Mtg. Hardware, Instructions and Individual Packaging
LT	Adds Lever-Trol™	Lever-Trol feature restricts potentiometer rotation to 120° so that a lever type knob can be utilized
NS	Deletes On/Off Line Switch	When On/Off switch is not supplied the standard control output is from "Low to High"
I	Deletes RFI Filter	Caution must be exercised when eliminating RFI filter (see application notes)
F	Adds Built-In Fuse	Built-in fuse is available on KBMC models only. Fuse rating and type must be specified.
L	Adds Auxiliary 3rd Lead	Total current of motor load and auxiliary load must not exceed 4.0 amps.
R	Reverses Control Output Vs. Pot. Rotation	(See general information on Potentiometer Rotation)

TECHNICAL DATA D-157

TYPICAL DIMENSIONS (INCHES)



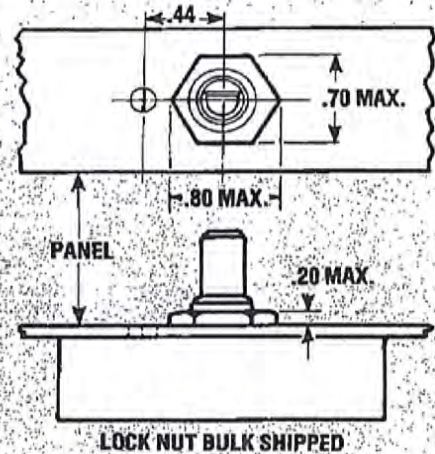
POTENTIOMETER ROTATION (Except Lever-Trol.)



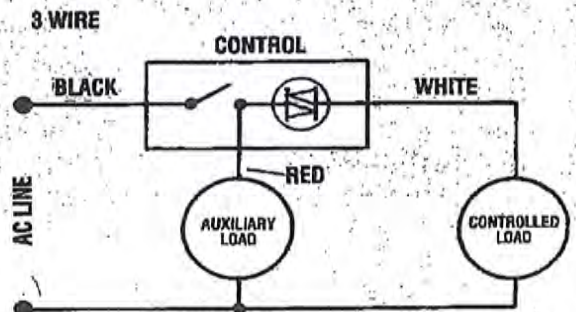
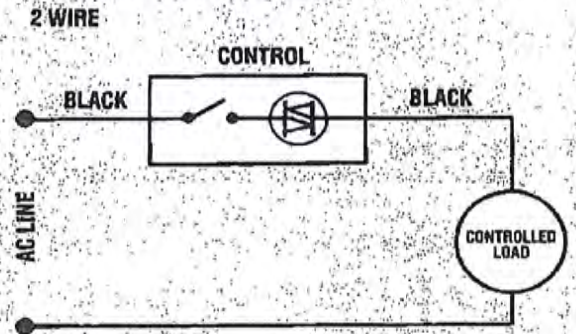
ALTERNATE MOUNTING BUSHING



MOUNTING DIMENSIONS



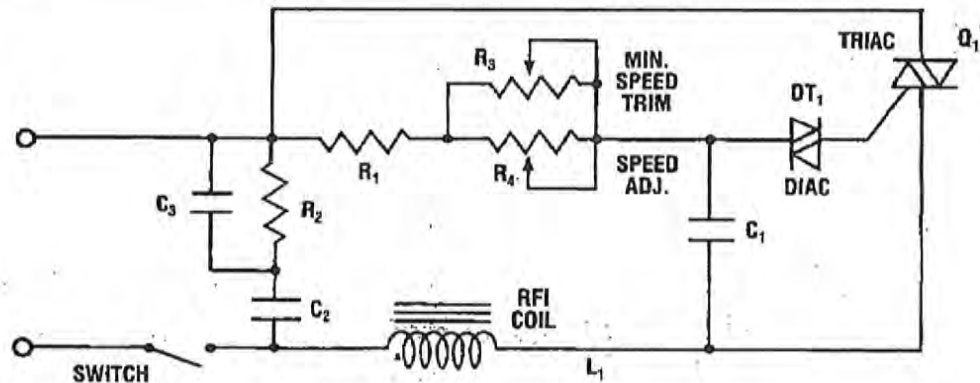
CONNECTION DIAGRAMS



NOTE: SWITCH rated 4.0 amps RMS.

TECHNICAL DATA D-157

SCHEMATIC



NOTE: In some models actual circuits used may vary from schematic as shown.

APPLICATION NOTES:

1. *Temperature Test* — The non-sinusoidal output voltage of a solid state control may increase motor heating. Therefore, it is necessary that a temperature test be performed to insure that motor is operating within manufacturer's specifications.

2. *Failure Mode* — Certain failure modes of solid state controls, such as half-waving, can cause high levels of DC. This may produce severe overheating and motor burnout. Therefore, a thermal overload protector is required which will limit the maximum motor temperature as prescribed by the manufacturer.

3. *Radio Frequency Interference (RFI)* — Solid state speed controls usually generate annoying radio noise on the AM broadcast band. KB controls incorporate, as standard, a high-gain RFI suppression filter which significantly reduces this interference.

4. *Low End Set Point* — All controls are set to 65 volts

+/- 3V output as standard with an input voltage of 120 volts. An average responding AC voltmeter is used for calibration. Custom voltage settings are available as per customer requirements.

5. *Motor Suitability* — Motors must be loaded to near full capacity with appropriate fan blade in order to achieve proper speed control. Generally, motor suitability is established by determining motor speed as a function of applied voltage. Motor is determined as suitable if it changes speed linearly over a wide range of voltage.

6. *Overseas Markets* — Standard snubber network components are prone to failure when used on power sources with abnormally high transients. Therefore, controls that are used in remote areas of the world, such as Asia, Africa, and Australia, or where power generation is not properly regulated, require a special snubber. KB uses metalized paper capacitors and flameproof resistors in these applications.

Other Variable Speed Solid State AC Motor Controls

• DESIGNED FOR 2" x 4" ELECTRICAL WALL BOX INSTALLATION •



2.5, 3.0, 4.0, 5.0 &
6.0 AMP. MODELS



8.0 & 10.0 AMP. MODELS



10.0, 12.0 & 15.0 AMP. MODELS



NEW FROM KB

The KBMS-13 has been packaged into a compact plug-in control with no wires to connect.

Just plug your fan into the convenient DIAL-A-TEMP receptacle. Then plug DIAL-A-TEMP into a standard 120 volt outlet.

MATERIAL SAFETY DATA SHEET

SECTION I

Trade Name and Synonyms: Fiberglass Rope, Tape, Sleeving
Chemical Name and Synonyms: Continuous Filament Fiberglass (Fibrous Glass, Glass Fibers)
Manufacturer's Name: Fil-Tec, Inc.
Address: P.O. Box B, Hagerstown, MD 21741-1508
Telephone #: (301) 824-6166

SECTION II - INGREDIENTS

Ingredients:	%	TLV(R) (Units)	PEL
<u>Fibrous Glass:</u> Composition consisting principally of oxides of silicon, aluminum, calcium, boron and magnesium fused in an amorphous vitreous state.	≥ 96.5	10 mg/M ³	None Established (5 mg/M ³ - respirable nuisance dust)
<u>Surface Sizing:</u>	≥ 3.5	Non Established	Non Established

SECTION III - PHYSICAL DATA

Melting Point (Softening): 800°C Specific Gravity (Bare Glass): 2.59
Boiling Point (°F): Not Applicable Percent, Volatile (Volume): 0
Vapor Pressure (mm Hg.): Not Applicable Evaporation Rate: Not Applicable
Vapor Density (Air=1): Not Applicable Solubility in Water: Insoluble
Appearance and Odor: A texturized product consisting of yellow-white to white fibers bound together in strands and manufactured into rope, tape or sleeving.
Fiber Diameter: Normally there are no fibers with diameters smaller than 4.7 microns in any Fil-Tec, Inc. rope, tape or sleeving products.

SECTION IV - FIRE AND EXPLOSION HAZARD DATA

Flash Point: Non-Burning
Flammable Limits: Not Applicable
Extinguishing Media: Not Applicable
Special Fire Fighting Procedures: In a sustained fire, self-contained breathing apparatus (SCBA) should be worn.
Unusual Fire and Explosion Hazards: Not Applicable

SECTION V - HEALTH HAZARD DATA

Primary Routes(s) of Entry: Inhalation
Signs and Symptoms of Overexposure: Rash, itching, conjunctivitis, coughing, sneezing.
Health Hazards: (Acute): Exposure to glass fibers sometimes causes irritation of the skin and, less frequently, irritation of the eyes, nose or throat.
(Chronic): A number of epidemiology studies, done over many years, of workers employed for up to 40 years in the manufacture of fiberglass have shown no evidence of increases in either malignant or non-malignant respiratory disease attributable to exposure to fiberglass. However, recent studies have shown slight increases in lung cancer among workers employed in the manufacture of glass wool and mineral wool insulation products.

FIBERGLASS ROPE SEALS PART # FR1LD.625G	DATE: 4/8/99		FIL-TEC, INC.
	DRWG: CMP	APP. AY	P.O. BOX B, HAGERSTOWN, MD 21741-1191
			NO. FR1LD.625G

DESCRIPTION: GRAPHITE COATED TYPE 1 LOW DENSITY FIBERGLASS ROPE

SPECIFICATIONS:

Diameter: .625 ($\pm 5\%$)
Material: Fiberglass texturized yarn, service rating 1000°F (538°C)
Yield: 19.94 ft/lb. ($\pm 5\%$)



FIBERGLASS ROPE SEALS PART # FTBH125X1.00GA	DATE: 4/8/99		FIL-TEC, INC.
	BY: CMP	APP: CHR	P.O. BOX B, HAGERSTOWN, MD 21741-1191 NO. FTBH125X1.00GA

DESCRIPTION: .125" X 1" graphite coated fiberglass bolt hole tape
w/pressure sensitive adhesive

SPECIFICATIONS:

Yield: 54 ft/lb. \pm 5% *without adhesive*

Width: 1" \pm 5%

Thickness: .125" \pm 5%

Material: Fiberglass texturized yarn, service rating 1000°F (538°C)
Acrylic based pressure sensitive adhesive



ELECTRICAL SUBMITTALS

Manufacturer: RJW MANUFACTURING, INC
 Model No.: SBLOS4-OJ
 Type of Appliance: BLOWER

MOTOR:

Manufacturer	<u>JAKEL, INC</u>	
Model Number	<u>J239-115-025271</u>	
Voltage	<u>115V</u>	
F.L. Amps	<u>93/80 A</u>	
L.R. Amps	<u>1.4/1.2 A</u>	
Phase/Cycle	<u>SINGLE 50/60 HZ</u>	
Horsepower	<u>1/50</u>	
R.P.M.	<u>3000 RPM 60 HZ</u>	
Approval Agency	<u>UL</u>	<u>CSA</u>
File Number	<u>E48562</u>	<u>LR10432</u>
Winding Type	<u>WOUND ROBBIN SINGLE</u>	<u>COIL</u>
Temperature Rating	<u>130°C</u>	
Is motor Impedance Protected?	<u>NO-THERMALLY</u>	
Insulation class of Leads	<u>125°C</u>	
Type of strain relief provided at leads?	<u>STRAIN RELIEF POCKETS</u>	

OVERLOAD PROTECTIVE DEVICE:

Manufacturer	<u>TEXAS INSTRUMENTS</u>	
Model Number	<u>TAM209AS</u>	
Approval Agency	<u>UL</u>	<u>CSA</u>
File Number	<u>E15962</u>	<u>113720</u>
Voltage	<u>115V</u>	
Current Rating	<u>22A</u>	
Temperature rating	<u>110°C</u>	
Authority for temp	<u>±5°C</u>	

MATERIAL SAFETY DATA SHEET
100% RTV Silicone

PREPARED: 3/27/92

PALMETTO G & B PRODUCTS

106 N. HAMPTON ST.
 KERSHAW, SC 29067
 PH. 803-475-8766

I PRODUCT IDENTIFICATION

Product Identification: 100% RTV Silicone
Chemical Name: Silicone Sealant

Chemical Family: Silicone Sealant
Formula: Mixture

II PRODUCT COMPONENTS

Product Composition	Approx. %	ACGIH TLV	OSHA PEL	UNITS	CAS REG NO.
A. Hazardous					
Methyltriacetoxysilane	< 05%	10		PPM	4253-34-3 *
B. Non-Hazardous					
** Product Information	NA	NA	NA	NA	NA

III PHYSICAL DATA

****Product Information**

- Boiling Point NA (F) NA (C)
- Physical State Paste
- Vapor Pressure (20C)
- Odor Acetic Acid
- Vapor Density (Air=1) NEG.
- Color All Colors
- Solubility in Water (20C) Insoluble PH NA
- Solubility in Organic Solvent Acidity/Alkalinity Unknown MEG/G
 (State Solvent) Unknown
- Freezing Point NA (F) NA (C) Density 1066.4 KG/M3
- Melting Point NA (F) NA (C) Specific Gravity (Water=1) 1.07
- % Volatile By Volume < 5 ; Evaporation Rate (Butyl Acetate=1) < 1

IV FIRE AND EXPLOSION DATA

- Flash Point > 400 (F) > 204 (C) By TCC Ignition Temp UNK (F) UNK (C)
- Flamable Limits in Air (%): Lower NA Upper NA
- Extinguishing Media: All Standard Firefighting Media Dry Chemical
- Special Firefighting Procedures: None Known

V REACTIVITY DATA

- Stability: X Stable Unstable
- Hazardous: Polyherization will not Occur
- Carbon Monoxide.
- Carbon Dioxide.
- Silicon Dioxide.
- Acetic Acid.

- Incompatibility (Materials to Avoid): None Known
- Conditions to Avoid: None Known.

PALMETTO G & B PRODUCTS

106 N. Hampton St.
Kershaw, SC 29067

PRODUCT NAME:

Rhodorsil 3B- A one
component Silicone
Elastomeric Sealant

MANUFACTURER:

Rhône-Poulenc Inc.
Specialty Plastics Division
CN-5266

Difference in
test results using
III-Temperature
Red Sealant

CHARACTERISTIC

As Supplied		
Specific Gravity at 77F	1.03	1.07
Tack-Free Time at 77F and 50% RH, min	10-20	
Flow Rate (sag or slump on 1/4 x 4" bead), in	NIL	
Extrusion Rate (1/4" orifice, 90psi), gms/min	350	335
Cure Time at 77F and 50% RH (1/4" thickness), hrs	24	

As Cured ¹ - Physical	TEST METHOD		
Tensile Strength, psi (MPa)	ASTM D 412	350	375
Peel Strength, ² ppl, glass	ASTM D 412	20	
Tear Strength, ppl	ASTM D 412	28	
Durometer Hardness, Shore A, Points	ASTM D 676	25	30
Elongation, Percent	ASTM D 412	500	400
Brittle Point, Degrees	ASTM D 746	100F	
Weight Loss, after 100 hrs at 392F, Percent		NONE	
Water Absorption-7 days at 77F, Percent	ASTM D 570	0.40	
Volume Coefficient of Thermal Expansion, 32-212F	ASTM D 213A		
		9.3×10^{-4}	
BTU per (ft) (degrees F) (hr)		0.11	0.12
Thermal Conductivity, cal/(cm) (degrees C) (sec)		0.45×10^{-3}	0.5×10^{-3}
Shrinkage, after 3 days at 77F, Percent		NIL	
Lap Shear Adhesion, ³ strength, psi			
1/16-inch lap joint thickness		192	
1/8-inch lap joint thickness		113	
1/4-inch lap joint thickness		67	
3/8-inch lap joint thickness		44	
1/2-inch lap joint thickness		37	

As Cured ⁴ - Electrical			
Volume Resistivity, ohm-cm	ASTM D 257	1.5×10^{13}	3×10^{14}
Dielectric Strength, ⁵ volts/mil	ASTM D 149	550	500
Dielectric Constant at 60 Hz	ASTM D 150	2.8	
at 100 Hz	"	2.8	
at 100 KHz	"	2.8	
Dissipation Factor at 60 Hz	ASTM D 150	0.0015	0.0026
at 100 Hz	"	0.0015	0.0026
at 100 KHz	"	0.0015	0.0026
Arc Resistance, Seconds	ASTM D 489	50	
Maximum Continuous Operating Temperature, degrees		+450°F	+500°F
Maximum Intermittant Operating Temperature, degrees		+500°F	+650°F

- 1 Measured on 1.91-mm-thick (0.075-inch) slabs after curing 72 hours at 25 C (77 F) and 50% RH.
- 2 Tested on standard sheet glass.
- 3 Measured with 1/4-inch overlap on test piece.
- 4 Measured on 1.91-mm-thick (0.075-inch) cross section after vulcanizing 72 hours at 25 C (77 F) and 50% RH.
- 5 Measured at 65-mil thickness, 1/4-inch ASTM electrodes in oil, rapid rise.

These values are not intended for preparation of specifications. All technical information contained herein is based on tests we believe to be reliable, but the accuracy thereof is not guaranteed.

Please Note: III-Temp Red is designed to meet low volatility requirements as specified by General Motors for use on vehicles equipped with oxygen sensors.



SC-000-041 REV.7
DATE 1/97

Material Safety Data Sheet (MSDS)

Conforms to requirements of OSHA standard 1910.1200
"Hazard Communication" and to various state "Employee Right to Know" Laws
© Copyright 1997 American Foundrymen's Society, Inc.

Vendor name and address:

THE FOUNDRY OF THE SHOALS, INC
201 COMMERCE STREET
P. O. BOX 916
FLORENCE, AL 35631

Emergency phone number:

(256) 760-2050

GRAY IRON

SECTION I — PRODUCT IDENTIFICATION

This MSDS supplied for: GRAY IRON

ASTM ALLOY DESIGNATION

SECTION II — HAZARDOUS COMPONENTS

INGREDIENT	CAS NO.	PERCENT	TLV (mg/m ³)	PEL (mg/m ³)
Carbon	7440-44-0	2.5-4.0	N/E	N/E
Chromium*	7440-47-3	0.01-0.9		
Chromium (II) Compounds as Cr			0.5	0.5
Chromium (III) Compounds as Cr			0.5	0.5
Chromium Metal as Cr			0.5	1.0
Chromium VI Insoluble Compounds			0.01	N/E
Chromic Acid and Chromates as CrO ₃			N/E	1.0 mg/10m ³
Chromium VI Compounds Water Soluble as Cr			0.05	0.1 (CL)

Iron	1309-37-1	86.3-96.2		
Iron Oxide Fume (Fe ₂ O ₃)			N/E	10.0
Iron Oxide Dust and Fume (Fe ₂ O ₃)			5.0	N/E
Manganese* (as Mn)	7439-96-5	0.2-1.1		
Fume as Mn			N/E	5.0 (CL)
Elemental and Inorganic Compounds as Mn			0.2	N/E

SECTION II — HAZARDOUS COMPONENTS (cont'd.)

INGREDIENT	CAS NO.	PERCENT	TLV (mg/m ³)	PEL (mg/m ³)
Nickel*(as Ni)	7440-02-0	0.01-1.5		
Metal			1.0	1.0
Insoluble Compounds as Ni			1.0	1.0
Soluble Compounds as Ni			0.1	1.0
Silicon	7440-21-3	1.0-3.5		
Total Dust			10.0	15.0
Total Respirable Dust			N/E	5.0

N/E = none established. N/A = not applicable. N/D = no data available.
TLV = American Conference of Governmental Industrial Hygienists (ACGIH) Threshold Limit Value (8-hour time weighted average).
PEL = OSHA Permissible Exposure Limit. The PEL values given are those promulgated as final limits as part of OSHA's 1989 PEL project (8-hour time weighted average).
mg/m³ = Milligrams per cubic meter of air.
NTP = National Toxicology Program.
CL = Ceiling Limit.
STEL = Short Term Exposure Limit.

CARCINOGEN CLASSIFICATION

INGREDIENT	OSHA	NTP	IARC	TARGET ORGAN
Chromium Hexavalent	N	1	1	Lung
Nickel	N	2	2B	Lung, nasal

Y = Listed as Human Carcinogen. N = Not Listed as a Human Carcinogen.
Code for IARC (International Agency for Research on Cancer) evidence for human carcinogenicity: 1 = positive; 2A = probable; 2B = possible; 3 = not classified; 4 = probably negative.
Elements having a listed percentage greater than zero will be present in all grades. Those having a value of "0" may not be present in certain grades.

N/E means none established. N/A means not applicable. N/D means no data available.

Material Safety Data Sheet (MSDS)

Label information for SC-000-041 REV. 7 DATE 1/97

The following hazard information is required for labels under OSHA Standard 1910.1200 and applicable instructions. Other label information may be added.

GRAY IRON

CAUTION

Grinding, welding, or arc gouging of this casting creates dust or fumes containing substances listed below with corresponding possible health effects after prolonged or repeated overexposure:

Carbon: Respiratory and skin irritation.

Chromium, Hexavalent: Lung cancer.

Iron: Siderosis "iron pigmentation" of the lung, which can be seen in a chest x-ray but causes little or no disability.

Manganese: Central nervous system effects are: sleepiness, weakness in legs, spastic gait, emotional disturbances.

Nickel: Dermatitis, lung and nasal cancer.

Silicon: Skin, eye and nose irritation.

Wear eye protection. Wear approved dust and fume respirator if exposures exceed safe limits.

For additional information, see Material Safety Data Sheet SC-000-041 Rev. 7 for this material.

SECTION II — HAZARDOUS COMPONENTS (cont'd.)

*This constituent, a toxic chemical, makes this product subject to the reporting requirements of Section 313 of Title III of the Superfund Amendments and Reauthorization Act of 1986 and 40 CFR Part 372. Quantity threshold amounts are 25,000 pounds for manufacturing, importing or processing and 10,000 pounds for otherwise using the listed chemical. Chemicals marked ** are reportable only if in the form of dust or fume.

SECTION III — OVERVIEW

There are no chemical hazards from these castings in solid form.

Dust or fumes generated by machining, grinding, or welding of the casting will put contaminants in the air. Since the casting is over 85% iron, most of the dust or fume will be iron or iron oxide. There is no TLV for iron dust, but available information indicates that a concentration of 10 mg/cu.m., as if it were a nuisance dust, will serve as a guideline until a TLV is established.

High production dry machining of gray iron castings usually requires local exhaust ventilation.

Flame cutting, arc gouging, or welding of the casting generates iron oxide fume. Inhalation of too much iron oxide fume over a long time can cause siderosis, sometimes called "iron pigmentation" of the lung. It can be seen on a chest x-ray but causes little or no disability. Also see the MSDS for the welding rod being used.

Welding or flame cutting may convert a fraction of the chromium to the water insoluble hexavalent (carcinogenic) form, but the chromium content of the casting is so low that over-exposure is not likely.

Nickel has been shown to cause cancer in laboratory animals. However, its potential to cause cancer in humans has not been determined. The nickel content of the casting is so low that over-exposure is not likely.

Grinding castings that have not been cleaned or that contain embedded sand will generate significant amounts of dust containing free silica, which can cause silicosis. Good local ventilation is frequently required to prevent over-exposure in this situation.

SECTION III — OVERVIEW (cont'd.)

If good ventilation is not available, use a NIOSH-approved dust respirator. IARC has listed crystalline silica as Class 2A, probably can cause lung cancer. Other toxic metals in the alloy are present in small amounts that will not represent a hazard if iron dust and fume are adequately controlled.

SECTION IV — PHYSICAL DATA

PHYSICAL DESCRIPTION: Solid, silver gray in color, no odor
BOILING POINT: 2750C for iron
VAPOR PRESSURE: N/A
VAPOR DENSITY: N/A
SOLUBILITY IN WATER: N/A
SPECIFIC GRAVITY: 7.86 for iron
PERCENT VOLATILE BY VOLUME: N/A
EVAPORATION RATE: N/A

SECTION V — FIRE AND EXPLOSION DATA

Castings will not burn or explode.

SECTION VI — HEALTH HAZARD DATA

EYES: Metal particles in the eyes may cause irritation if not removed. Contact lenses should be worn with caution in a metalcasting environment. Obey work rules concerning contact lenses.

SKIN: Carbon: Skin irritation; Nickel: Dermatitis; Silicon: Skin irritation.

BREATHING: Prolonged or repeated overexposure to dust or fumes from these castings may cause the following health effects:

Carbon: Respiratory irritation.

Chromium, Hexavalent: Lung cancer.

Iron: Siderosis "iron pigmentation" of the lung, which can be seen in a chest x-ray but causes little or no disability.

SECTION VI — HEALTH HAZARD DATA (cont'd)

Manganese: Central nervous system effects are: sleepiness, weakness in legs, spastic gait, emotional disturbances.

Nickel: Lung and nasal cancer.

Silicon: Skin, eye and nose irritation.

Breathing excessive amounts of silica dust for a long time can cause silicosis. Silicosis causes shortness of breath, reduced capacity to do work, and weakens the defenses against other lung diseases.

INGESTION: Hand, clothing, food and drink contact with metal dust, fume or powder can cause ingestion of particulate during hand to mouth activities such as eating, drinking, smoking, nail biting, etc.

NOISE: Grinding or machining castings is noisy. The OSHA limit for noise averaged over eight hours is 90 decibels (dBA). A hearing conservation program is required if exposure is over 85 dBA. If noise is at or above 90 dBA, you should wear ear muffs or ear plugs.

FIRST AID

IF IN EYES: Metal particles should be removed by a trained individual such as a nurse or physician.

IF ON SKIN: Use a mild hand cream if irritation develops.

IF BREATHED: (Fumes from welding): Move to fresh air.

IF INGESTED: Consult local physician.

SECTION VII — REACTIVITY DATA

HAZARDOUS POLYMERIZATION: Will not occur

STABILITY: Stable.

INCOMPATIBILITY: Metal dust can burn or explode and must be protected from ignition sources such as grinding sparks, etc. Under some conditions, metal dust is incompatible with some oxidizing conditions and may be incompatible with oxidizers, acids and water and may ignite or explode.

SECTION VIII — SPILL OR LEAK PROCEDURES

STEPS TO BE TAKEN IF MATERIAL IS RELEASED OR SPILLED:

If damaged, return castings to vendor or send to scrap reclaimer.

Collected dust from machining, welding, etc., may be classed as a "hazardous waste" depending on circumstances. Consult local authorities regarding disposal.

SECTION IX — PROTECTIVE EQUIPMENT TO BE USED

RESPIRATORY PROTECTION: Wear a NIOSH approved respirator for dusts or fume if concentrations exceed the TLV or PEL.

VENTILATION: Provide general ventilation and/or local exhaust if necessary to maintain concentrations below the TLVs.

PROTECTIVE GLOVES: Work gloves advisable for handling castings.

EYE PROTECTION: Safety glasses with side shields and/or face shields for particles (grinding). Welding goggles or helmet for welding.

OTHER PROTECTIVE EQUIPMENT: Wear a protective apron and gauntlets if arc-air gouging or cutting, or welding castings. Safety shoes may be required during certain operations.

If noise is at or above 90 dBA, you should wear ear muffs or ear plugs.

SECTION X — SPECIAL PRECAUTIONS OR OTHER COMMENTS

STORAGE: Keep dry to reduce rusting.

THE INFORMATION HEREIN IS BASED ON THE VENDOR'S MSDS WITH ADDITIONS AS NECESSARY TO COMPLY WITH CURRENT REGULATIONS. THE INFORMATION IS BELIEVED TO BE ACCURATE BUT UNDER THE CIRCUMSTANCES IS NOT WARRANTED TO BE.



WHITACREGreer
Quality Since 1900

PRODUCT DATA SHEET - REFRACTORIES
March 1, 1998

PRODUCT: W-G Low Duty Firebrick
PLANT: Alliance, Ohio
METHOD OF MANUFACTURE: Vacuum Dry Press

TYPICAL CHEMICAL ANALYSIS

SiO ₂	66.9%
Al ₂ O ₃	25.6%
Fe ₂ O ₃	2.5%
CaO.....	0.2%
MgO.....	0.7%
TiO ₂	1.5%
Alkali.....	2.6%

TYPICAL PHYSICAL PROPERTIES

P. C. E.	20 - 26
Apparent Porosity.....	13 - 17%
Modulus of Rupture.....	700-1200psi

Temperature fired to during manufacture = 2100⁰ F (1149⁰ C)

Manufactured to meet ASTM C 27 (Low Duty) and C 1261

Recommended maximum operating temperature = 2000⁰ F

NOTE: All data subject to reasonable deviation and should not be used as specification.

**Firebrick/Ladle Brick
Material Safety Data Sheet**

Section 6

Potential Exposure

When
Installation:
Removal:

Hazard Form
Dust from handling and cutting brick - see note under Special Precautions
Dust from tearing-out brick after service

Section 7

Corrosivity and Reactivity Data

Stability (stable or unstable):	Stable
Incompatibility (Materials to avoid):	None
Decomposition Products:	N/A
Conditions to be Avoided	NE

Section 8

Disposal Procedures

Spill or Leak Procedures:
Waste Disposal Method:

Use dustless vacuum or sweep up using dust suppressant
Approved landfill in accordance with all Federal, State and Local regulations.

Section 9

Personal Protective Equipment/Procedures

Respiratory Protection: Yes

Type: NIOSH or MSHA Approved dust Respirator

Ventilation:

Local:
Mechanical (General):
Other:

Protective Gloves: Yes

Eye Protection: Yes

Other Equipment: Safety Shoes

Action to be taken during repair and maintenance of equipment that has been in contact with this product: None

Section 10

Special Precautions

During Storage: None

Other:

- A) Brick work must be completely dry before introduction of molten metal to avoid explosion from steam.
- B) See ASTM E1132-86, "Standard Practice for Health Requirements Relating to Occupational Exposure to Quartz Dust."
- C) Avoid creating and breathing dust. Dust generated by dry sawing may contain crystalline silica. Wet sawing is recommended.

Section 11

Preparation/Revision

Date: 2/8/93 Revised 5/1/98

N/A = Not Applicable

NI = No Information or Test Data

NE = Not Established

MATERIAL SAFETY DATA SHEET

=====

| SECTION 1 - CHEMICAL PRODUCT AND COMPANY IDENTIFICATION |

=====

PRODUCT NAME : CHARCOAL GRAY METALLIC H/RESIS
 IDENTIFICATION NUMBER: 1-6-6215 DATE PRINTED: 10/02/97
 PRODUCT USE/CLASS :

SUPPLIER: WARLICK PAINT COMPANY 945 MONROE STREET PO DRAWER 1508 STATESVILLE, NC 28677	MANUFACTURER: WARLICK PAINT COMPANY 945 MONROE STREET PO DRAWER 1508 STATESVILLE, NC 28677
--	--

EMERGENCY TELEPHONE: 704-873-2244 8 AM TO 5 PM MONDAY THRU FRIDAY	EMERGENCY TELEPHONE: 704-873-2244 8 AM TO 5 PM MONDAY THRU FRIDAY
--	--

PREPARER: DGG, PHONE: 704-873-2244, PREPARE DATE: 08/06/97

=====

| SECTION 2 - COMPOSITION/INFORMATION ON INGREDIENTS |

=====

ITEM	CHEMICAL NAME	CAS NUMBER	WT/WT % EQUAL TO
01	ALUMINUM SILICATE	1332-58-7	0.2 %
02	MINERAL SPIRITS	8052-41-3	9.5 %
03	VM&P NAPHTHA	64742-89-8	42 %
04	XYLENE	1330-20-7	4.0 %
05	TOLUENE	108-88-3	6.0 %
06	ISOBUTANOL	78-83-1	14 %
07	METHYL ETHYL KETONE	78-93-3	3.1 %
08	AROMATIC HYDROCARBON	64742-95-6	1.7 %

ITEM	ACGIH		OSHA		COMPANY	SKIN
	TLV-TWA	TLV-STEL	PEL-TWA	PEL-CEILING		
01	10MG/M3	NO INFO				NO
02	100 PPM	NO INFO				YES
03	300 PPM	NO INFO	300 PPM			YES
04	100 PPM	150 PPM				YES
05	50 PPM	NO INFO				YES
06	50 PPM	NO INFO				YES
07	200 PPM	300 PPM				YES
08	100 PPM	150 PPM	50 PPM			YES

(See Section 16 for abbreviation legend)

(Continued on Page 2)

|-----|
SECTION 3 - HAZARDS IDENTIFICATION

*** EMERGENCY OVERVIEW ***: No Information.

EFFECTS OF OVEREXPOSURE - EYE CONTACT: EYES - CAN CAUSE SEVERE IRRITATION, REDNESS, TEARING, AND BLURRED VISION.

EFFECTS OF OVEREXPOSURE - SKIN CONTACT: SKIN - PROLONGED OR REPEATED CONTACT CAN CAUSE MODERATE IRRITATION, DEFATTING, DERMATITIS.

EFFECTS OF OVEREXPOSURE - INHALATION: BREATHING - IN POORLY VENTILATED AREAS EXCESSIVE INHALATION OF VAPORS MAY CAUSE NASAL AND RESPIRATORY IRRITATION, DIZZINESS, WEAKNESS, FATIGUE, NAUSEA, HEADACHE, POSSIBLE UNCONCIOUSNESS AND ASPHYXIATION.

EFFECTS OF OVEREXPOSURE - INGESTION: INGESTION - MAY BE HARMFUL IF SWALLOWED.

EFFECTS OF OVEREXPOSURE - CHRONIC HAZARDS: No Information.

PRIMARY ROUTE(S) OF ENTRY: INHALATION SKIN CONTACT INGESTION

|-----|
SECTION 4 - FIRST AID MEASURES

FIRST AID - EYE CONTACT: EYES - FLUSH WITH LARGE AMOUNTS OF WATER.

FIRST AID - SKIN CONTACT: SKIN - THOROUGHLY WASH EXPOSED AREA WITH SOAP AND WATER.

FIRST AID - INHALATION: No Information.

FIRST AID - INGESTION: SWALLOWING - CALL PHYSICIAN. DILUTE WITH WATER. DO NOT INDUCE VOMITING.

|-----|
SECTION 5 - FIRE FIGHTING MEASURES

FLASH POINT: 24 F
(TAGLIABUE CLOSED CUP)

LOWER EXPLOSIVE LIMIT: 0.7 %
UPPER EXPLOSIVE LIMIT: 11.4 %

AUTOIGNITION TEMPERATURE:

EXTINGUISHING MEDIA: WATER FOG DRY CHEMICAL FOAM CO2

UNUSUAL FIRE AND EXPLOSION HAZARDS: VAPORS ARE HEAVIER THAN AIR AND MAY TRAVEL ALONG THE GROUND OR BE MOVED BY VENTILATION AND IGNITED BY HEAT, PILOT LIGHTS, OTHER FLAMES, AND IGNITION SOURCES. CLOSED CONTAINERS MAY EXPLODE WHEN EXPOSED TO EXTREME HEAT. *** STATIC ELECTRICITY PRECAUTION - ALL CONTAINERS MUST BE GROUNDED

(Continued on Page 3)

SECTION 5 - FIRE FIGHTING MEASURES

WHEN IN USE. ****

SPECIAL FIREFIGHTING PROCEDURES: No Information.

SECTION 6 - ACCIDENTAL RELEASE MEASURES

STEPS TO BE TAKEN IN CASE MATERIAL IS RELEASED OR SPILLED: DIKE AND CONTAIN SPILL WITH AN INERT MATERIAL AND TRANSFER THE LIQUID TO CONTAINERS FOR RECOVERY OR DISPOSAL.

SECTION 7 - HANDLING AND STORAGE

HANDLING: TO PREVENT REPEATED OR PROLONGED SKIN CONTACT, WEAR IMPERMEABLE CLOTHING OR BOOTS.

STORAGE: CONTAINERS OF THIS PRODUCT MAY BE HAZARDOUS WHEN EMPTIED SINCE EMPTIED CONTAINERS RETAIN PRODUCT RESIDUES (VAPORS, LIQUID, AND/OR SOLID). ALL HAZARD PRECAUTIONS GIVEN HERE MUST BE OBSERVED.

SECTION 8 - EXPOSURE CONTROLS/PERSONAL PROTECTION

ENGINEERING CONTROLS: No Information.

RESPIRATORY PROTECTION: IN CASE OF POOR VENTILATION, USE NIOSH/MSHA JOINTLY APPROVED AIR SUPPLIED RESPIRATOR.

SKIN PROTECTION: RESISTANT GLOVES.

EYE PROTECTION: SAFETY GOGGLES.

OTHER PROTECTIVE EQUIPMENT: No Information.

HYGIENIC PRACTICES: No Information.

SECTION 9 - PHYSICAL AND CHEMICAL PROPERTIES

BOILING RANGE	: 175 - 383 F	VAPOR DENSITY	: Is heavier than air
ODOR	: SOLVENT	ODOR THRESHOLD	:
APPEARANCE	: BLACK LIQUID	EVAPORATION RATE:	Is slower than Ether
SOLUBILITY IN H2O	: NONE IN WATER		
FREEZE POINT	:	SPECIFIC GRAVITY:	0.8616
VAPOR PRESSURE	:	pH @ 0.0 %	:
PHYSICAL STATE	:	VISCOSITY	:

COEFFICIENT OF WATER/OIL DISTRIBUTION:

(Continued on Page 4)

SECTION 9 - PHYSICAL AND CHEMICAL PROPERTIES

(See Section 16 for abbreviation legend)

SECTION 10 - STABILITY AND REACTIVITY

CONDITIONS TO AVOID: STRONG OXIDING AGENTS.

INCOMPATIBILITY: No Information.

HAZARDOUS DECOMPOSITION PRODUCTS: THERMAL DECOMPOSITION YIELDS OXIDES OF CARBON.

HAZARDOUS POLYMERIZATION: Will not occur under normal conditions.

STABILITY: This product is stable under normal storage conditions.

SECTION 11 - TOXICOLOGICAL PROPERTIES

No product or component toxicological information is available.

SECTION 12 - ECOLOGICAL INFORMATION

ECOLOGICAL INFORMATION: ALL RAW MATERIALS LISTED ON TOSCA.

SECTION 13 - DISPOSAL CONSIDERATIONS

DISPOSAL METHOD: DESTROY LIQUID BY INCINERATION. CONTAMINATED ABSORBENT MAY BE DEPOSITED IN A LANDFILL IN ACCORDANCE WITH LOCAL, STATE, AND FEDERAL REGULATIONS.

SECTION 14 - TRANSPORTATION INFORMATION

No transportation information is available.

SECTION 15 - REGULATORY INFORMATION

U.S. FEDERAL REGULATIONS: AS FOLLOWS -

OSHA: Hazardous by definition of Hazard Communication Standard (29 CFR 1910.1200)

SECTION 15 - REGULATORY INFORMATION

CERCLA - SARA HAZARD CATEGORY:

This product has been reviewed according to the EPA 'Hazard Categories' promulgated under Sections 311 and 312 of the Superfund Amendment and Reauthorization Act of 1986 (SARA Title III) and is considered, under applicable definitions, to meet the following categories:

None

SARA SECTION 313:

This product contains the following substances subject to the reporting requirements of Section 313 of Title III of the Superfund Amendments and Reauthorization Act of 1986 and 40 CFR Part 372:

CHEMICAL NAME	CAS NUMBER	WT/WT %
XYLENE	1330-20-7	4.0 %
TOLUENE	108-88-3	6.0 %
METHYL ETHYL KETONE	78-93-3	3.1 %

TOXIC SUBSTANCES CONTROL ACT:

This product contains the following chemical substances subject to the reporting requirements of TSCA 12(B) if exported from the United States:

CHEMICAL NAME	CAS NUMBER
XYLENE	1330-20-7
TOLUENE	108-88-3
ISOBUTANOL	78-83-1
METHYL ETHYL KETONE	78-93-3
AROMATIC HYDROCARBON	64742-95-6
SILICONE ALKYD	MIXTURE
GRAPHITE	7782-42-5
NO CHEMICAL NAME FOUND	
ALUMINUM PASTE	7429-90-5
NO CHEMICAL NAME FOUND	

NEW JERSEY RIGHT-TO-KNOW:

The following materials are non-hazardous, but are among the top five components in this product:

CHEMICAL NAME	CAS NUMBER
SILICONE ALKYD	MIXTURE

PENNSYLVANIA RIGHT-TO-KNOW:

The following non-hazardous ingredients are present in the product at greater than 3%:

CHEMICAL NAME	CAS NUMBER
SILICONE ALKYD	MIXTURE
GRAPHITE	7782-42-5

|=====|
| SECTION 15 - REGULATORY INFORMATION |
|=====|

CALIFORNIA PROPOSITION 65:

WARNING: The chemical(s) noted below and contained in this product, are known to the state of California to cause cancer, birth defects or other reproductive harm:

----- CHEMICAL NAME ----- CAS NUMBER
No Proposition 65 chemicals exist in this product.

INTERNATIONAL REGULATIONS: AS FOLLOWS -

CANADIAN WHMIS: This MSDS has been prepared in compliance with Controlled Product Regulations except for use of the 16 headings.

CANADIAN WHMIS CLASS: No information available.

|=====|
| SECTION 16 - OTHER INFORMATION |
|=====|

HMIS RATINGS - HEALTH: 2 FLAMMABILITY: 3 REACTIVITY: 0

PREVIOUS MSDS REVISION DATE: 01/08/97

VOLATILE ORGANIC COMPOUNDS (VOCs): 5.70 lbs/gal, 683 grams/ltr

LEGEND: N.A. - Not Applicable, N.E. - Not Established,
N.D. - Not Determined

The information contained on this MSDS has been checked and should be accurate. However, it is the responsibility of the user to comply with all Federal, State, and Local laws and regulations.

<END OF MSDS>

Operating Instructions for the High Valley 1600 (XTEC) Noncatalytic Woodstove

Primary Air Control:

Pushing the control rod in reduces the size of the orifice.

Low (≤ 1.0 kg/hr): At the stop - 0.55" open

MLow (1.0 - 1.25 kg/hr) : Stop to 1.0625" open

MHi (1.25 - 1.90 kg/hr): .875 - 1.75" open

High (> 1.90 kg/hr): Wide open

Fan Confirmation Test: Stop to 1.0625" open

Door:

Normally close the door as soon as the fuel is loaded into the stove. If ignition is delayed, crack door open slightly. Close door as soon as ignition occurs.

Fan:

Low: On high @ 30 min.

MLow: On high @ 30 min.

MHi: On high @ 30 min.

High: On high @ 5 min.

FCT: Off

LPAO:

Clear coals away from immediately in front of the LPAO (1-3").

High Valley Stoves Model 1600 Step Top Non-Catalytic Wood Burning Stove

Installation
Operation &
Safety Handbook

High Valley Construction & Maintenance Corporation
6573 Highway 226 South
Spruce Pine NC 28777
www.highvalleystoves.com

Safety Notice: If this wood burning stove is not properly installed a house fire may result. For your safety, follow the installation directions. Contact your local building or fire officials about restrictions and installation inspections in your area.

- Section I Safety Precautions
 Wood Burning Stove Installation
 Installation of Legs
 Stove Pipe Installation
 Mobile Home Use and Installation
 Firebrick and Fire Blanket Installation
- Section II Installation of Blower (optional)
 Wiring Diagram
- Section III Glass Installation
 Use and Care of Glass
- Section IV Operations
 Building an Efficient Fire in the Model 1600
- Section V Warranty
 Owner Registration Card

7. SAFETY NOTICE: If this wood stove is not properly installed, a house fire may result. For your safety, follow the installation directions. Contact local building officials about restrictions and installation inspection in your area.
8. Inspect chimney connector and chimney twice monthly and clean if necessary.
9. Keep stove away from combustibles. Follow suggested distances.
10. Install smoke pipe segments with crimped end down. This permits creosote to drip back into the stove and be burned away.
11. The use of aluminum type "B" gas vent is unsafe and prohibited by the National Fire Prevention Association Code.
12. The area through which the chimney pipe will travel should be inspected. If the installation requires cutting a hole in the ceiling, check the attic for wires, ducting, etc., that may interfere.
13. It is vitally important that single wall pipe is *never* closer than three times the diameter of the pipe from a combustible surface. *never* use single wall pipe through a combustible surface.
14. Use only an insulated, all fuel chimney to vent the hot gases out of the house. It will reduce the amount of creosote buildup and improve the draft needed to vent hot gases from the stove.
15. Use a 6" diameter insulated thimble or an 6" diameter insulated all-fuel chimney section when passing through a combustible wall or ceiling.
16. Do not use more than one elbow in the stove pipe
17. Any horizontal pipe should be pitched upward toward the chimney at least 1/4" inch for each horizontal foot.
18. Ensure that the ventilating pipe does not extend so far into chimney flue that it blocks air flow.
19. Particular attention should be paid to the point where the flue passes through a wall or ceiling. This penetration should always be made with insulated pipe and the proper accessories.
20. The longer the pipe and the larger the number of elbows, the greater the chance of dangerous creosote and ash buildup. Modern stoves are engineered to achieve maximum heat dispersal without lengthy vents eliminating a potentially hazardous situation.
21. Use heavy gauge stove pipe: at least 18 gauge, 6 inch diameter.
22. Each stove pipe connection should be joined and secured with sheet metal screws to avoid possible separation during use.
23. The top of the flue must be at least three feet higher than the roof at the point of exit. In pitched roofs, the top of the stovepipe must be at least two feet to the highest point of the roof and at least ten feet away.

6. Install the chimney connector. If it is passing through combustible walls, it must be insulated, such as triplewall pipe. Also, if it is impossible to maintain 10" between your smoke pipe and a combustible wall, use an insulated chimney pipe. Also consult your local building codes and regulations.
7. After the pipe connector is in place, run the stovepipe with the crimped edge down from the chimney connector to the stove. The crimped edges must be down so creosote accumulating on the walls of the stovepipe can run back into the stove and not out the joints of the pipe.
8. Check the installation to determine the pipe is connected properly using three sheet metal screws per joint; that the proper distances have been maintained from combustible surfaces with the stove and the stovepipe; and the chimney is in good repair and is installed properly.

Instructions for Mobile Home Use

Optional outside air kit required

1. Before mounting legs onto unit remove the four leveling bolts on bottom of legs.
2. Mount four legs onto unit.
3. Position the stove onto the floor protector in its final location. Making sure all minimum clearances are met. Mark the location of the four legs. Remove the stove and drill a 5/16" hole through the floor of the home in the four locations
4. Reposition the stove and insert a 5/16" bolt (not supplied) through the hole in the bottom of each leg and fasten to the floor.
5. The stove should be grounded to the chassis with a #8 AGW copper wire or equivalent.
6. Place the outside air kit on the rear of the unit with the elbow turned toward the bottom of the unit and fasten with 2 tec screws supplied. Connect a 4" flex pipe (not supplied) to the outside air kit, place a screen on the other end and insert through the wall of the home.
7. On the front of the stove located under the hearth notice a 5" X 1 5/8" opening. Place the 6" X 2" plate (provided with the outside kit) over this opening and attach.

Section V

HIGH VALLEY STOVES LIMITED WARRANTY

PRODUCTS GUARANTEED

This limited warranty covers all stoves manufactured by High Valley Construction & Maintenance Corporation.

GENERAL WARRANTY PROVISIONS

High Valley Stoves, warrants the model 1600 against defects in material and workmanship for 5 years as long as it is owned by the original purchaser provided (1) stove is installed by an authorized installer: (2) stove has not been repaired by an unauthorized person in any way, so as, in our judgement as manufacture, performance or reliability is reduced: (3) stove has not been subject to unauthorized modification: (4) the right to repair or replace the stove is at the option and considered the judgment of the manufacturer: (5) obligation under this warranty does not include or extend to paint on surface of stove, glass door, nor decor kit an optional attachment.

SPECIFIC WARRANTY PROVISIONS & TIME PERIODS

Period 1: 30 days after purchase.

1) Stove should be used within first 30 days by having a fire started, the blower activated, and heat generated in the owners home.

Period 2: 90 days after Purchase.

1) All electrical parts are warranted for 90 days from the date of purchase.

Period 3: Five Years from date of purchase.

1) High Valley Stoves will replace or repair, at its option, any part defective in material or workmanship with the exception of electrical components (blower, thermostat, rehostat, etc.), damper, damper handles and rod, fireclay castable lining, and all parts not permanently attached to the heating unit. Parts not permanently attached to the heating unit are defined as any part removable with common hand tools.

2) The cost of parts only are included. The customer pays any labor or transportation charges required (owner is responsible for any cost involved with stove or part removal and reinstallation.)

Procedure

Should you feel that your stove is defective, you should contact your stove dealer for assistance and for the correct procedures to resolve the problem. If for any reason you are dissatisfied with the suggested procedure, you may contact us in writing at: High Valley Stoves, 6573 Highway 226 South, Spruce Pine, NC 28777.

CONDITIONS & EXCLUSIONS

- 1) There is no other express warranty. All implied warranties or merchantability and fitness are limited to the duration of the express warranty.
- 2) High Valley Stoves is not liable for indirect, incidental, or consequential damages in connection with the use of the product including any cost or expense of providing substitute equipment or service during periods of malfunction or non-use. Some states do not allow limitations on how long an implied warranty lasts, so the above limitation may not apply to you.
- 3) Warranty repairs for reimbursement must be performed by an authorized High Valley Dealer, manufacture's representative, or by customer as directed by dealer or the manufacturer.
- 4) Dealers will receive special instructions regarding minor repairs.
- 5) Warranty void if serial plate has been removed or defaced.
- 6) Warranty gives you specific legal rights and you may also have other rights which vary from state to state.

OWNER REGISTRATION CARD

The owner registration card must be completed in its entirety and mailed to the address on the card within ten (10) days from the purchase in order for warranty coverage to begin.

**VISIT US ON THE WEB @
www.highvalleystoves.com**

HIGH VALLEY STOVES
OWNER REGISTRATION CARD

NAME _____

ADDRESS _____

CITY _____ STATE ____ ZIP _____

TELEPHONE () _____

DEALER WHERE STOVE WAS PURCHASED _____

SELLING PRICE LESS TAX _____

DATE PURCHASED _____

DATE INSTALLED _____

MODEL 1600

SERIAL NUMBER OF WOOD STOVE
(FOUND ON REAR OF UNIT) _____

*REMOVE PAGE FROM BOOK
FOLD IN HALF AND STAPLE*

WOODSTOVE DATA SHEET # 30
STOVE STORAGE

stove storage4/99

The High Valley 1600 noncatalytic woodstove

tested by Myren Consulting, Inc. is being held in custody by

High Valley Stoves/ High Valley Construction and Maintenance, Inc.
and is being stored at:

High Valley Stoves/ High Valley Construction Contact person(s):

6573 Highway 226

Bob or Matt Buchanan

Spruce Pine, NC 28777

Phone: (828) 765-4004

A. Temporary storage at Myren Consulting until certification is granted:

A single strap of steel banding is placed around the stove so that the banding crosses the door horizontally, making it impossible to open the door on the unit. If it is necessary to break the banding to check an internal dimension or component, the banding is immediately replaced after the work on the unit is completed. The unit is identified with its name written on a stove storage label that is taped to the window of the unit. (See next page for an example copy of a stove storage label:)

B. Permanent storage after certification has been granted:

The following measures have been taken to permanently seal the unit and prevent tampering. Several lengths of steel banding are placed around the stove in a manner that prevents the door from being opened. At least two of these lengths cross at 90° angles. At each 90° crossing point on the top of the stove and perhaps elsewhere, a Myren Consulting address label is placed over the crossing point. The lab manager then initials the label and it is then taped in place with 2" clear packing tape. The stove is then loaded onto a pallet and strapped to the pallet with several lengths of steel banding. A box - either cardboard, chipboard or plywood - is placed over the stove and attached to the pallet.

C. The sealed unit is identified as follows:

The name of the unit is written on a Myren Consulting address label which is affixed to the outside of the box. The top and sides of the box also have several stove storage labels affixed to it which clearly identify the unit as a test stove being stored pursuant to 40 CFR Part 60. These labels have the name of the stove clearly written on them. (A sample stove storage label follows on the next page.)

D. The unit was returned to the manufacturer via: common carrier -
USF Reddaway .

WST5-Form11

W A R N I N G

SEALED EPA TEST STOVE

DO NOT OPEN OR TAMPER WITH THE SEALS AND PACKAGING ON THIS STOVE.

TO DO SO WILL VOID THE CERTIFICATION ON THIS STOVE.

High Valley 1600

WST5-Form11

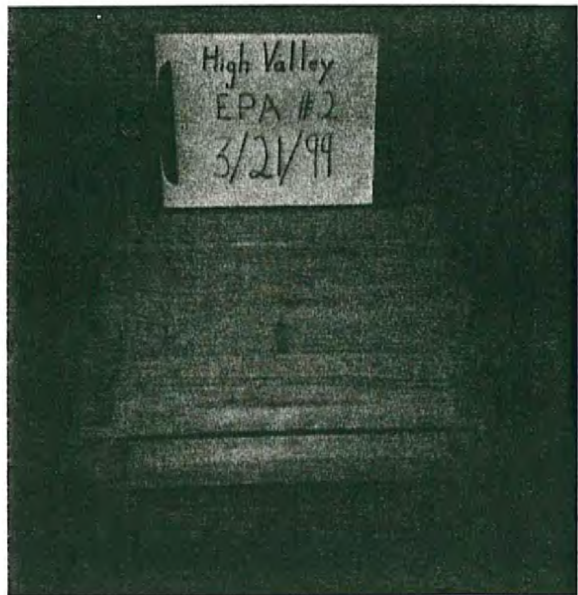
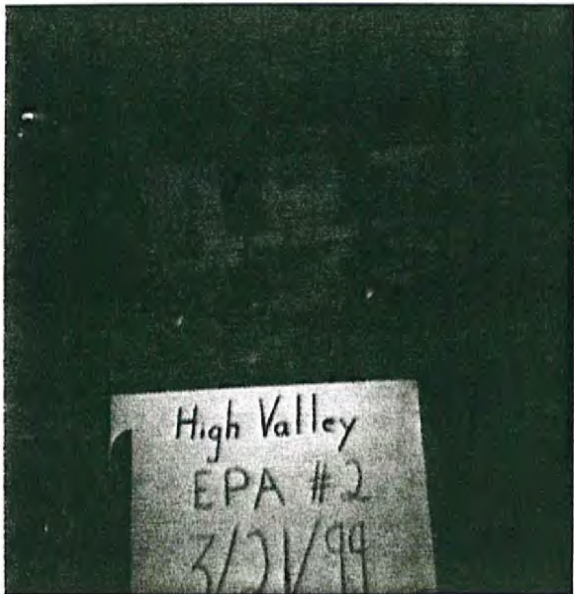
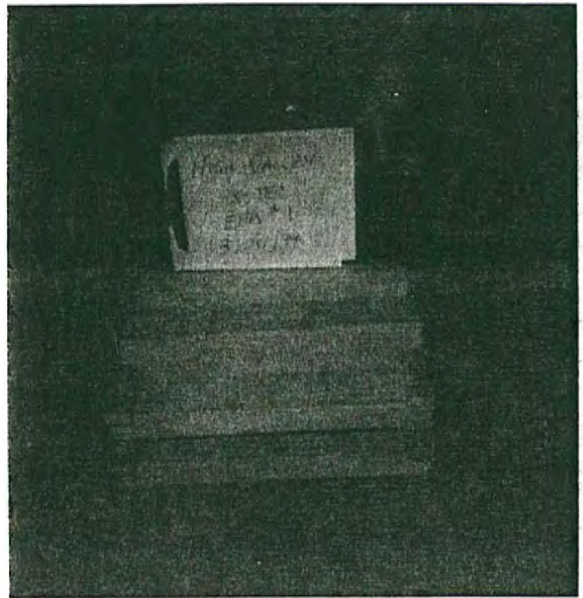
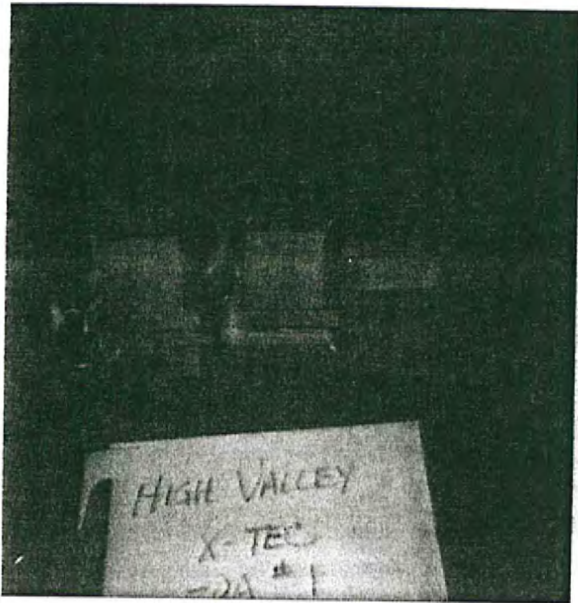
W A R N I N G

SEALED EPA TEST STOVE

DO NOT OPEN OR TAMPER WITH THE SEALS AND PACKAGING ON THIS STOVE.

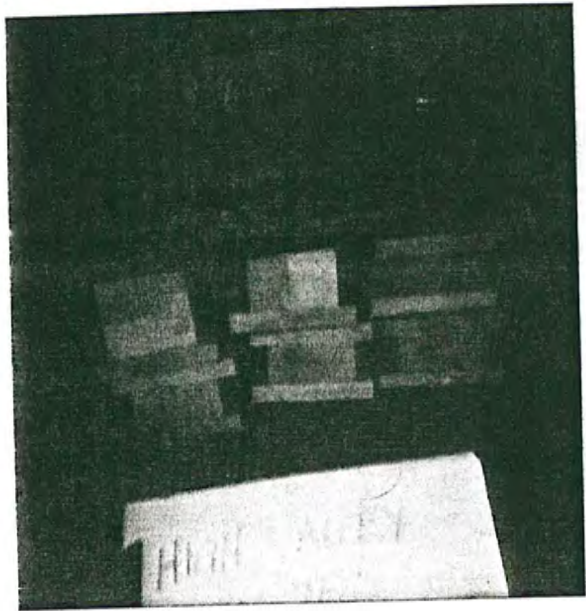
TO DO SO WILL VOID THE CERTIFICATION ON THIS STOVE.

High Valley 1600

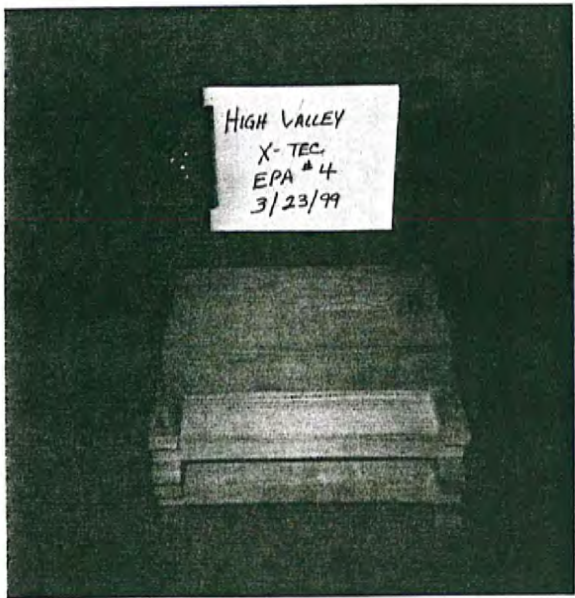




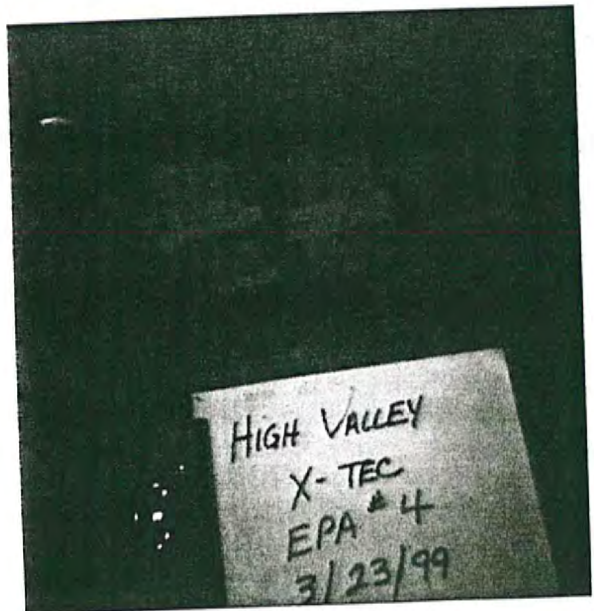
HIGH VALLEY
X-TEC
EPA #3
3/22/99



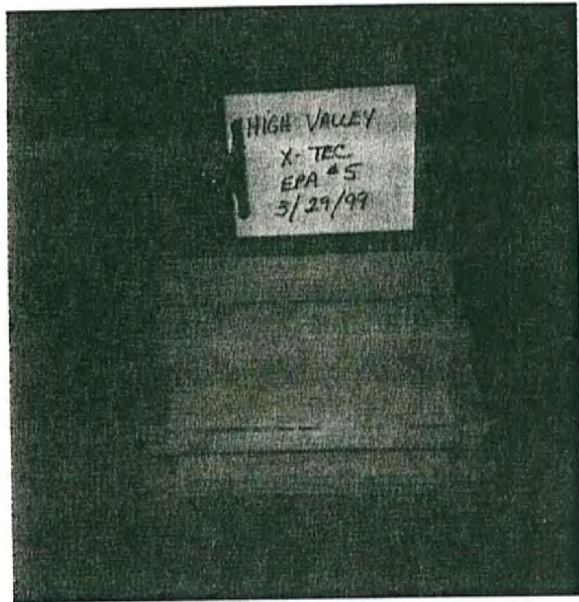
HIGH VALLEY



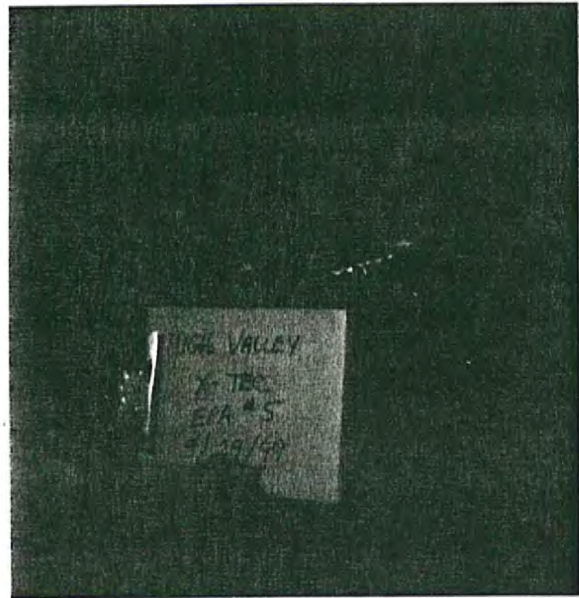
HIGH VALLEY
X-TEC
EPA #4
3/23/99



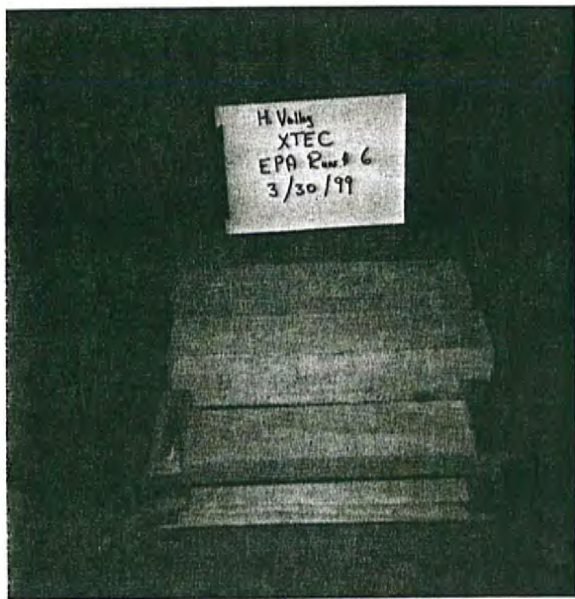
HIGH VALLEY
X-TEC
EPA #4
3/23/99



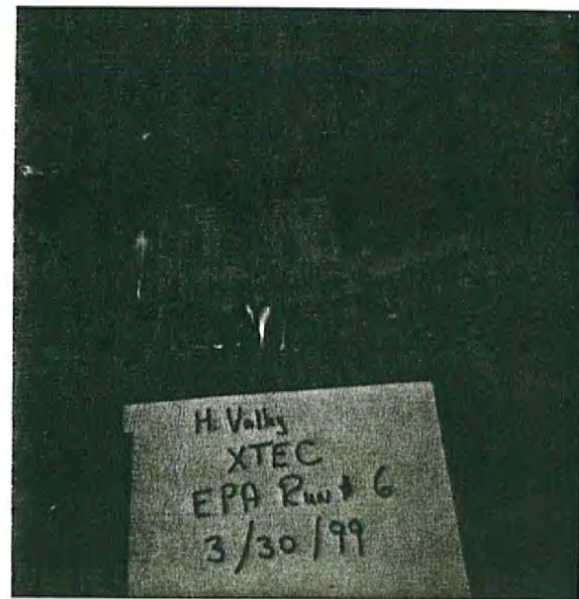
HIGH VALLEY
X-TEC
EPA #5
3/29/99



HIGH VALLEY
X-TEC
EPA #5
3/29/99



H. Valley
XTEC
EPA Ruv # 6
3/30/99



H. Valley
XTEC
EPA Ruv # 6
3/30/99

